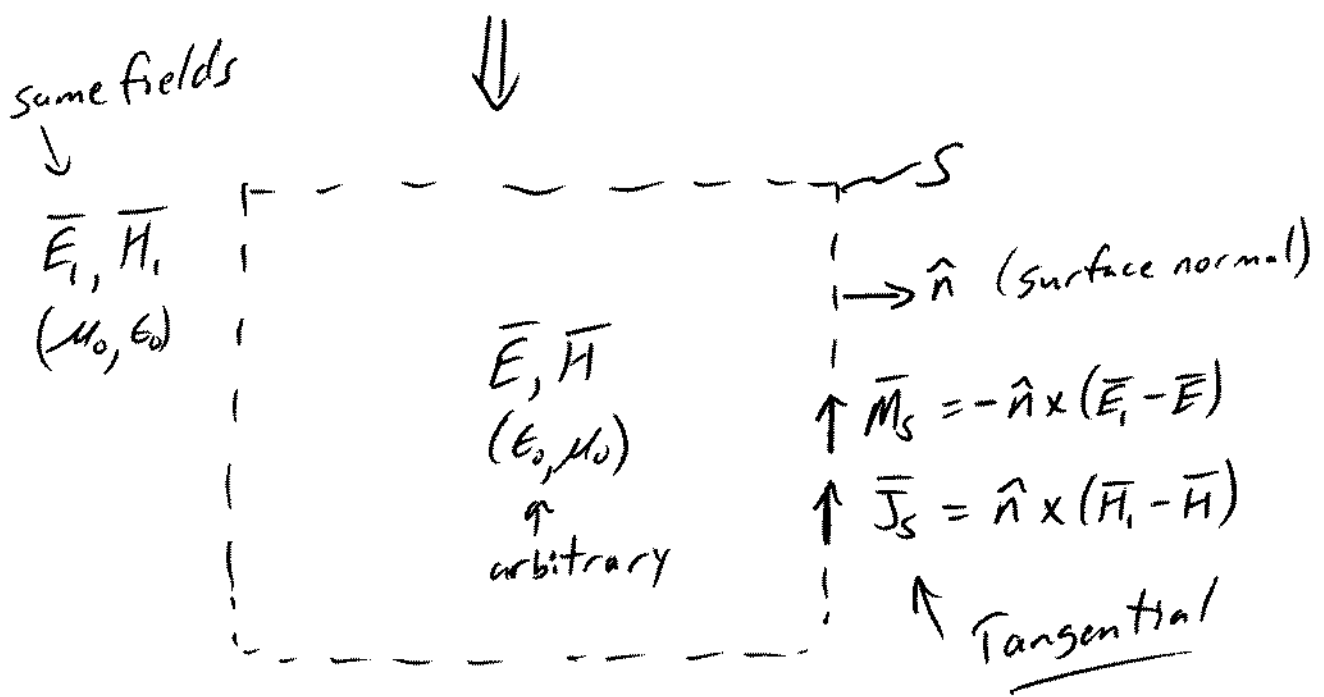
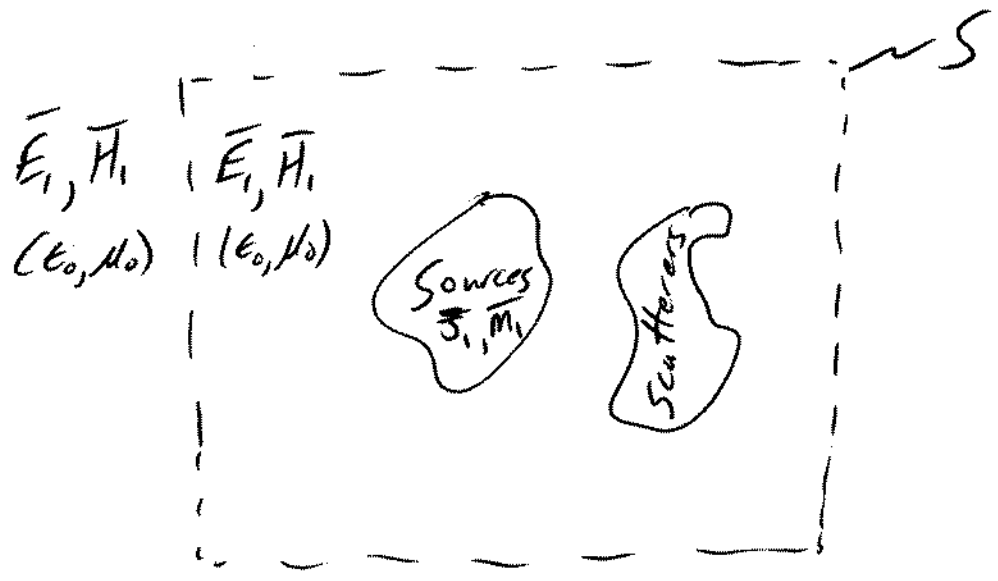


Chapter 8 Near-to-Far-Field Transformation

- use NTFF for Near-to-Far-Field
- do not need to extend FDTD modeling space to the far-field, but can transform near-field data to obtain far-field results
- often done in experimental situations where measurements in the near-field are used to compute far-field results via a NTFF transformation.
- we'll only consider the time-domain NTFF transformations

8.4 Surface Equivalence Theorem

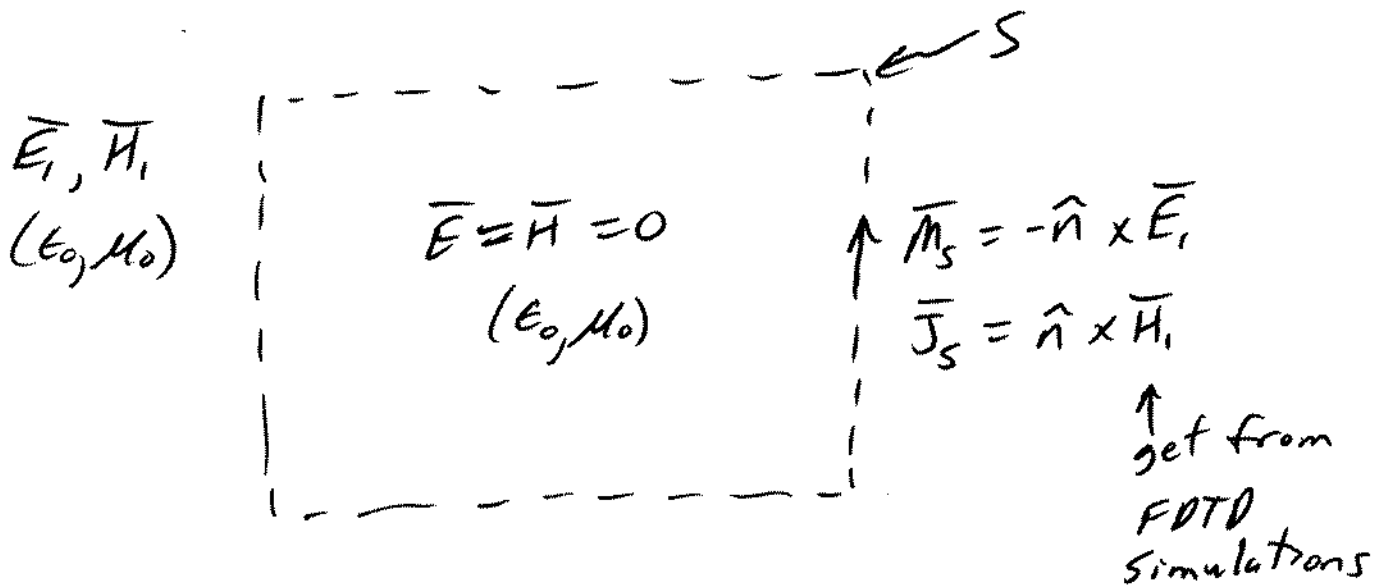
→ NUFF transforms based on the premise that if we know the tangential field components on a closed contour/surface that we can find the fields external to that surface w/out knowing what is going on in the interior



8.4 cont.

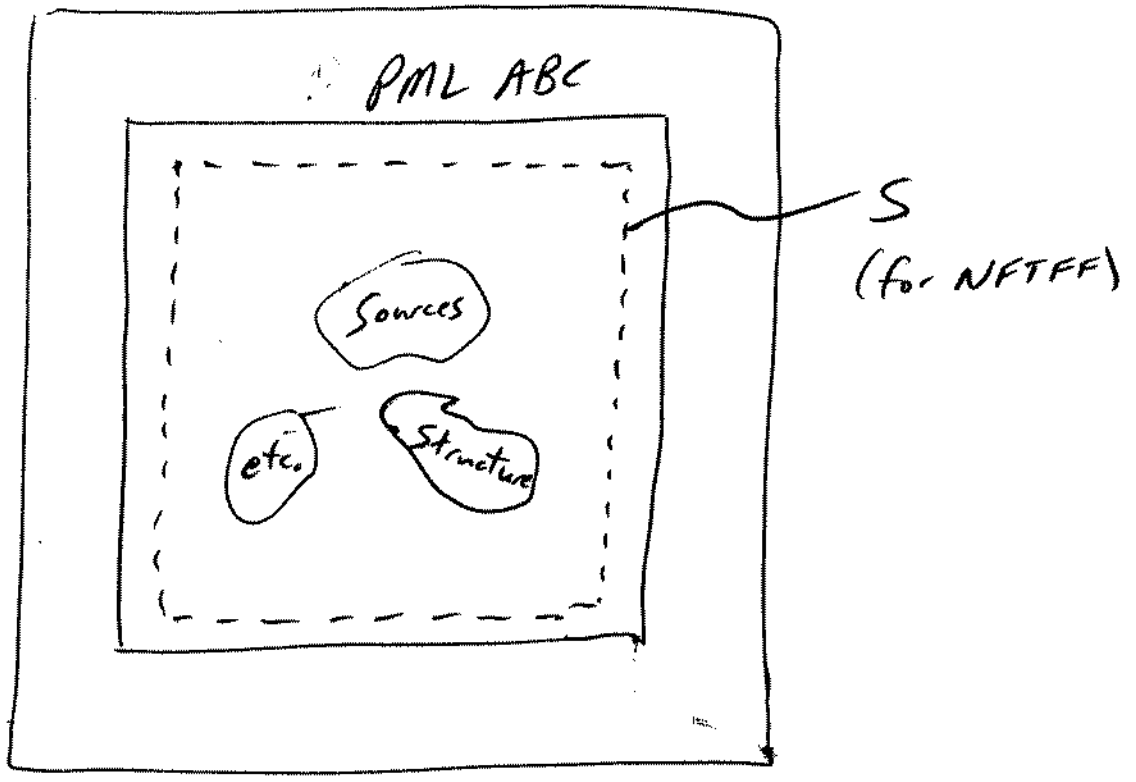
Note that the electric \bar{J}_S + magnetic \bar{M}_S surface current densities do NOT physically exist, but are selected so that $\bar{E}_i + \bar{H}_i$ outside S are the same.

Next, choose $\bar{E} + \bar{H}$ to be zero inside S (still want $\bar{E}_i + \bar{H}_i$ outside S). Then, our equivalent problem is



→ These \bar{M}_S + \bar{J}_S can be used to calculate the far-fields outside of S regardless of what sources +/or objects/structures are inside S

Typical modeling situation



8.6 Time-Domain Near-to-Far-Field Transformation 5

→ while we could store the tangential $\vec{E} + \vec{H}$ vs time for all points on the surface S , & then calculate $\vec{M}_S + \vec{J}_S$, & finally calculate $\vec{E}_{\text{off}}(t) + \vec{H}_{\text{off}}(t)$, it is more convenient to do the necessary calculations "on-the-fly" (i.e., part of regular time loop in the FDTD algorithm) keeping a running sum of the contributions of $\vec{E} + \vec{H}$ on the surface S at each time-step.

→ Start w/ Luebbers, Kunz, Schneider, & Hunsberger approach (give out paper) that draws on background EM material covered in Balanis' Advanced Engineering Electromagnetics & Antenna Theory texts (time-harmonic / phasor case)

In the far-field, the magnetic vector potential is

$$\vec{A} = \frac{\mu_0}{4\pi} \iint_S \vec{J}_S \frac{e^{-jkR}}{R} ds' \approx \frac{\mu_0 e^{-jkR}}{4\pi R} \vec{N}$$

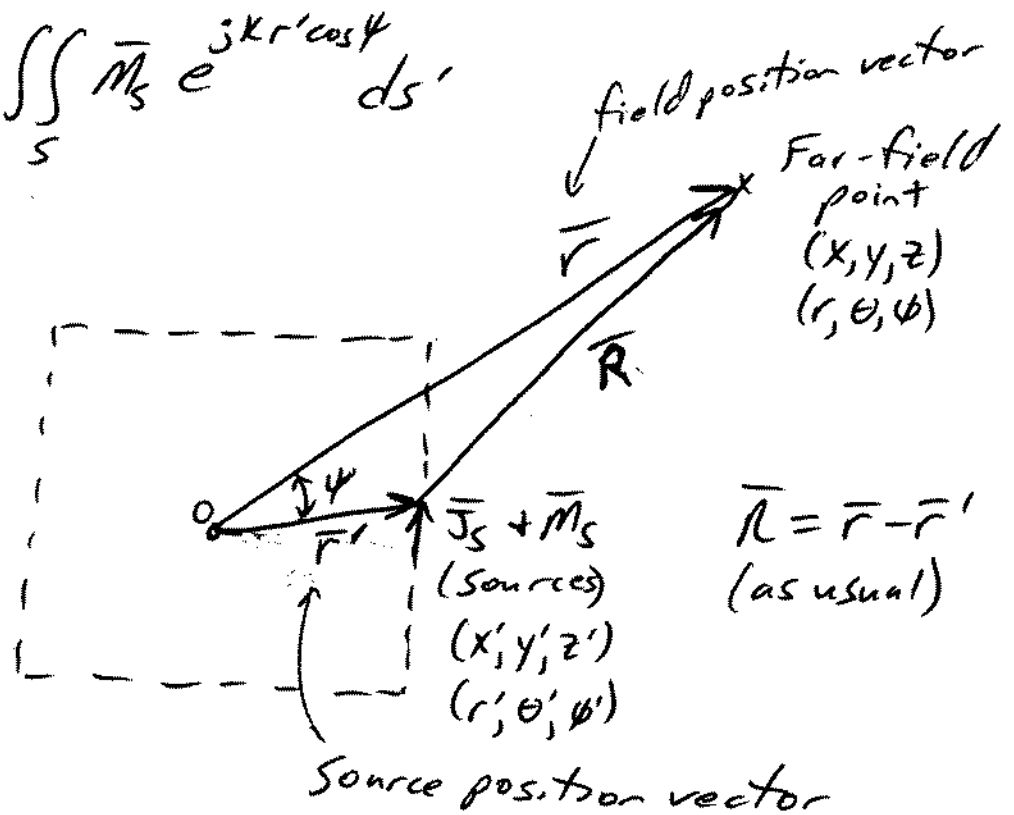
where

$$\vec{N} = \iint_S \vec{J}_S e^{jkR' \cos \psi} ds'$$

Similarly, the electric vector potential is

$$\vec{F} = \frac{\epsilon_0}{4\pi r} \iint_S \vec{M}_s \frac{e^{-jkR}}{R} ds' \approx \frac{\epsilon_0 e^{-jkr}}{4\pi r} \vec{L}$$

where $\vec{L} = \iint_S \vec{M}_s e^{jk r' \cos \psi} ds'$



$\psi \equiv$ angle between \vec{r} & \vec{r}'

$$r' \cos \psi = \vec{r}' \cdot \hat{a}_r \quad \hat{a}_r = \hat{a}_x \sin \theta \cos \phi + \hat{a}_y \sin \theta \sin \phi + \hat{a}_z \cos \theta$$

(by defn of dot product)

Balanis has shown that, in the far-field:

$$E_\theta = -j\omega A_\theta - j\omega \eta_0 F_\phi = -j\omega \frac{\mu_0 e^{-jkr}}{4\pi r} N_\theta - j\omega \eta_0 \frac{\epsilon_0 e^{-jkr}}{4\pi r} L_\phi$$

$$= \frac{-jke^{-jkr}}{4\pi r} (L_\phi + \eta_0 N_\theta) = \frac{-je^{-jkr}}{2\lambda_0 r} (L_\phi + \eta_0 N_\theta)$$

(8.38)

8.6 cont.

$$\begin{aligned}
 E_{\phi} &= -j\omega A_{\phi} + j\omega\eta_0 F_{\theta} = -j\omega \frac{\mu_0 e^{-jkr}}{4\pi r} N_{\phi} + j\omega\eta_0 \frac{\epsilon_0 e^{-jkr}}{4\pi r} L_{\theta} \\
 &= \frac{+j k \epsilon_0 e^{-jkr}}{4\pi r} (L_{\theta} - \eta_0 N_{\phi}) = \frac{j e^{-jkr}}{2\lambda_0 r} (L_{\theta} - \eta_0 N_{\phi}) \quad (8.39)
 \end{aligned}$$

If the magnetic fields are also desired

$$H_{\theta} = j \frac{\omega}{\eta_0} A_{\phi} - j\omega F_{\theta} = -\frac{E_{\phi}}{\eta_0}$$

$$H_{\phi} = -j \frac{\omega}{\eta_0} A_{\theta} - j\omega F_{\phi} = \frac{E_{\theta}}{\eta_0}$$

Compute

E_{θ} + E_{ϕ}

+ get H_{θ} + H_{ϕ}

by these relations

$E_r = H_r = 0$ in far-field

Next, define some new vector potentials

$$\bar{W} = \frac{j e^{-jkr}}{2\lambda_0 r} \bar{N} \quad (8.40) \quad + \quad \bar{U} = \frac{j e^{-jkr}}{2\lambda_0 r} \bar{L} \quad (8.41)$$

which allows us to write

$$E_{\theta} = -\eta_0 W_{\theta} - U_{\phi} \quad (8.42) \quad + \quad E_{\phi} = -\eta_0 W_{\phi} + U_{\theta} \quad (8.43)$$

Now, it is time to head back to the time-domain using inverse Fourier Transforms

$$\mathcal{F}^{-1}\{\bar{W}\} = \bar{w}$$

$$\frac{\partial(x(t))}{\partial t} \leftrightarrow j\omega X(\omega)$$

8.6 cont.

8

The inverse Fourier Transform of $\bar{W} + \bar{U}$ yields

$$\bar{W}(\bar{r}, t) = \frac{1}{4\pi rc} \frac{d}{dt} \left[\iint_S \bar{J}_s \left(t - \frac{r - \bar{r}' \cdot \hat{r}}{c} \right) ds' \right] \quad (8.44)$$

$$\bar{U}(\bar{r}, t) = \frac{1}{4\pi rc} \frac{d}{dt} \left[\iint_S \bar{M}_s \left(t - \frac{r - \bar{r}' \cdot \hat{r}}{c} \right) ds' \right] \quad (8.45)$$

and

$$\mathcal{E}_\theta(\bar{r}, t) = -\eta_0 \mathcal{W}_\theta(\bar{r}, t) - \mathcal{U}_\phi(\bar{r}, t) \quad (8.46)$$

$$\mathcal{E}_\phi(\bar{r}, t) = -\eta_0 \mathcal{W}_\phi(\bar{r}, t) + \mathcal{U}_\theta(\bar{r}, t) \quad (8.47)$$

$$\mathcal{H}_\theta(\bar{r}, t) = \frac{-\mathcal{E}_\phi(\bar{r}, t)}{\eta_0}$$

$$\mathcal{H}_\phi(\bar{r}, t) = \frac{\mathcal{E}_\theta(\bar{r}, t)}{\eta_0}$$

Now, the $\frac{r - \bar{r}' \cdot \hat{r}}{c}$ term represents the time delay in getting from some point on surface S to the far-field point

$$\tau_d = \frac{r - \bar{r}' \cdot \hat{r}}{c} = \frac{r - r' \cos \psi}{c}$$

Also, from our Surface Equivalence Theorem material

$$\bar{\mathbf{M}}_S = \mathcal{F}^{-1} \{ \bar{\mathbf{M}}_S = -\hat{\mathbf{n}} \times \bar{\mathbf{E}}_i \} = -\hat{\mathbf{n}} \times \bar{\mathbf{E}}_i(\bar{\mathbf{r}}', t) \leftarrow \text{No time-delay}$$

$$\bar{\mathbf{J}}_S = \mathcal{F}^{-1} \{ \bar{\mathbf{J}}_S = \hat{\mathbf{n}} \times \bar{\mathbf{H}}_i \} = \hat{\mathbf{n}} \times \bar{\mathbf{H}}_i(\bar{\mathbf{r}}', t) \checkmark$$

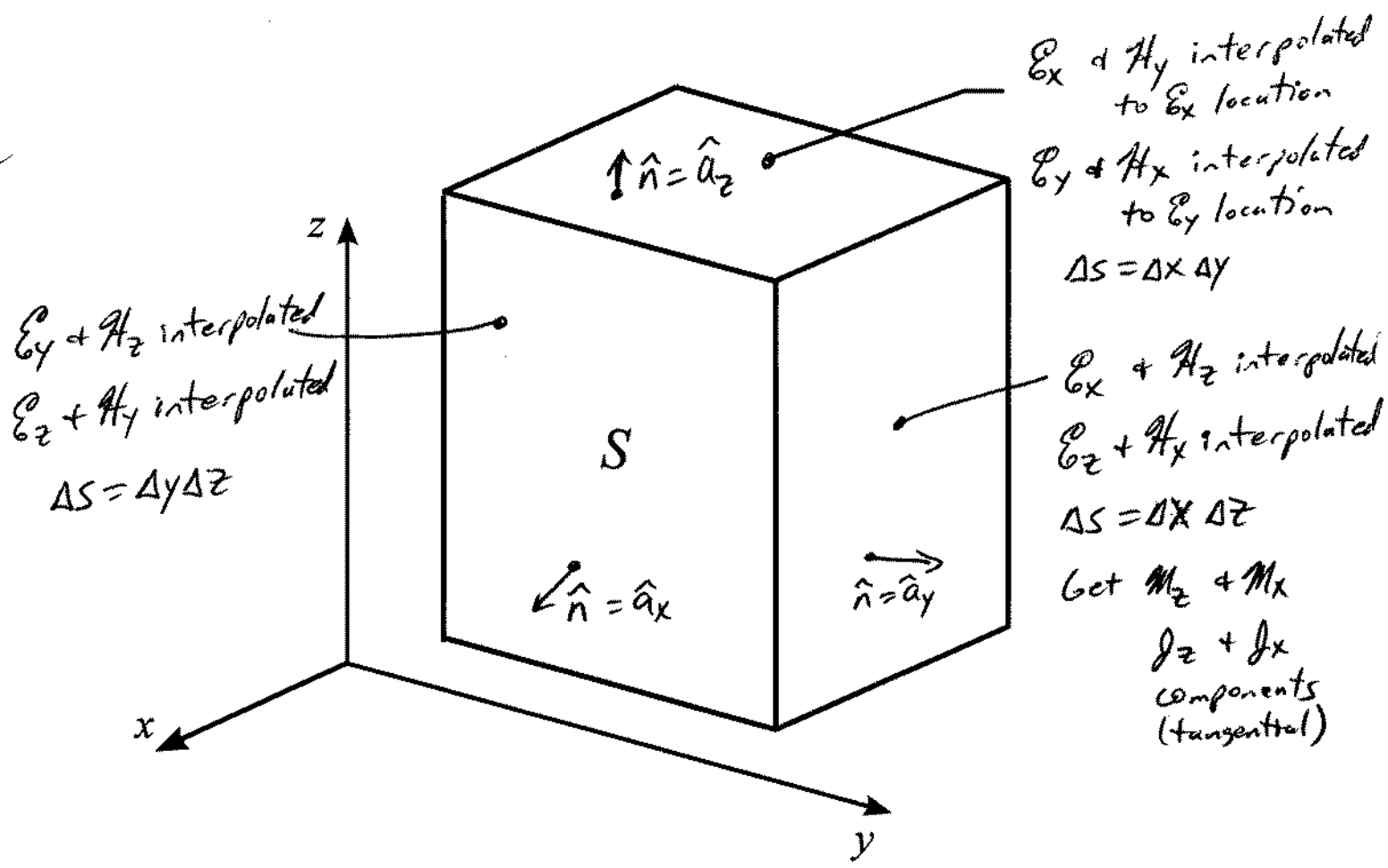
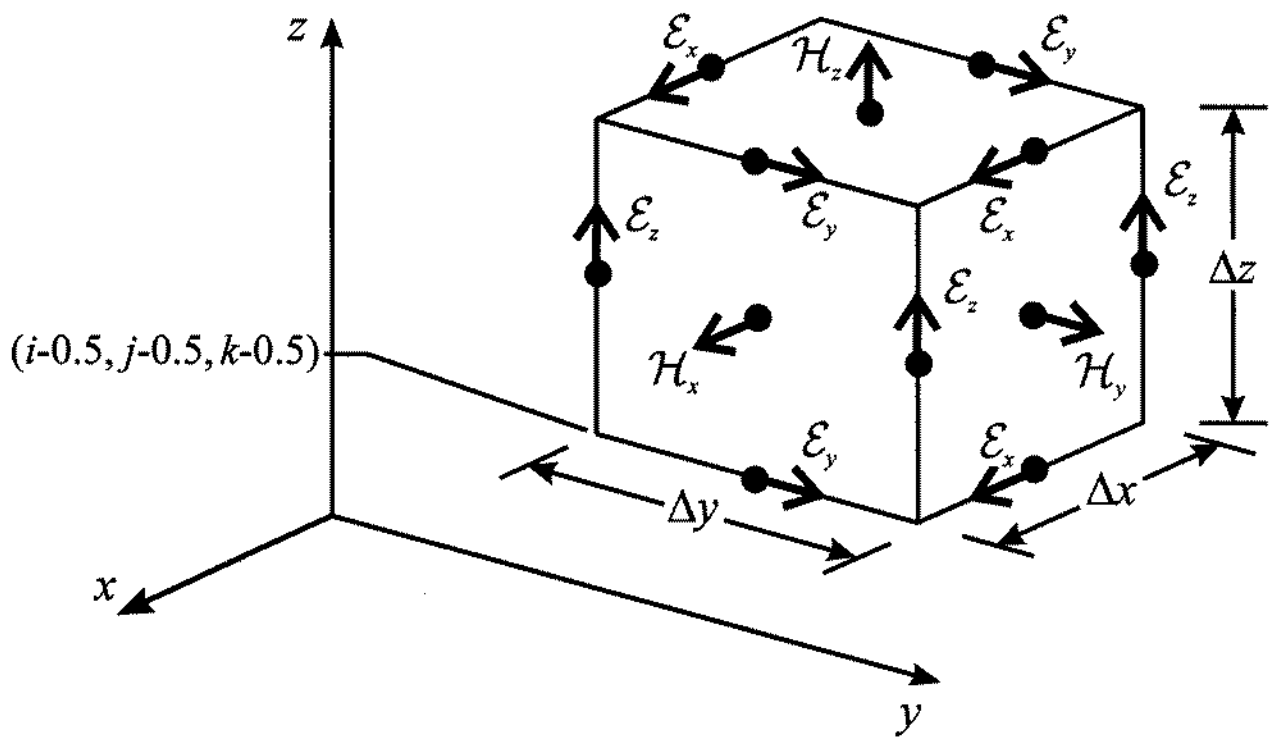
The big challenge is to implement (8.44) + (8.45) on the surface S (see figure on next page)

→ Need to evaluate (8.44) + (8.45) on each of six sides of S in Cartesian coordinates (i.e. $W_x(\bar{\mathbf{r}}, t)$, $W_y(\bar{\mathbf{r}}, t)$, $W_z(\bar{\mathbf{r}}, t)$, $U_x(\bar{\mathbf{r}}, t)$, $U_y(\bar{\mathbf{r}}, t)$, + $U_z(\bar{\mathbf{r}}, t)$) at each time-step (Keep a running sum)

→ Convert from Cartesian to spherical coordinates after finishing time-loop

i.e. Use $A_\theta = A_x \cos \theta \cos \phi + A_y \cos \theta \sin \phi - A_z \sin \theta$

$$A_\phi = -A_x \sin \phi + A_y \cos \phi$$



Surface S for 3D Cartesian FDTD model has six sides (e.g. Top at $z = z_{top}$, $x_{front} \leq x \leq x_{back}$, $y_{left} \leq y \leq y_{right}$)

8.6 cont.

To illustrate the process, let's look at the

right side of S ($y'=y_0$, $x_{\text{back}} \leq x' \leq x_{\text{front}}$, $z_{\text{bot}} \leq z' \leq z_{\text{top}}$)
 $\vec{r}' = x' \hat{a}_x + y_0 \hat{a}_y + z' \hat{a}_z$

First, what equivalent electric + magnetic surface currents are there?

E_x : $\vec{M}_{E_x} = -\hat{a}_y \times E_x \hat{a}_x = \hat{a}_z E_x(i, j+0.5, k+0.5)$

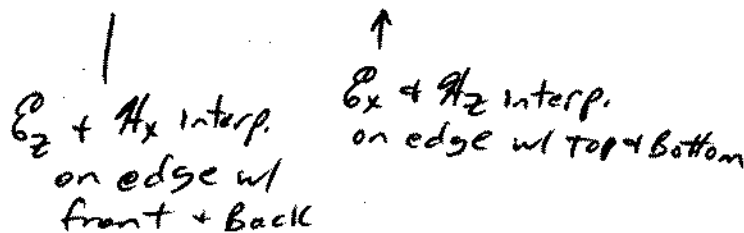
H_z : $\vec{J}_{H_z} = \hat{a}_y \times H_z \hat{a}_z = \hat{a}_x H_z$ ← interpolated left/right to E_x location
 $= \hat{a}_x \left(\frac{H_z(i, j+1, k+0.5) + H_z(i, j+k+0.5)}{2} \right)$

E_z : $\vec{M}_{E_z} = -\hat{a}_y \times E_z \hat{a}_z = -\hat{a}_x E_z(i+0.5, j+0.5, k)$

H_x : $\vec{J}_{H_x} = \hat{a}_y \times H_x \hat{a}_x = -\hat{a}_z H_x$ ← interpolated left/right to E_z location
 $= -\hat{a}_z \left(\frac{H_x(i+0.5, j+1, k) + H_x(i+0.5, j, k)}{2} \right)$

Now on the right face $ds' = dx' dz' \approx \Delta x \Delta z$

⇒ Be careful w/ field components on edges of S (e.g. $\frac{\Delta x}{2} \Delta z$ or $\Delta x \frac{\Delta z}{2}$ might be appropriate)



8.6 cont.

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Following some E_x components contribution (assume somewhere in middle of right face of S) we see that it will contribute to $\bar{U}(\bar{r}, t)$ as it generates $\bar{M}_{E_x} = \hat{a}_z E_x$. Specifically,

$$\Delta \bar{U} = \frac{1}{4\pi r c} \frac{\partial}{\partial t} \left[\hat{a}_z E_x(i, j+0.5, k+0.5) \Delta x \Delta z \right]$$

$$= \hat{a}_z \frac{\Delta x \Delta z}{4\pi r c} \frac{\partial E_x(i, j+0.5, k+0.5)}{\partial t}$$

$$\Delta U_z = \frac{\Delta x \Delta z}{4\pi r c} \frac{\partial E_x(i, j+0.5, k+0.5)}{\partial t}$$

Finish discretizing by doing a central-difference approx. to $\frac{\partial}{\partial t}$ about time $t = (n + \frac{1}{2}) \Delta t$

$$\Delta U_z = \frac{\Delta x \Delta z}{4\pi r c} \frac{E_x^{n+1}() - E_x^n()}{\Delta t}$$

Now, we need to "credit" this contribution to the overall $U_z(\bar{r}, t)$ function. To do so, we realize that U_z is saved at discrete times $t = n \Delta t$ and that we have a time delay going from the E_x location to the far-field. In terms of Δt , the delay is

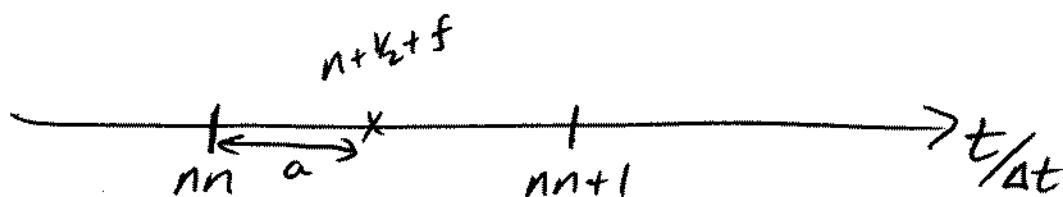
$$f = \frac{\tau_d}{\Delta t} = \frac{r - r' \cos \psi}{c \Delta t} \quad \text{input in terms of } E_x \text{ location}$$

Here $\vec{r}' = x' \hat{a}_x + y_0 \hat{a}_y + z' \hat{a}_z$ becomes

$$\vec{r}'_{\phi} = i \Delta x \hat{a}_x + (j+0.5) \Delta y \hat{a}_y + (k+0.5) \Delta z \hat{a}_z$$

$$r' \cos \psi = i \Delta x \sin \theta \cos \phi + (j+0.5) \Delta y \sin \theta \sin \phi + (k+0.5) \Delta z \cos \theta$$

So the time index to which ΔU_z must be credited is $n + \frac{1}{2} + f$. However, this sum is unlikely to be exactly an integer. Therefore, we split ΔU_z between the closest adjacent U_z temporal locations



where $nn = \text{INT}(n + \frac{1}{2} + f)$ ← rounds down to closest integer

$$a = (n + \frac{1}{2} + f) - nn \quad 0 \leq a \leq 1$$

$$U_z^{nn} \Big|_{\vec{r}} = U_z^{nn} \Big|_{\vec{r}} + (1-a) \Delta U_z \quad \leftarrow \text{smaller } a \Rightarrow \text{bigger contrib.}$$

$$U_z^{nn+1} \Big|_{\vec{r}} = U_z^{nn+1} \Big|_{\vec{r}} + a \Delta U_z \quad \leftarrow \text{bigger } a \Rightarrow \text{bigger contrib.}$$

running sum

8.6 cont.

Obviously, we need to ensure that the $U_z|_{\bar{r}}$ vector has enough memory locations M .

Let $S\Delta$ = Maximum diagonal distance on S
 fractional Δ in max diagonal dist.

& use the Courant Stability factor S_c to see

we need
$$M = N_{max} + \frac{S\Delta}{(A/S_c)} = N_{max} + \left(\frac{1}{S_c}\right) S$$

 time loop max. index # of time steps per Δ fractional Δ in max diagonal

e.g. $N_{max} = 1000$

max diagonal = 50Δ

$S = 0.5$

$$M = 1000 + \left(\frac{1}{0.5}\right) 50 = 1100 \text{ en/locations}$$

Note that we have NOT specified at which values of n we start & stop the indices (depends on value of r selected)

→ most of the time: $n_{min} = INT(\text{Min}(f))$

can be used or start @ $n=1$ by subtracting n_{min}

8.6 cont.

15

A similar process can be used for the other contributions to \bar{U} and for the contributions to \bar{W} .

Notes:

1) \bar{H} components are being interpolated onto S

2) \bar{H} components are shifted by $\Delta t/2$ relative to \bar{E} components

3) Careful w/ signs for equiv. currents.

After running your time loop, the

Six Cartesian components $W_x, W_y, W_z, U_x, U_y,$
 $+ U_z$ (at $\bar{r} + v_s n/t_n$) need to be used

~~converted~~ to find $W_\theta, W_\phi, U_\theta, + U_\phi$

by standard vector conversions

$$W_{\theta}(\vec{r}, t) = W_x \cos \theta \cos \phi + W_y \cos \theta \sin \phi - W_z \sin \theta$$

$$W_{\phi}(\vec{r}, t) = -W_x \sin \phi + W_y \cos \phi$$

$$U_{\theta}(\vec{r}, t) = U_x \cos \theta \cos \phi + U_y \cos \theta \sin \phi - U_z \sin \theta$$

$$U_{\phi}(\vec{r}, t) = -U_x \sin \phi + U_y \cos \phi$$

which can then be used to calculate

$$E_{\theta}, E_{\phi}, H_{\theta}, H_{\phi} \text{ in the far-field.}$$