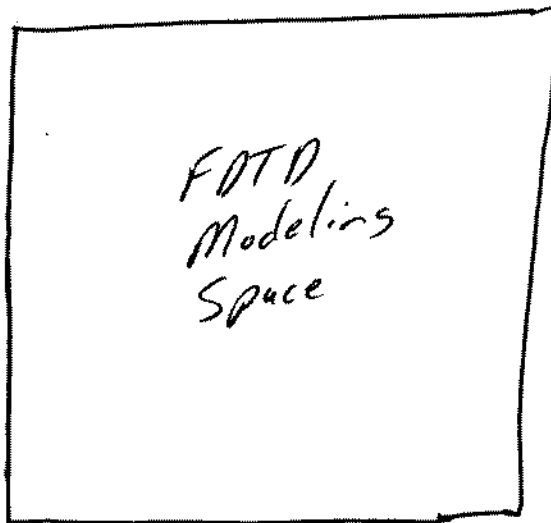


Chapter 6 Analytical Absorbing Boundary 1

Conditions

6.1 Intro

- For open problems (i.e. problems where waves could keep propagating indefinitely), we need a means of truncating the FDTD grid/lattice due to finite computational resources.



or Absorbing Boundary Condition (ABC)

or

Radiation Boundary Condition (RBC)

→ want only outward propagating waves thru an ABC or RBC (no reflections) $|\Gamma| \sim 0$

→ problem is that what to do w/ field components on edges of the FDTD modeling space where we don't have the needed components for central difference updates.

6.1 cont.

2

- the best ABCs can now yield $|\Gamma| \sim 10^{-4}$ to 10^{-6} (or -80dB to -120dB) so a dynamic range of $\sim 70\text{dB}$ + is achievable. (dynamic range is also limited by dispersion, ...)
- Analytical ABCs were the first to be developed, but have largely been replaced by perfectly matched layer (PML) ABC (next chapter).
- ABCs - some "material" absorbs or dissipates outward propagating waves
- RBCs - simulate the outward propagating wave continuing to propagate past the boundary



We'll just use the term ABC regardless of underlying technique.

Simple 1D ABC cont.

4

ex. $S=1$ (1) $\Delta z = \Delta z = v_p \Delta t$ \leftarrow Travel $1 \Delta z$ per Δt

$S=0.7$ $0.7 \Delta z = v_p \Delta t$ \leftarrow Travel $0.7 \Delta z$ per Δt

$S=0.5$ $0.5 \Delta z = v_p \Delta t \Rightarrow \Delta z = v_p (2 \Delta t)$ \leftarrow Travel $0.5 \Delta z$ per Δt

\rightarrow Using this knowledge and the knowledge that waves must propagate in the $\pm z$ -directions, we can say that the voltages at the two ends of the TIL are related to those inside the TIL by the Courant stability factor

e.g. At $z=0$, with $S=1$, ^{outward} wave must be in $-z$ -dir

$$V^{n+1}(0) = V^n(1) \quad \text{Since it takes the wave a single } \Delta t \text{ to travel a single } \Delta z$$

However, if $S=0.5$

$$V^{n+1}(0) = V^{n-1}(1) \quad \text{Since it takes a wave two } \Delta t \text{ to travel a single } \Delta z$$

Simple 1D ABC cont.

5

What about $V(k_{\max})$? Outward wave must be going in $+z$ -direction, so $V(k_{\max})$ depends on $V(k_{\max-1})$

e.g. $S=1$

$$V^{n+1}(k_{\max}) = V^n(k_{\max-1})$$

e.g. $S=1/3$

$$V^{n+1}(k_{\max}) = V^{n-2}(k_{\max-1})$$

This result extends to TEM waves in 2D grids (Hint!).

⇒ Makes it look as if the wave just keeps propagating off the mesh.

⇒ Works best if $S=1/n$, $n = \text{integer}$

⇒ Interpolation possible, but not as accurate

FDTD ABCs cont.

We'll examine the Merewether algorithm for an RBC to illustrate the technique.

→ First, we assume the field near the boundary S enclosing our problem space can be approximated by or as an outwardly propagating spherical wave with the functional form

$$\frac{f(t - \frac{R}{v_p})}{R}$$

v_p - velocity of wave

R - distance from source

ex.

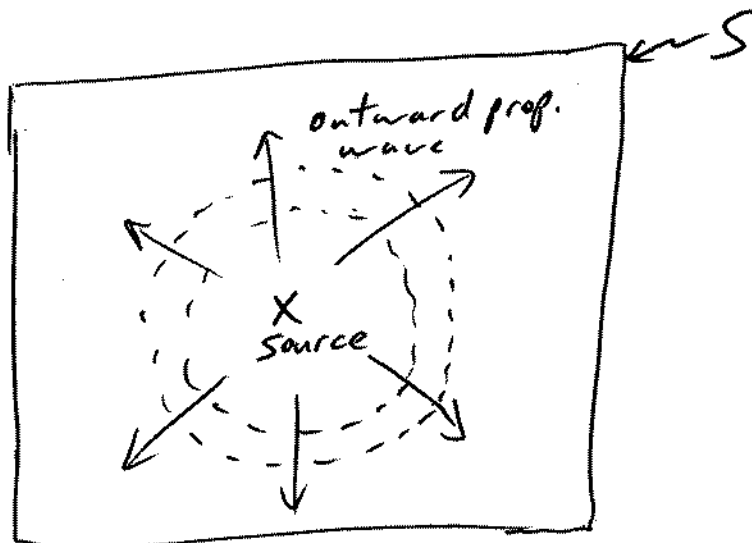


Fig. 1

→ Good approx. if you have a single/multiple source(s) near middle of modeling space and are in the far-field ($\sim R > \frac{20^2}{\lambda}$)

FDTD ABCs cont.

→ Second, we'll limit ourselves to a 2D

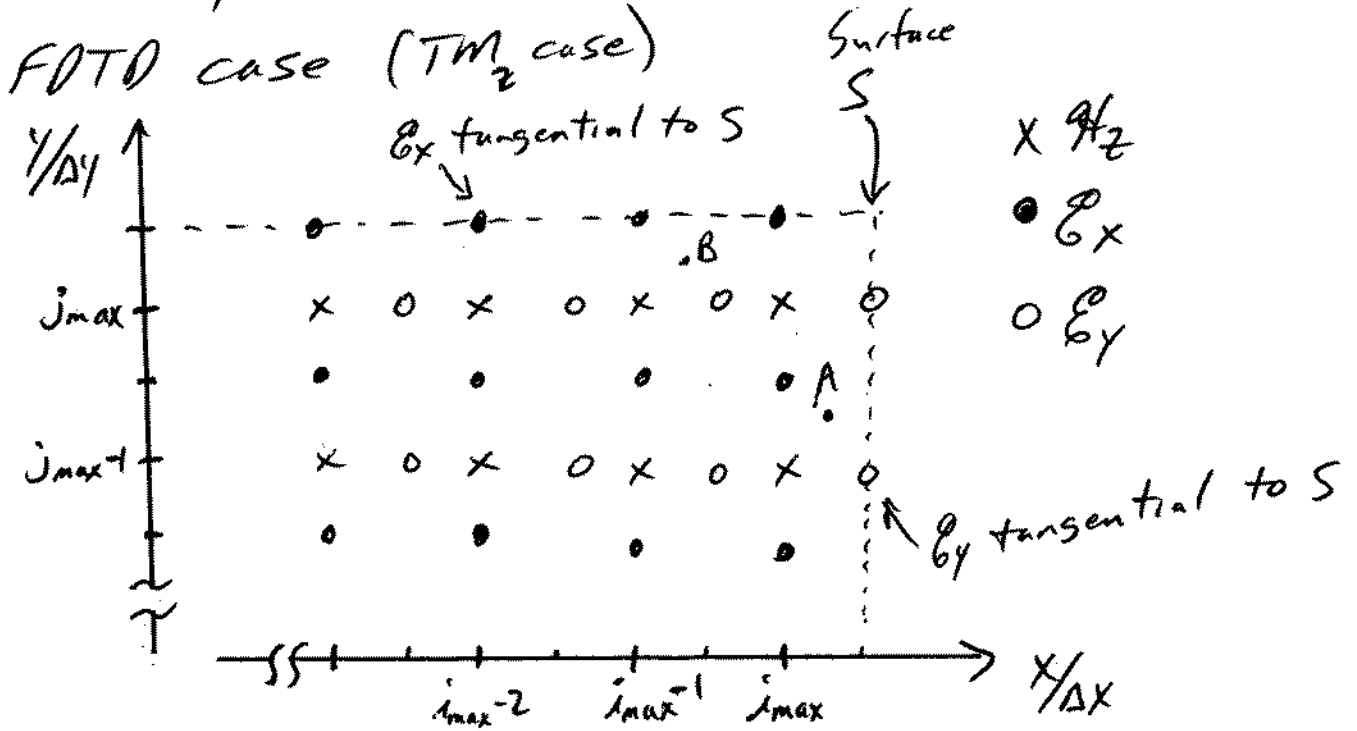


Fig. 2

→ Now, we'll want to predict the value of E_x or E_y that will arrive at the boundary S at time $t = (n+1)\Delta t$ using values of E_x or E_y at time $n\Delta t$.

From $\frac{f(t - \frac{R}{v_p})}{R}$, we get

$$E_x^{n+1}(i, j_{max} + 0.5) = \left(\frac{R - v_p \Delta t}{R} \right) E_x^n(\text{point B})$$

and

$$E_y^{n+1}(i_{max} + 0.5, j) = \left(\frac{R - v_p \Delta t}{R} \right) E_y^n(\text{point A})$$

FDTD ABCs cont.

B

The points A + B are illustrated in the close-up figures shown below.

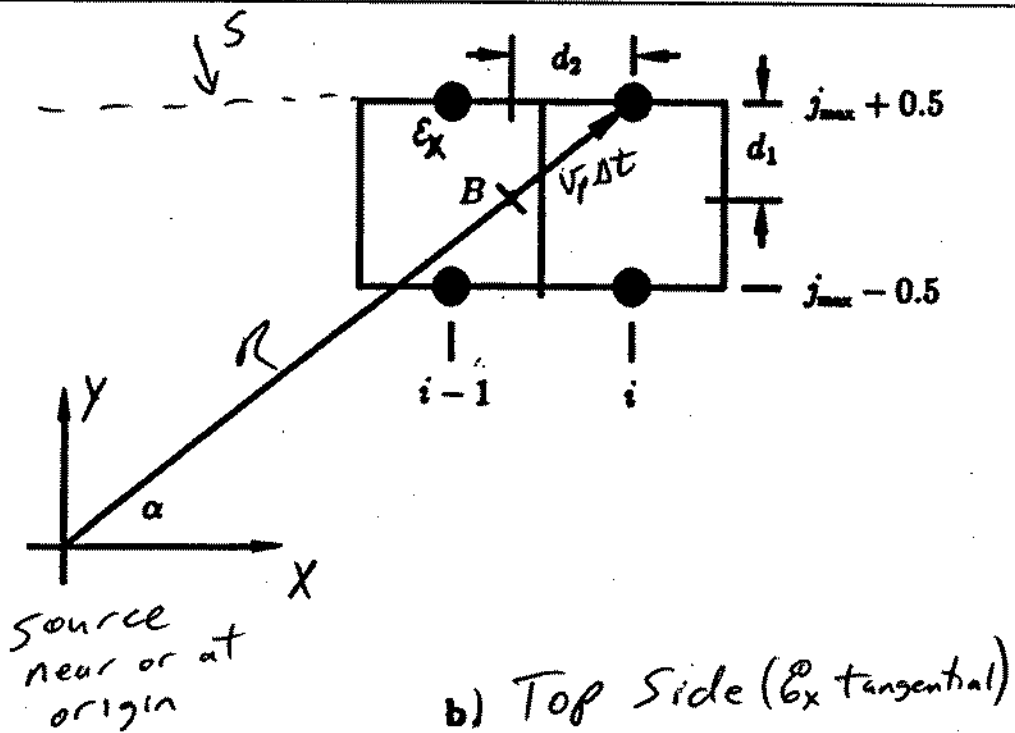
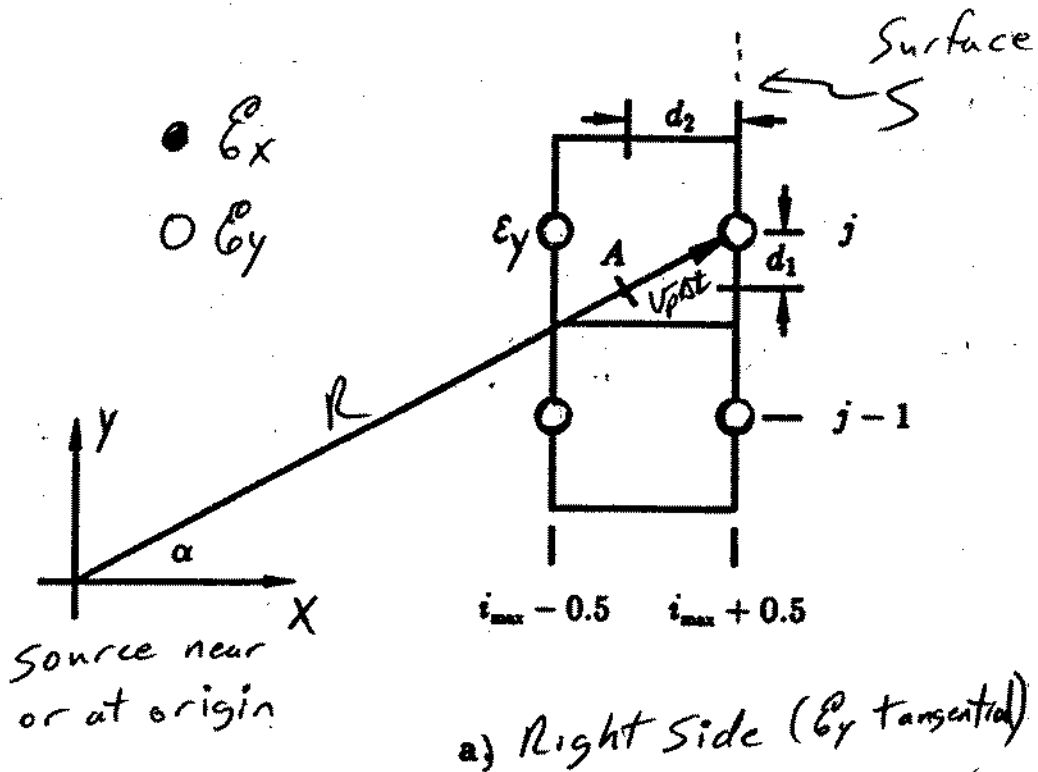


Fig. 3

On the right side (Fig. 3a), we see that, in general, no E_y value will be located at point A. Therefore, we will use bilinear interpolation to calculate $E_y(A)$ from available (in the grid) adjacent values.

$$\begin{aligned}
 E_y^n(A) \approx & \left(1 - \frac{d_1}{\Delta y}\right) \left(1 - \frac{d_2}{\Delta x}\right) E_y^n(i_{\max} + 0.5, j) \\
 & + \left(1 - \frac{d_1}{\Delta y}\right) \left(\frac{d_2}{\Delta x}\right) E_y^n(i_{\max} - 0.5, j) \\
 & + \left(\frac{d_1}{\Delta y}\right) \left(\frac{d_2}{\Delta x}\right) E_y^n(i_{\max} - 0.5, j - 1) \\
 & + \left(\frac{d_1}{\Delta y}\right) \left(1 - \frac{d_2}{\Delta x}\right) E_y^n(i_{\max} + 0.5, j - 1)
 \end{aligned}$$

where $d_1 = v_p \Delta t \sin \alpha$, $d_2 = v_p \Delta t \cos \alpha$, and α is the angle (wrt x) from the origin to point A, as shown. The distance R from the origin is easily calculated using Pythagorean's Thm @ each $E_y^{n+1}(i_{\max} + 0.5, j)$ location as

$$R = \sqrt{[(i_{\max} + 0.5)\Delta x]^2 + (j\Delta y)^2}$$

The angle $\alpha = \tan^{-1}\left(\frac{j\Delta y}{(i_{\max} + 0.5)\Delta x}\right)$.

Similarly, on the top boundary of S (see Fig 3 b), we see that, in general, no E_x value exists at point B . Again, using bilinear interpolation, we can calculate

$$\begin{aligned}
 E_x^n(B) \approx & \left(1 - \frac{d_1}{\Delta y}\right) \left(1 - \frac{d_2}{\Delta x}\right) E_x^n(i, j_{\max} + 0.5) \\
 & + \left(1 - \frac{d_1}{\Delta y}\right) \left(\frac{d_2}{\Delta x}\right) E_x^n(i-1, j_{\max} + 0.5) \\
 & + \left(\frac{d_1}{\Delta y}\right) \left(\frac{d_2}{\Delta x}\right) E_x^n(i-1, j_{\max} - 0.5) \\
 & + \left(\frac{d_1}{\Delta y}\right) \left(1 - \frac{d_2}{\Delta x}\right) E_x^n(i, j_{\max} - 0.5)
 \end{aligned}$$

where $d_1 = v_p \Delta t \sin \alpha$, $d_2 = v_p \Delta t \cos \alpha$, and α is the angle wrt the x -axis to point B from the origin as shown. Along the top surface of S at the $E_x^{n+1}(i, j_{\max} + 0.5)$ locations the distance R from the origin is

$$R = \sqrt{(i \Delta x)^2 + [(j_{\max} + 0.5) \Delta y]^2}$$

and

the angle $\alpha = \tan^{-1} \left(\frac{(j_{\max} + 0.5) \Delta y}{i \Delta x} \right)$