

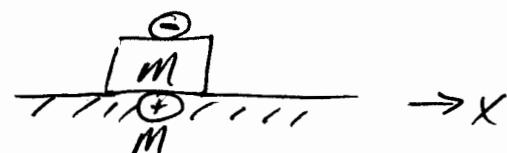
2.9 AC Variations in Materials

→ ϵ , μ , σ all vary w/ frequency

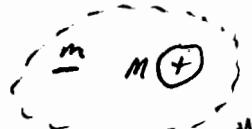
2.9.1 Complex Permittivity

→ Make analogy between polarizing an atom w/ a mechanical model of a mass, attached to a spring, being moved back-n-forth

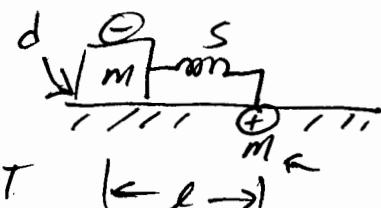
$$\bar{\epsilon}_a = 0$$



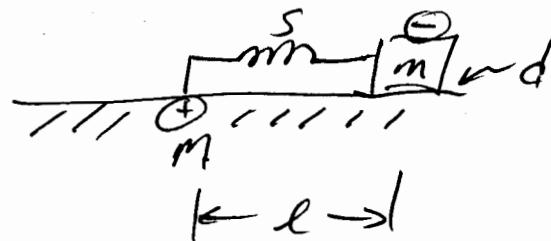
$$\bar{\epsilon}_a > 0$$



Nucleus stays put



$$\bar{\epsilon}_a < 0$$



$M \equiv$ mass of nucleus + Q

$m \equiv$ " " electrons - Q

$d \equiv$ damping/friction coefficient or takes power/energy to move charges

$s \equiv$ spring/tension coefficient or stored power/energy

$l \equiv$ displacement distance for centroids of nucleus & electrons

2.9.1 cont.

For a time-harmonic applied electric field, leads to a 2nd order ODE

$$M \frac{d^2 l}{dt^2} + d \frac{dl}{dt} + S l = Q E(t) = Q E_0 e^{j\omega t}$$

("ma" "dr" "sl" "driving force")

$$\frac{d^2 l}{dt^2} + 2\alpha \frac{dl}{dt} + \omega_0^2 l = \frac{Q}{m} E_0 e^{j\omega t}$$

where $\alpha = \frac{d}{2m}$ + $\omega_0 = \sqrt{\frac{S}{m}}$ ↑ very similar
to RLC circuits

If $\alpha > \omega_0 \rightarrow$ overdamped

$\alpha = \omega_0 \rightarrow$ critically damped

$\alpha < \omega_0 \rightarrow$ underdamped

complementary (Source-free) Transient	Two solns	↓ Particular soln
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+ $l_p(t) = l_0 e^{j\omega t}$

$l_c(t) = \begin{cases} \text{underdamped} \\ \text{critically damped} \\ \text{overdamped} \end{cases}$

where $l_0 = \frac{Q/m E_0}{(\omega_0^2 - \omega^2) + j\omega(d/m)}$

$$l(t) = l_c(t) + l_p(t)$$

↑
goes to zero as $t \rightarrow \infty$ as long as $d \neq 0$

Assuming an underdamped system ($\alpha < \omega_0$), we can determine the damped resonant frequency (natural frequency) to be

$$\omega_d = \sqrt{\omega_0^2 - \alpha^2} = \sqrt{\frac{S}{m} - \left(\frac{d}{2m}\right)^2}$$

2.9.1 cont.

If $d=0$ (no damping), $\omega_d = \omega_0 = \sqrt{S/m}$.

At steady-state (i.e., $\dot{E}_c(t) \rightarrow 0$), the time-varying polarization is

$$P = P(t) = N_e Q \dot{E}_c(t) = \frac{N_e \left(\frac{Q^2}{m} \right) E_0 e^{j\omega t}}{\left(\omega_0^2 - \omega^2 \right) + j\omega(d/m)}$$

dipoles
per unit
volume

Back in section 2.2, $\bar{D} = \epsilon_0 \bar{E}_a + \bar{P} = \epsilon_0 \bar{E}_a + \epsilon_0 S_c \bar{E}_a$

$$\text{Now } \frac{P}{\epsilon} = \frac{N_e \left(\frac{Q^2}{m} \right)}{\left(\omega_0^2 - \omega^2 \right) + j\omega(d/m)} \quad \text{or complex #!}$$

$$\epsilon = \epsilon_0 + \frac{|\bar{P}|}{|\bar{E}_a|}$$

and

$$\begin{aligned} \text{complex permittivity} &\equiv \dot{\epsilon} = \epsilon_0 + \frac{P}{\epsilon} = \epsilon_0 + \frac{N_e \left(\frac{Q^2}{m} \right)}{\left(\omega_0^2 - \omega^2 \right) + j\omega(d/m)} \\ &= \epsilon' - j\epsilon'' \end{aligned}$$

$$\begin{aligned} \text{relative complex permittivity} &\equiv \dot{\epsilon}_r = \frac{\dot{\epsilon}}{\epsilon_0} = \epsilon_r' - j\epsilon_r'' = 1 + \frac{\frac{N_e Q^2}{\epsilon_0 m}}{\left(\omega_0^2 - \omega^2 \right) + j\omega(d/m)} \end{aligned}$$

$$\text{w/ } \epsilon_r' = 1 + \frac{\frac{N_e Q^2}{\epsilon_0 m} (\omega_0^2 - \omega^2)}{(\omega_0^2 - \omega^2)^2 + (d\omega/m)^2}$$

$$\epsilon_r'' = \frac{N_e Q^2}{\epsilon_0 m} \left[\frac{\omega(d/m)}{(\omega_0^2 - \omega^2)^2 + (d\omega/m)^2} \right]$$

↑
multiply top
& bottom by
complex conj.
of denom.

2.9.1 cont.

define complex index of refraction $\hat{\epsilon}_r = \sqrt{\epsilon_r}$

$$\text{Note: If } d=0, \epsilon_r' = 1 + \frac{\frac{N_e Q^2}{\epsilon_0 m}}{\omega_0^2 - \omega^2} + \epsilon_r'' = 0$$

How does having $\hat{\epsilon} = \epsilon' - j\epsilon''$ impact Maxwell's Equations? Ampere's Law now becomes (phasor form)

$$\begin{aligned}\bar{\nabla} \times \bar{H} &= \bar{J}_i + \bar{J}_c + j\omega \hat{\epsilon} \bar{E} = \bar{J}_t \\ &= \bar{J}_i + \sigma_s \bar{E} + j\omega (\epsilon' - j\epsilon'') \bar{E} \\ &= \bar{J}_i + (\sigma_s + \omega \epsilon'') \bar{E} + j\omega \epsilon' \bar{E} \\ &= \bar{J}_i + \underbrace{\sigma_e \bar{E}}_{\text{eff. cond. current dens.}} + j\omega \epsilon' \bar{E} \text{ or effective displacement current density}\end{aligned}$$

$$\text{Equivalent conductivity} \equiv \sigma_e = \sigma_s + \omega \epsilon'' = \sigma_s + \sigma_a$$

$$\text{alternating field conductivity} \equiv \sigma_a = \omega \epsilon''$$

$$\text{static conductivity} \equiv \sigma_s$$

Some materials have modest σ_s and larger σ_a (think microwave oven)

2.9.1 cont.

We can express the total current density

$$\begin{aligned}\bar{J}_t &= \bar{J}_i + \sigma_e \bar{E} + j\omega e' \bar{E} = \bar{J}_i + j\omega e' \left(1 - j \frac{\sigma_e}{\omega e'}\right) \bar{E} \\ &= \bar{J}_i + j\omega e' (1 - j \tan \delta_e) \bar{E}\end{aligned}$$

Define

$$\begin{aligned}\text{effective loss tangent} &\equiv \tan \delta_e = \frac{\sigma_e}{\omega e'} = \frac{\sigma_s}{\omega e'} + \frac{\sigma_a}{\omega e'} \\ &= \frac{\sigma_s}{\omega e'} + \frac{\epsilon''}{\epsilon'} = \tan \delta_s + \tan \delta_a\end{aligned}$$

$$\begin{aligned}\text{static loss tangent} &\equiv \tan \delta_s = \frac{\sigma_s}{\omega e'}\end{aligned}$$

$$\begin{aligned}\text{alternating loss tangent} &\equiv \tan \delta_a = \frac{\epsilon''}{\epsilon'}\end{aligned}$$

\Rightarrow Manufacturers of PCBs and TLs when giving conductivity σ , loss tangent $\tan \delta$, and relative permittivity ϵ_r at selected frequencies typically mean σ_e , $\tan \delta_e$, and ϵ_r' . See Table 2-5.

\Rightarrow Look at the effective conduction + displacement current densities on complex plane

$$\begin{aligned}\bar{J}_{cd} &= \bar{J}_{cc} + \bar{J}_{de} \\ &= j\omega e' \left(1 - j \frac{\sigma_e}{\omega e'}\right) \bar{E} \\ \begin{array}{c} \text{Diagram: A right-angled triangle in the complex plane. The horizontal axis is labeled } \bar{J}_{cc} = \sigma_e \bar{E}. \text{ The vertical axis is labeled } \bar{J}_{de} = j\omega e' \bar{E}. \text{ The hypotenuse is labeled } \bar{J}_{cd} = j\omega e' \bar{E}. \text{ The angle between the horizontal axis and the hypotenuse is labeled } \delta_e. \end{array} \\ &\Rightarrow \tan \delta_e = \frac{\sigma_e}{\omega e'}\end{aligned}$$

TABLE 2-5 Dielectric constants and loss tangents of typical dielectric materials

Material	ϵ'_r	$\tan \delta$
Air	1.0006	
Alcohol (ethyl)	25	0.1
Aluminum oxide	8.8	6×10^{-4}
Bakelite	4.74	22×10^{-3}
Carbon dioxide	1.001	
Germanium	16	
Glass	4–7	1×10^{-3}
Ice	4.2	0.1
Mica	5.4	6×10^{-4}
Nylon	3.5	2×10^{-2}
Paper	3	8×10^{-3}
Plexiglas	3.45	4×10^{-2}
Polystyrene	2.56	5×10^{-5}
Porcelain	6	14×10^{-3}
Pyrex glass	4	6×10^{-4}
Quartz (fused)	3.8	7.5×10^{-4}
Rubber	2.5–3	2×10^{-3}
Silica (fused)	3.8	7.5×10^{-4}
Silicon	11.8	
Snow	3.3	0.5
Sodium chloride	5.9	1×10^{-4}
Soil (dry)	2.8	7×10^{-2}
Styrofoam	1.03	1×10^{-4}
Teflon	2.1	3×10^{-4}
Titanium dioxide	100	15×10^{-4}
Water (distilled)	80	4×10^{-2}
Water (sea)	81	4.64
Wood (dry)	1.5–4	1×10^{-2}

2.9.1 cont.

Ex. Rogers Corporation RO4003C hydrocarbon/ceramic laminate substrate. From the datasheet

$$\rho_s = 1.7 \times 10^{10} \quad \Rightarrow \quad \sigma_s = 5.88 \times 10^{-15} \text{ S/m}$$

$$\tan \delta = \tan \delta_e = 0.0021 \quad @ 2.5 \text{ GHz}$$

$$= 0.0027 \quad @ 10 \text{ GHz}$$

$$\epsilon_{re} = \epsilon_r' = 3.67 \quad @ 2.5 \text{ GHz}$$

$$= 3.651 \quad @ 10 \text{ GHz}$$

Find the effective conductivity, imaginary part of $\hat{\epsilon}$, and $\hat{\epsilon}_r$, the complex permittivity and relative permittivity.

@ 2.5 GHz $\sigma_e = \omega \epsilon' \tan \delta_e = 2\pi(2.5 \times 10^9) 3.67 \epsilon_0 (0.0021)$

$$\underline{\sigma_e = 0.001072 \text{ S/m} = 1.072 \text{ mS/m}}$$

$$\epsilon'' = \frac{\sigma_e - \sigma_s}{\omega} = \frac{0.001072 - 5.88 \times 10^{-15}}{2\pi(2.5 \times 10^9)} = \underline{6.824 \times 10^{-14} \text{ F/m}}$$

$$\epsilon_r'' = \frac{\epsilon''}{\epsilon_0} = 0.007707 \quad (\text{pretty small compared to } \epsilon_r' = 3.67)$$

@ 10 GHz $\sigma_e = 2\pi(10 \times 10^9) 3.651 (8.8542 \times 10^{-12}) 0.0027$

$$\underline{\sigma_e = 0.005484 \text{ S/m} = 5.484 \text{ mS/m}}$$

$$\epsilon'' = \frac{\sigma_e - \sigma_s}{\omega} = \frac{0.005484 - 5.88 \times 10^{-15}}{2\pi(10 \times 10^9)} = \underline{8.7282 \times 10^{-14} \text{ F/m}}$$

$$\epsilon_r'' = \frac{\epsilon''}{\epsilon_0} = 0.009858 \quad (\text{small compared to } \epsilon_r' = 3.651)$$

Consider the extremes

1. Good dielectrics ($\tan \delta_e = \frac{\sigma_e}{\omega \epsilon'} \ll 1$)

$$\bar{J}_{cd} \approx j\omega \epsilon' \bar{E} \quad (\text{nearly all displacement current density})$$

2. Good conductors ($\tan \delta_e = \frac{\sigma_e}{\omega \epsilon'} \gg 1$)

$$\bar{J}_{cd} \approx \sigma_e \bar{E} \quad (\text{nearly all conduction current density})$$

Going back to section 2.2, it was mentioned that electric polarization could occur due to different mechanisms: 1) dipole/orientational, 2) ionic/molecular, & 3) electronic. Depending on the material, 1, 2, or 3 of these mechanisms may apply and typically would occur @ different frequencies/frequency ranges.

Writing the phasor polarization vector as a function of frequency

$$\bar{P}(\omega) = \epsilon_0 \chi_e(\omega) \bar{E}_a(\omega)$$

we'll note that the electric susceptibility is a function of frequency. Further, $\chi_e(\omega)$ must be complex since ϵ is complex.

$$\begin{aligned} X_e(\omega) &= X_e'(\omega) - j X_e''(\omega) \\ &= \left[X_{ed}'(\omega) + X_{ei}'(\omega) + X_{ee}'(\omega) \right] - j \left[X_{es}''(\omega) + X_{ei}''(\omega) + X_{ee}''(\omega) \right] \\ &\quad \begin{matrix} \uparrow & \uparrow & \uparrow \\ \text{dipole} & \text{ionic} & \text{electronic} \end{matrix} \quad \begin{matrix} \uparrow & \uparrow & \uparrow \\ \text{dipole} & \text{ionic} & \text{electronic} \end{matrix} \end{aligned}$$

In general, $X_e'(\omega) = X_e'(-\omega)$ real part is even

$$X_e''(-\omega) = -X_e''(\omega) \text{ imag. part is odd}$$

Figures 2-18 + 2-19 show general samples as to how $\epsilon_e + \epsilon_r$ can vary with frequency

→ Note, both $\epsilon_e'' + \epsilon_r''$ peak @/near resonant frequencies while $\epsilon_e' + \epsilon_r'$ dip (negative slope), called anomalous dispersion.

→ Other than near resonant frequencies $|\epsilon_r| + \epsilon_r'$ exhibit positive slopes, i.e., normal dispersion.

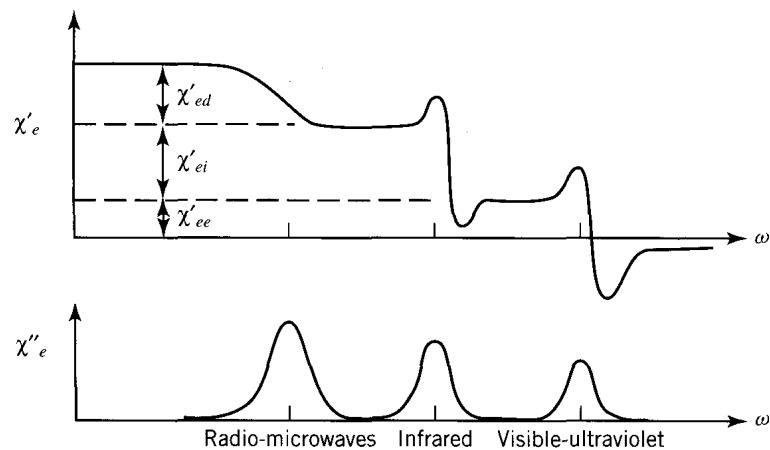


Figure 2-18 Electric susceptibility (real and imaginary) variations as a function of frequency for a typical dielectric.

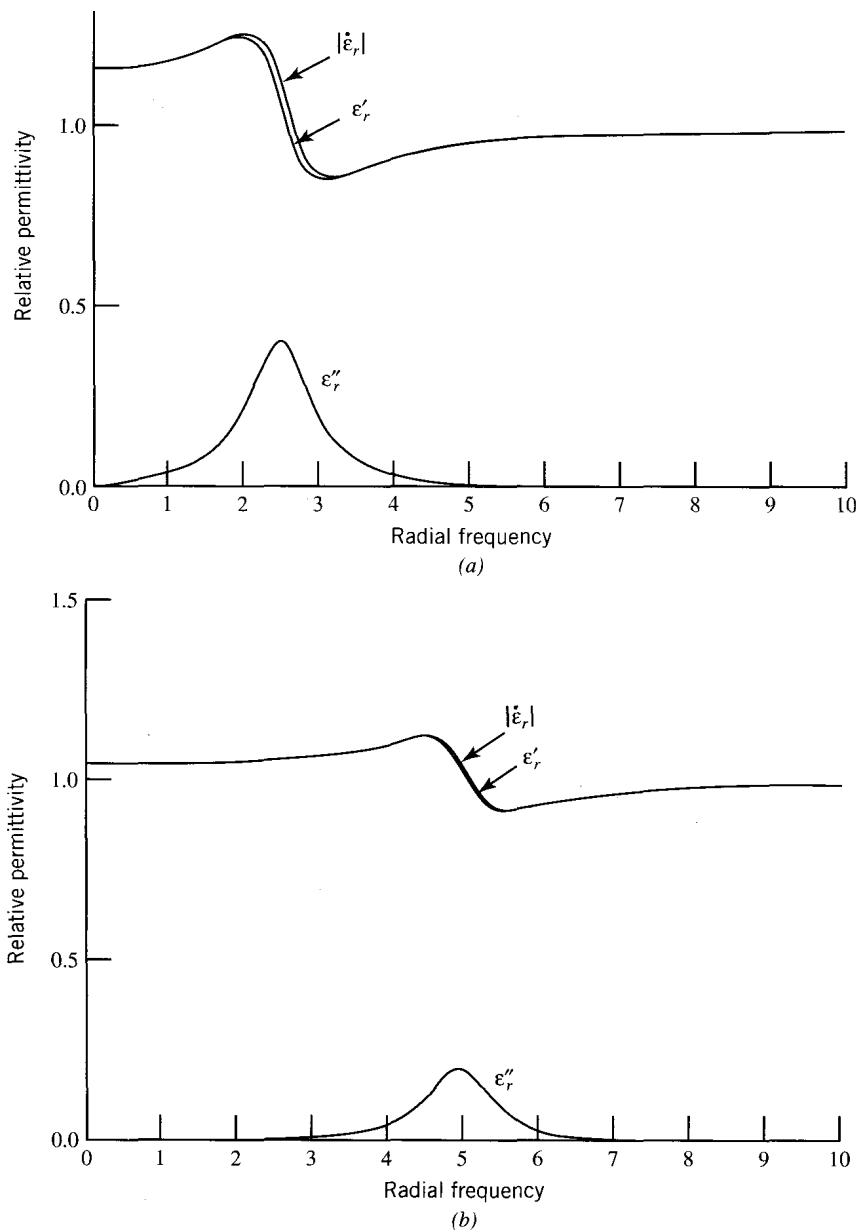


Figure 2-19 Typical frequency variations of real and imaginary parts of relative permittivity of dielectrics.
 (a) $N_e Q^2 / \epsilon_0 m = 1$, $d/m = 1$, $\alpha/\omega_0 = 1/5$, $\omega_0 = 2.5$. (b) $N_e Q^2 / \epsilon_0 m = 1$, $d/m = 1$, $\alpha/\omega_0 = 1/10$, $\omega_0 = 5$.

2.9.1 cont.

For our mechanical analogy, we assumed a single resonant frequency. However, actual material can have multiple resonances due to different mechanisms. To allow for this possibility, or ρ resonances, let-

$$\frac{\rho}{\epsilon} = \sum_{s=1}^{\rho} \frac{N_e \frac{Q^2}{m}}{(\omega_s^2 - \omega^2) + j \frac{\omega d}{m}}$$

$$\dot{\epsilon} = \epsilon' - j\epsilon'' = \epsilon_0 + \sum_{s=1}^{\rho} \frac{N_e \frac{Q^2}{m}}{(\omega_s^2 - \omega^2) + j \frac{\omega d}{m}}$$

$$\dot{\epsilon}_r = \epsilon_r' - j\epsilon_r'' = 1 + \sum_{s=1}^{\rho} \frac{N_e \frac{Q^2}{\epsilon_0 m}}{(\omega_s^2 - \omega^2) + j \frac{\omega d}{m}}$$

$$\epsilon_r' = 1 + \sum_{s=1}^{\rho} \frac{\frac{N_e Q^2}{\epsilon_0 m} (\omega_s^2 - \omega^2)}{(\omega_s^2 - \omega^2)^2 + (\frac{\omega d}{m})^2}$$

$$\epsilon_r'' = \sum_{s=1}^{\rho} \frac{N_e Q^2}{\epsilon_0 m} \frac{\omega d/m}{(\omega_s^2 - \omega^2)^2 + (\omega d/m)^2}$$

$\Rightarrow \epsilon_r'$ & ϵ_r'' are related by the Kramers-Kronig equations

$$\epsilon_r'(\omega) = 1 + \frac{2}{\pi} \int_0^\infty \frac{\omega' \epsilon_r''(\omega')}{\omega'^2 - \omega^2} d\omega'$$

$$\epsilon_r''(\omega) = \frac{2\omega}{\pi} \int_0^\infty \frac{1 - \epsilon_r'(\omega')}{\omega'^2 - \omega^2} d\omega'$$

2.9.1 cont.

For many materials, the Debye equation can be used to find the complex relative permittivity (as well as $\sigma_e(\omega)$)

$$\dot{\epsilon}_r(\omega) = \epsilon'_{r\infty} + \frac{\epsilon'_{rs} - \epsilon'_{r\infty}}{1 + j\omega\tau_e}$$

where

$$\begin{aligned} \text{new relaxation} \\ \text{time constant} \equiv \tau_e &= \gamma \frac{\epsilon'_{rs} + 2}{\epsilon'_{r\infty} + 2} \end{aligned}$$

$$\epsilon'_r(\omega) = \epsilon'_{r\infty} + \frac{\epsilon'_{rs} - \epsilon'_{r\infty}}{1 + (\omega\tau_e)^2} \Rightarrow \omega_e = \frac{1}{\tau_e}$$

$$\epsilon''_r(\omega) = \frac{(\epsilon'_{rs} - \epsilon'_{r\infty})\omega\tau_e}{1 + (\omega\tau_e)^2} \underbrace{\text{relaxation frequencies}}_{f_c = \frac{1}{2\pi\tau_e}}$$

provided that the following are known

$\epsilon'_{rs} \equiv$ static relative permittivity ($\omega=0$)

$\epsilon'_{r\infty} \equiv$ relative permittivity as $\omega \rightarrow \infty$

τ_e or γ

$\sigma_0 \equiv$ static conductivity (S/m)

\Rightarrow This is good for a single resonance.

More terms can be added to account for multiple resonances.