

# Design of Yagi-Uda Antennas

## Typical characteristics/parameters:

- $4.3 \text{ dBi} \leq \text{Directivity (Gain)} \leq 19 \text{ dBi}$
- $15 \ \Omega \leq \text{Input Impedance} \leq 70 \ \Omega$  (w/out feed)
- Bandwidth  $\leq 2\%$  (about center frequency)
- Frequency bands where Yagi-Uda antennas are typically utilized include: HF (3-30 MHz), VHF (30-300 MHz), and UHF (300-1000 MHz)
- Transmission line feeds:
  - Coaxial using a Gamma match, Omega match, or modified Gamma match at the driven element.
  - Twin-lead using a T-match at the driven element or with a folded dipole as the driven element.
- Pre-determined designs are available.
- Also, computer-aided design tools, which allow the antenna to be optimized for particular performance characteristics, are available. For example, several shareware programs that use NEC (Numerical Electromagnetics Code), a Method of Moments program, as an engine are freely available on the internet.

# Yagi-Uda Antenna Design Procedure

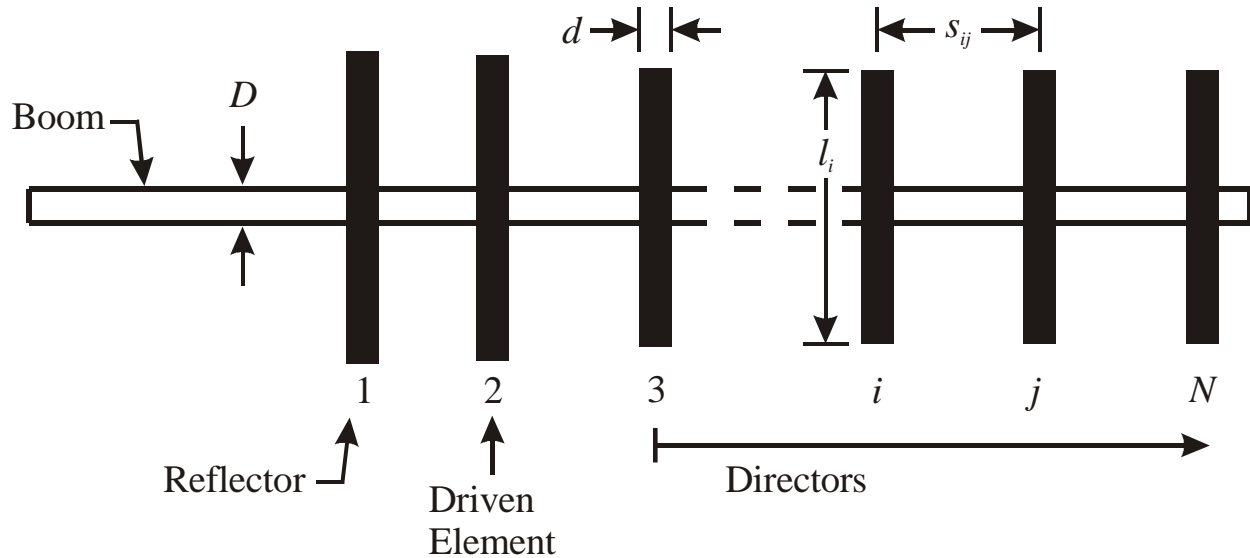


Figure 1 Yagi-Uda Antenna Layout

## Notes:

- Design procedure based on: P.P. Viezbicke, "Yagi Antenna Design," NBS Technical Note 688, U.S. Department of Commerce/National Bureau of Standards, December 1976.
- This design procedure utilizes a table (Table 10.6) and two figures (Fig. 10.25 & 10.26) taken from the NBS Tech. Note.
- The directivities given by Table 10.6 are in dBd,  $\text{dBi} = \text{dBd} + 2.15 \text{ dB}$ .
- The design(s) described by Table 10.6 assume that the antenna uses a certain diameter for the elements and has a dielectric boom. If a different element diameter is used, element length adjustments are made using Figure 10.25. If a metal boom is used, element length adjustments are made using Figure 10.26.

## **Design Steps:**

1. Select or specify design parameters:
  - a. Desired directivity (gain)
    - Six values, ranging from 9.25 to 16.35 dBi, are available in Table 10.6.
  - b. Design Frequency (center frequency of 1-2% bandwidth)
  - c. Desired input impedance  $R_0$  (real) based on desired or given transmission line.
2. Select diameter  $d$  of elements and diameter  $D$  of metallic supporting boom (optional, only necessary if a metallic boom is to be used) based on mechanical considerations such as strength and/or rigidity and parts availability.
3. Calculate wavelength at design frequency ( $\lambda = c/f$ ). Use this to calculate  $s_{12}$  (reflector-driven element spacing) and  $s_{ij}$  [driven-director & director-director spacing(s)] using Table 10.6 values.
4. Calculate  $d / \lambda$ . Is  $0.001 \leq d / \lambda \leq 0.04$ ? If not, go to step 2 and reconsider selection of diameter of elements  $d$ .
5. If a metal boom is used (otherwise, go to next step), calculate  $D / \lambda$ . Is  $0.001 \leq D / \lambda \leq 0.04$ ? If not, go to step 2 and reconsider selection of diameter of boom  $D$ .

**Table 10.6** OPTIMIZED UNCOMPENSATED LENGTHS OF PARASITIC ELEMENTS FOR YAGI-UDA ANTENNAS OF SIX DIFFERENT LENGTHS

| $d/\lambda = 0.0085$<br>$s_{12} = 0.2\lambda$  |          | LENGTH OF YAGI-UDA (IN WAVELENGTHS) |       |       |       |       |       |
|--|----------|-------------------------------------|-------|-------|-------|-------|-------|
|  |          | 0.4                                 | 0.8   | 1.20  | 2.2   | 3.2   | 4.2   |
| LENGTH OF REFLECTOR ( $l_1/\lambda$ )          |          | 0.482                               | 0.482 | 0.482 | 0.482 | 0.482 | 0.475 |
| LENGTH OF DIRECTORS, $\lambda$                 | $l_3$    | 0.442                               | 0.428 | 0.428 | 0.432 | 0.428 | 0.424 |
|  | $l_4$    |                                     | 0.424 | 0.420 | 0.415 | 0.420 | 0.424 |
|  | $l_5$    |                                     | 0.428 | 0.420 | 0.407 | 0.407 | 0.420 |
|  | $l_6$    |                                     |       | 0.428 | 0.398 | 0.398 | 0.407 |
|  | $l_7$    |                                     |       |       | 0.390 | 0.394 | 0.403 |
|  | $l_8$    |                                     |       |       | 0.390 | 0.390 | 0.398 |
|  | $l_9$    |                                     |       |       | 0.390 | 0.386 | 0.394 |
|  | $l_{10}$ |                                     |       |       | 0.390 | 0.386 | 0.390 |
|  | $l_{11}$ |                                     |       |       | 0.398 | 0.386 | 0.390 |
|  | $l_{12}$ |                                     |       |       | 0.407 | 0.386 | 0.390 |
|  | $l_{13}$ |                                     |       |       |       | 0.386 | 0.390 |
|  | $l_{14}$ |                                     |       |       |       | 0.386 | 0.390 |
|  | $l_{15}$ |                                     |       |       |       | 0.386 | 0.390 |
|  | $l_{16}$ |                                     |       |       |       | 0.386 |       |
| $l_{17}$                                       |          |                                     |       |       | 0.386 |       |       |
| SPACING BETWEEN DIRECTORS ( $s_{ij}/\lambda$ ) |          | 0.20                                | 0.20  | 0.25  | 0.20  | 0.20  | 0.308 |
| DIRECTIVITY RELATIVE TO HALF-WAVE DIPOLE (dB)  |          | 7.1                                 | 9.2   | 10.2  | 12.25 | 13.4  | 14.2  |
| DESIGN CURVE (SEE FIGURE 10.25)                |          | (A)                                 | (B)   | (B)   | (C)   | (B)   | (D)   |

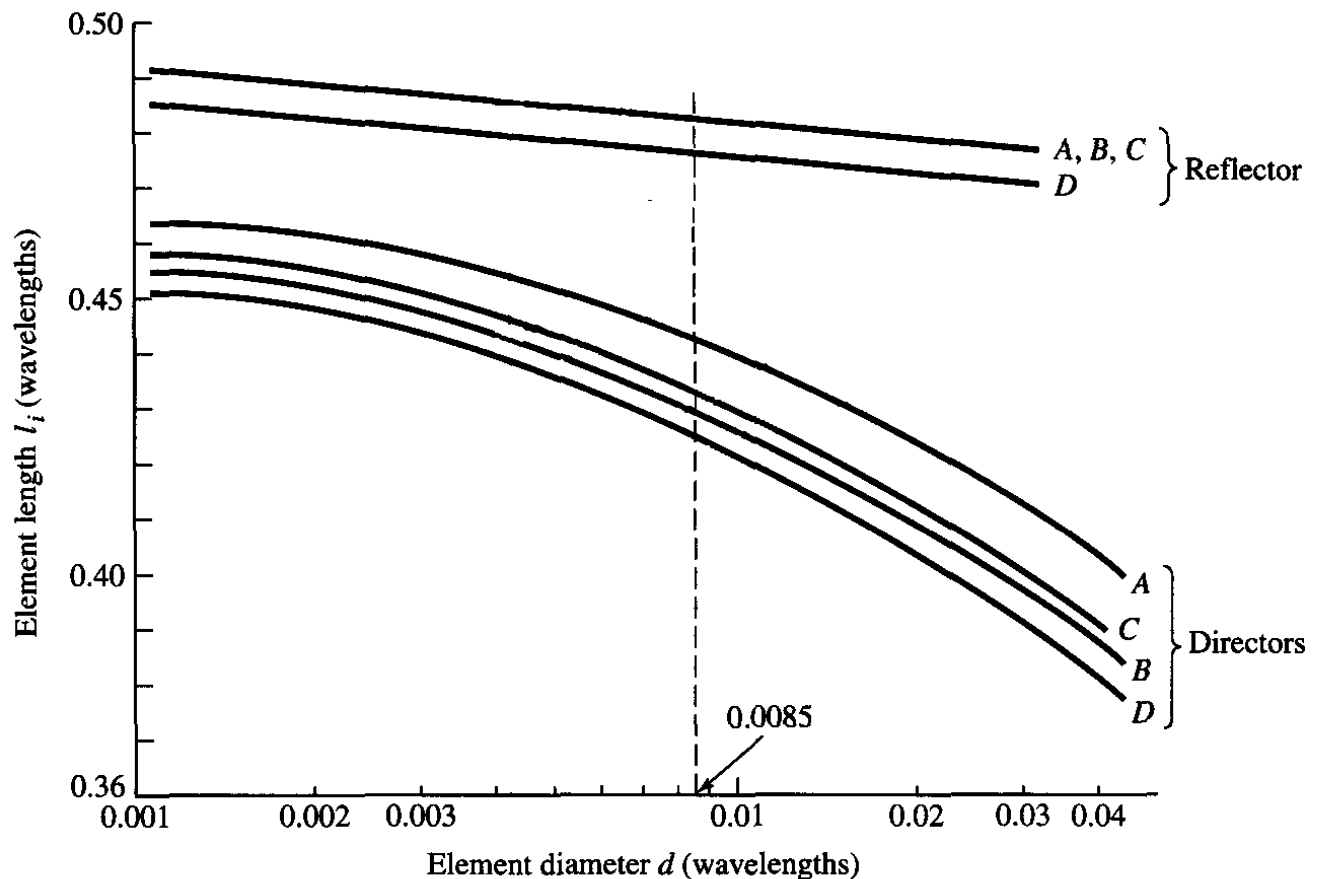
SOURCE: Peter P. Viezbicke, *Yagi Antenna Design*, NBS Technical Note 688, December 1976.

Table 1 Available tubing/pipe/rod sizes

| Nominal Diameter |          | Outer Diameter* |          |
|------------------|----------|-----------------|----------|
| (inches)         | (cm)     | (inches)        | (cm)     |
| 3/32             | 0.238125 | 3/32            | 0.238125 |
| 1/8              | 0.3175   | 1/8             | 0.3175   |
| 5/32             | 0.397    | 5/32            | 0.397    |
| 3/16             | 0.476    | 3/16            | 0.476    |
| 7/32             | 0.556    | 7/32            | 0.556    |
| 1/4              | 0.635    | 1/4             | 0.635    |
| 9/32             | 0.714    | 9/32            | 0.714    |
| 5/16             | 0.794    | 5/16            | 0.794    |
| 11/32            | 0.873    | 11/32           | 0.873    |
| 3/8              | 0.9525   | 3/8             | 0.9525   |
| 13/32            | 1.032    | 13/32           | 1.032    |
| 7/16             | 1.111    | 7/16            | 1.111    |
| 1/2              | 1.27     | 1/2             | 1.27     |
| 1/2              | 1.27     | 9/16            | 1.429    |
| 1/2              | 1.27     | 5/8             | 1.5875   |
| 3/4              | 1.905    | 7/8             | 2.223    |

\* For brass tubing/pipe/rods, the nominal or outer diameters are the same (wall thickness negligible). For copper pipes, the wall thickness is substantial and should be measured as it varies between manufacturers.

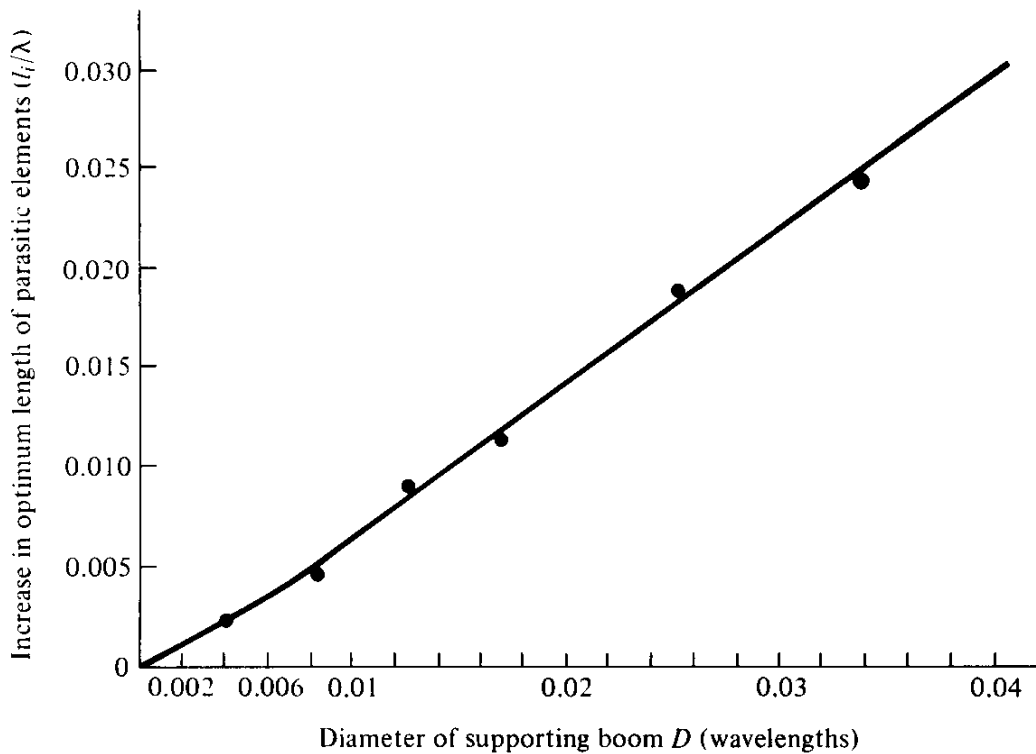
6. If  $d/\lambda = 0.0085$ , go to step 11 (no element diameter length corrections required). If  $d/\lambda \neq 0.0085$ , the elements lengths must be corrected. Plot the lengths of the reflector (element 1) and first director (element 3) from Table 10.6 on the appropriate design curves on Figure 10.25 (should fall on or near vertical line drawn from  $d/\lambda = 0.0085$ ). Label these points  $l_1''$  and  $l_3''$  respectively.



**Figure 10.25** Design curves to determine element lengths of Yagi-Uda arrays. (SOURCE: P. P. Viezbicke, "Yagi Antenna Design," NBS Technical Note 688, U.S. Department of Commerce/National Bureau of Standards, December 1976)

7. Draw a vertical line from the actual  $d / \lambda$  through the appropriate reflector and director design curves, where this line intersects the curves is the corrected lengths of the reflector  $l_1'$  and first director  $l_3'$ . To read the values, draw horizontal lines from the intersections to the left axis of the figure. The length  $l_3'$  should be used for any other directors that are the same original length as  $l_3$ .
8. Measure and label the arc length  $\Delta l$  between  $l_3''$  and  $l_3'$  along the design curve.
9. Plot the remaining original optimized director lengths from Table 10.6 on the appropriate director design curve on Figure 10.25 and label  $l_i''$  (Note: point(s) will not fall on the vertical line drawn from  $d / \lambda = 0.0085$ ).
10. To find the corrected (for element diameter) length(s) for the remaining directors, move  $\Delta l$  from  $l_i''$  (same direction as between  $l_3''$  and  $l_3'$ ) to the corrected length  $l_i'$ . To read the value(s), draw horizontal line(s) from  $l_i'$  to the left axis of the figure.
11. If a metal boom is used (else, skip to next step), the element lengths must be lengthened to compensate for it. On Figure 10.26, draw a vertical line from  $D / \lambda$  through the curve. Draw a horizontal line from the intersection to the left axis of the figure and read the compensation length. The final lengths of the elements (label  $l_i$ ) are found by adding this length to the original (Table 10.6) or the corrected (for element diameter) element lengths.

Note: By lengthening the elements, we are trying to make them have more inductive reactance, recall the reactance of a dipole goes from capacitive to inductive near the  $h/\lambda \sim 0.5$  resonance. This will counteract (hopefully) the parasitic capacitance introduced by the metallic boom.



**Figure 10.26** Increase in optimum length of parasitic elements as a function of metal boom diameter. (SOURCE: P. P. Viezbicke, "Yagi Antenna Design," NBS Technical Note 688, U.S. Department of Commerce/National Bureau of Standards, December 1976)

12. Design matching network (e.g., Gamma match, ...) to connect the driven element of the antenna to the selected transmission line. The length of the driven element  $l_2$  is empirically adjusted to achieve a match at the design frequency. Typically, it has a length between that of the reflector  $l_1$  and the first director  $l_3$ .