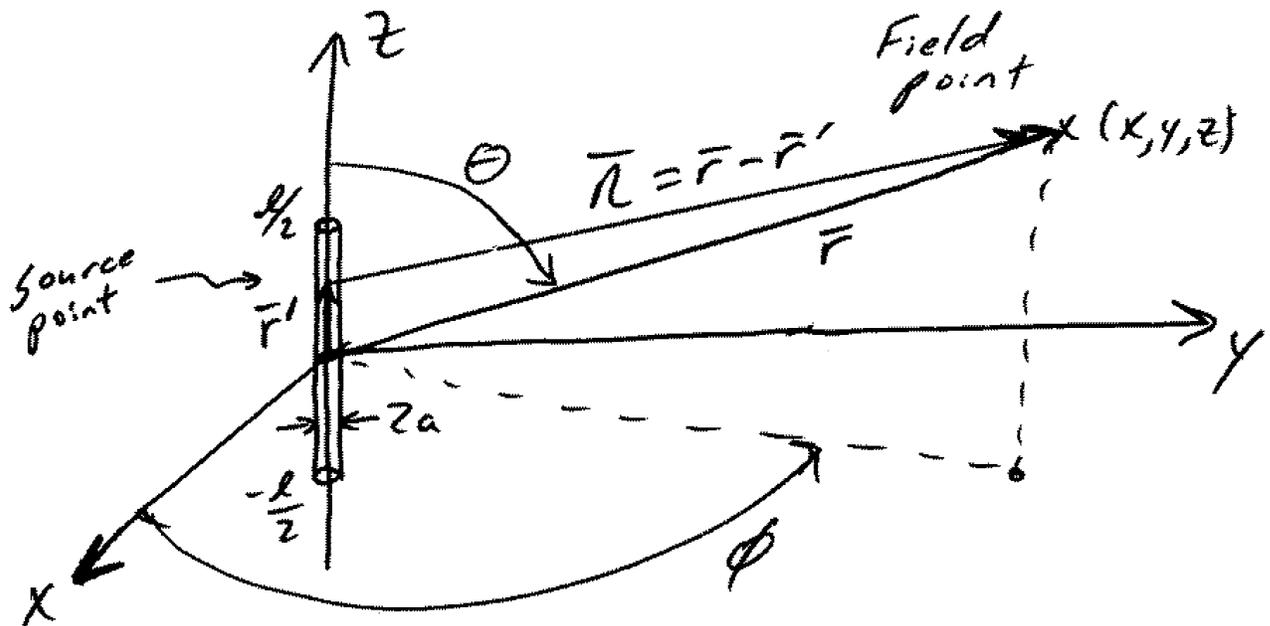


Chapter 4 Linear Wire Antennas

- Simple, robust, cheap, and give pretty good performance.
- Often used as base elements in antenna arrays

4.2 Infinitesimal Dipole

- length $l \leq \frac{\lambda}{50} \ll \lambda$ and radius $a \ll \lambda$
- not practical in reality, but are good approx. to capacitor-loaded (top-hat) antennas
- assume current is constant $\vec{I}(z') = \hat{a}_z I_0$



Geometry of infinitesimal dipole problem

4.2 cont.

Now to find $\bar{E} + \bar{H}$ for this dipole

Sources: $\bar{I}(z')$ $\rightarrow \bar{I}_0$, $\bar{J} = \bar{J}_s = 0$

$$\bar{I}_m = \bar{M}_s = \bar{m} = 0 \Rightarrow \underline{\underline{\bar{F} = 0}}$$

Therefore, $\bar{H} = \bar{H}_A$ + $\bar{E} = \bar{E}_A$

$$\bar{A} = \frac{\mu}{4\pi} \int \bar{I}_0 \frac{e^{-jkR}}{R} d\ell' \quad d\ell' = dz'$$

where $\bar{I}_0 = \bar{I}(z') = \hat{a}_z I_0$ $\bar{r} = x\hat{a}_x + y\hat{a}_y + z\hat{a}_z$
 $\bar{r}' = z'\hat{a}_z$

$$\bar{R} = \bar{r} - \bar{r}' = x\hat{a}_x + y\hat{a}_y + (z - z')\hat{a}_z$$

$$R = |\bar{R}| = \sqrt{x^2 + y^2 + (z - z')^2}$$

$$\approx \sqrt{x^2 + y^2 + z^2}$$

$$= r$$

for

$z' \ll z$ or

$z' \ll \sqrt{x^2 + y^2 + z^2}$

(better)

$$\bar{A} = \hat{a}_z \frac{\mu I_0}{4\pi} \frac{e^{-jkr}}{r} \int_{-l/2}^{l/2} dz'$$

$$\underline{\underline{\bar{A} = \hat{a}_z \frac{\mu I_0 l}{4\pi r} e^{-jkr}}}$$

\rightarrow convert $\hat{a}_z A_z$ over to spherical coordinates

4.2 conti.

$$A_r = A_x^{\circ} \sin \theta \cos \phi + A_y^{\circ} \sin \theta \sin \phi + A_z \cos \theta$$

$$= \frac{\mu I_0 l}{4\pi r} e^{-jkr} \cos \theta$$

$$A_{\theta} = A_x^{\circ} \cos \theta \cos \phi + A_y^{\circ} \cos \theta \sin \phi - A_z \sin \theta$$

$$= -\frac{\mu I_0 l}{4\pi r} e^{-jkr} \sin \theta$$

$$A_{\phi} = -A_x^{\circ} \sin \phi + A_y^{\circ} \cos \phi = 0$$

$$\bar{A} = (\hat{a}_r \cos \theta - \hat{a}_{\theta} \sin \theta) \frac{\mu I_0 l}{4\pi r} e^{-jkr}$$

$$\bar{H} = \frac{1}{\mu} \nabla \times \bar{A} = \frac{1}{\mu r^2 \sin \theta} \begin{vmatrix} \hat{a}_r & r \hat{a}_{\theta} & r \sin \theta \hat{a}_{\phi} \\ \frac{\partial}{\partial r} & \frac{\partial}{\partial \theta} & \frac{\partial}{\partial \phi} \\ \frac{\mu I_0 l}{4\pi r} e^{-jkr} \cos \theta & -\frac{\mu I_0 l}{4\pi r} e^{-jkr} \sin \theta & 0 \end{vmatrix}$$

$$= \frac{1}{\mu r^2 \sin \theta} \left[\hat{a}_r 0 - \hat{a}_r \frac{\partial A_{\phi}}{\partial \phi} \right] + \frac{1}{\mu r \sin \theta} \left[\hat{a}_{\theta} \frac{\partial A_r}{\partial \phi} - \hat{a}_{\theta} 0 \right]$$

$$+ \frac{1}{\mu r} \left[\frac{\partial}{\partial r} \left(-\frac{\mu I_0 l}{4\pi} e^{-jkr} \sin \theta \right) - \frac{\partial}{\partial \theta} \left(\frac{\mu I_0 l}{4\pi r} e^{-jkr} \cos \theta \right) \right] \hat{a}_{\phi}$$

$$= \frac{1}{\mu r} \left[+jk \frac{\mu I_0 l}{4\pi} e^{-jkr} \sin \theta + \frac{\mu I_0 l}{4\pi r} e^{-jkr} \sin \theta \right] \hat{a}_{\phi}$$

$$= \hat{a}_{\phi} \left[\frac{jk I_0 l}{4\pi r} e^{-jkr} \sin \theta + \frac{I_0 l}{4\pi r^2} e^{-jkr} \sin \theta \right]$$

$$\bar{H} = \hat{a}_{\phi} \frac{jk I_0 l \sin \theta}{4\pi r} \left(1 + \frac{1}{jkr} \right) e^{-jkr}$$

4.2 cont.

0 (free space)

$$(3-10) \quad \nabla \times \vec{H} = \vec{J} + j\omega \epsilon \vec{E} \Rightarrow \vec{E} = \frac{1}{j\omega \epsilon} \nabla \times \vec{H}$$

$$\vec{E} = \frac{1}{j\omega \epsilon r^2 \sin \theta} \begin{vmatrix} \hat{a}_r & r \hat{a}_\theta & r \sin \theta \hat{a}_\phi \\ \frac{\partial}{\partial r} & \frac{\partial}{\partial \theta} & \frac{\partial}{\partial \phi} \\ 0 & 0 & (r \sin \theta) \frac{jK I_0 l \sin \theta}{4\pi r} \left(1 + \frac{1}{jkr}\right) e^{-jkr} \end{vmatrix}$$

$$= \frac{1}{j\omega \epsilon r^2 \sin \theta} \hat{a}_r \frac{\partial}{\partial \theta} \left[\frac{jK I_0 l \sin^2 \theta}{4\pi} \left(1 + \frac{1}{jkr}\right) e^{-jkr} \right]$$

$$- \frac{1}{j\omega \epsilon r^2 \sin \theta} r \hat{a}_\theta \frac{\partial}{\partial r} \left[\frac{jK I_0 l \sin^2 \theta}{4\pi} \left(1 + \frac{1}{jkr}\right) e^{-jkr} \right]$$

$$= \hat{a}_r \frac{1}{j\omega \epsilon r^2 \sin \theta} \frac{jK I_0 l 2 \sin \theta \cos \theta}{4\pi} \left(1 + \frac{1}{jkr}\right) e^{-jkr}$$

$$- \hat{a}_\theta \frac{1}{j\omega \epsilon r \sin \theta} \frac{jK I_0 l \sin^2 \theta}{4\pi} \left[-jK e^{-jkr} \left(1 + \frac{1}{jkr}\right) + \left(0 - \frac{1}{jkr^2}\right) e^{-jkr} \right]$$

$$\text{use } \frac{K}{\omega \epsilon} = \frac{\omega \mu \epsilon}{\omega \epsilon} = \sqrt{\frac{\mu}{\epsilon}} = \eta$$

$$\vec{E} = \hat{a}_r \frac{\eta I_0 l \cos \theta}{2\pi r^2} \left(1 + \frac{1}{jkr}\right) e^{-jkr}$$

$$+ \hat{a}_\theta \frac{j\eta K I_0 l \sin \theta}{4\pi r} \left[1 + \frac{1}{jkr} - \frac{1}{(kr)^2} \right] e^{-jkr}$$

$$\vec{W}_{\text{ave}} = \frac{1}{2} \text{Re} \{ \vec{E} \times \vec{H}^* \} \quad (2-8)$$

$$= \frac{1}{2} \text{Re} \{ (\hat{a}_r E_r + \hat{a}_\theta E_\theta) \times \hat{a}_\phi H_\phi^* \}$$

4.2 cont.

$$\begin{aligned}
 \overline{\text{Wave}} &= \frac{1}{2} \text{Re} \left\{ -\hat{a}_\theta E_r H_\phi^* + \hat{a}_r E_\theta H_\phi^* \right\} \\
 &= \frac{1}{2} \text{Re} \left\{ \hat{a}_r \frac{j\eta k I_0 l \sin\theta}{4\pi r} \left[1 + \frac{1}{jkr} - \frac{1}{(kr)^2} \right] e^{jkr} \left(\frac{-j k I_0 l \sin\theta}{4\pi r} \right) \left(1 + \frac{1}{jkr} \right) e^{jkr} \right. \\
 &\quad \left. - \hat{a}_\theta \frac{\eta I_0 l \cos\theta}{2\pi r^2} \left(1 + \frac{1}{jkr} \right) e^{jkr} \left(\frac{-j k I_0 l \sin\theta}{4\pi r} \right) \left(1 + \frac{1}{jkr} \right) e^{jkr} \right\} \\
 &= \frac{1}{2} \text{Re} \left\{ \hat{a}_r \frac{-(-1)\eta k^2 |I_0 l|^2 \sin^2\theta}{(4\pi r)^2} \left(1 + \frac{1}{jkr} - \frac{1}{(kr)^2} - \frac{1}{jkr} + \frac{1}{(kr)^2} + \frac{1}{j(kr)^3} \right) \right. \\
 &\quad \left. + \hat{a}_\theta \frac{j\eta k |I_0 l|^2 \cos\theta \sin\theta}{8\pi^2 r^3} \left(1 - \frac{1}{jkr} + \frac{1}{jkr} + \frac{1}{(kr)^2} \right) \right\}
 \end{aligned}$$

use $k = \frac{2\pi}{\lambda}$ in \hat{a}_r term

$$\begin{aligned}
 &= \frac{1}{2} \text{Re} \left\{ \hat{a}_r \frac{\eta}{4} \left| \frac{I_0 l}{\lambda} \right|^2 \frac{\sin^2\theta}{r^2} \left(1 + \frac{1}{j(kr)^3} \right) \right. \\
 &\quad \left. + \hat{a}_\theta \frac{j\eta k |I_0 l|^2 \cos\theta \sin\theta}{8\pi^2 r^3} \left(1 + \frac{1}{(kr)^2} \right) \right\}
 \end{aligned}$$

$$\boxed{\overline{\text{Wave}} = \hat{a}_r \frac{\eta}{8} \left| \frac{I_0 l}{\lambda} \right|^2 \frac{\sin^2\theta}{r^2}}$$

$$\text{Prad} = \oiint \overline{\text{Wave}} \cdot d\vec{s}_r \quad (2-9)$$

$$\text{where } d\vec{s}_r = \hat{a}_r r^2 \sin\theta d\theta d\phi$$

4.2 cont.

$$\begin{aligned}
 P_{\text{rad}} &= \int_{\phi=0}^{2\pi} \int_{\theta=0}^{\pi} \frac{\eta}{8} \left| \frac{I_0 l}{\lambda} \right|^2 \sin^3 \theta \, d\theta \, d\phi \\
 &= \frac{\eta}{8} \left| \frac{I_0 l}{\lambda} \right|^2 \int_{\phi=0}^{2\pi} d\phi \int_{\theta=0}^{\pi} \sin^3 \theta \, d\theta \\
 &= \frac{\eta}{8} \left| \frac{I_0 l}{\lambda} \right|^2 (2\pi) \left(\frac{4}{3} \right)
 \end{aligned}$$

$$\underline{\underline{P_{\text{rad}} = \frac{\eta \pi}{3} \left| \frac{I_0 l}{\lambda} \right|^2}}$$

From (2-76) $P_{\text{rad}} = \frac{1}{2} |I_0|^2 R_r$ where $|I_0|^2 = |I_0|^2$

$$\text{So } R_r = \frac{\eta \frac{\pi}{3} \left| \frac{I_0 l}{\lambda} \right|^2}{\frac{1}{2} |I_0|^2} = \underline{\underline{\eta \frac{2\pi}{3} \left(\frac{l}{\lambda} \right)^2 \Omega}}$$

For free-space $\eta_0 = 376.73 \Omega$

$$\underline{\underline{R_r = 789 \left(\frac{l}{\lambda} \right)^2 \Omega}}$$

To be infinitesimal $\frac{l}{\lambda} \ll 1$ (usually say $\frac{l}{\lambda} \leq \frac{1}{50}$),

so $R_r \leq 0.3 \Omega$ (quite small)

→ Not practical, big mismatch problems w/ practical transmission lines

4.2 cont.

Since $\bar{I}_e = \hat{a}_z I_0 \leftarrow$ constant current distribution

$$\underline{R_L = R_{hf} = \frac{\ell}{\rho} \sqrt{\frac{\omega \mu_0}{2\sigma}} \quad (2-90b)}$$

The infinitesimal dipoles reactance will be negative (capacitive) \rightarrow use analogy w/ open-circ

stub where $Z_{in} = -j Z_0 / \tan(\beta \ell/2) \approx -j \frac{Z_0}{\beta \ell/2} = j X_A$

$$\text{Since } \beta = \frac{2\pi}{\lambda} \rightarrow \beta \frac{\ell}{2} = \pi \frac{\ell}{\lambda} \ll 1$$

and $\tan(x) = x$ when $x \ll 1$

$$\boxed{\text{Radian distance} \equiv r = \frac{\lambda}{2\pi} \Rightarrow \underline{kr=1}}$$

Note: Real + Imaginary parts of \bar{H} and E_r are equal in magnitude at the radian distance

$$\boxed{\text{Radian sphere} \rightarrow \text{sphere of radius } r = \frac{\lambda}{2\pi}}$$

\rightarrow Preactive $>$ Prad inside Radian Sphere

\uparrow
Stored energy/power (the imaginary parts of \bar{W})

4.2 cont.Near-field Region ($kr \ll 1$)

$$\vec{E} = \hat{a}_r \frac{\eta I_0 l \cos \theta}{2\pi r^2} \left(1 + \overset{\text{big}}{\frac{1}{jkr}} \right) e^{-jkr} \\ + \hat{a}_\theta \frac{j\eta k I_0 l \sin \theta}{4\pi r} \left[1 + \frac{1}{jkr} - \overset{\text{big}}{\frac{1}{(kr)^2}} \right] e^{-jkr}$$

$$\vec{E}_{NF} \approx \hat{a}_r (-j\eta) \frac{I_0 l \cos \theta}{2\pi kr^3} e^{-jkr} + \hat{a}_\theta (-j\eta) \frac{I_0 l \sin \theta}{4\pi kr^3} e^{-jkr}$$

$$\vec{H} = \hat{a}_\phi \frac{j k I_0 l \sin \theta}{4\pi r} \left(1 + \overset{\text{big}}{\frac{1}{jkr}} \right) e^{-jkr}$$

$$\vec{H}_{NF} \approx \hat{a}_\phi \frac{I_0 l \sin \theta}{4\pi r^2} e^{-jkr}$$

Note:

$$\underline{\underline{\text{Wave}_{NF} = \frac{1}{2} \text{Re} \{ \vec{E}_{NF} \times \vec{H}_{NF}^* \} = 0}}$$

↑
 $\vec{E} + \vec{H}$ 90° out of phase

4.2 cont.

Far-field Region ($Kr \gg 1$)

$$\begin{aligned} \bar{E} = & \hat{a}_r \frac{\eta I_0 l \cos\theta}{2\pi r^2} \left(1 + \frac{1}{jkr}\right) e^{-jkr} + \\ & + \hat{a}_\theta \frac{j\eta K I_0 l \sin\theta}{4\pi r} \left[1 + \frac{1}{jkr} - \frac{1}{(kr)^2}\right] e^{-jkr} \end{aligned}$$

$$\boxed{\bar{E}_{FF} \approx \hat{a}_\theta \frac{j\eta K I_0 l \sin\theta}{4\pi r} e^{-jkr}}$$

$$\bar{H} = \hat{a}_\phi \frac{jK I_0 l \sin\theta}{4\pi r} \left(1 + \frac{1}{jkr}\right) e^{-jkr}$$

$$\boxed{\bar{H}_{FF} = \hat{a}_\phi \frac{jK I_0 l \sin\theta}{4\pi r} e^{-jkr}}$$

Note that $Z_w = \frac{E_\theta}{H_\phi} = \eta \equiv$ wave impedance

Note! In far-field \bar{E} & \bar{H} are orthogonal & transverse to direction of propagation (\hat{a}_r) of wave

4.2 cont.

Directivity

We already found-

$$\overline{W}_{\text{ave}} = \bar{a}_r \frac{\eta}{8} \left| \frac{I_0 l}{\lambda} \right|^2 \frac{\sin^2 \theta}{r^2} \quad \& \quad P_{\text{rad}} = \frac{\eta \pi}{3} \left| \frac{I_0 l}{\lambda} \right|^2$$

Use $U = r^2 |\overline{W}_{\text{ave}}| = \frac{\eta}{8} \left| \frac{I_0 l}{\lambda} \right|^2 \sin^2 \theta$ (2-12)

and $D = \frac{4\pi U}{P_{\text{rad}}} = \frac{\cancel{4\pi} \cancel{\eta} \left| \cancel{I_0 l} \right|^2 \sin^2 \theta}{\cancel{8} \cancel{\eta} \left| \cancel{I_0 l} \right|^2}$

$$\underline{\underline{D(\theta) = 1.5 \sin^2 \theta}}$$

$$\underline{\underline{D_0 = 1.5 \quad (@ \theta = \pi/2)}}$$

$$\underline{\underline{D_0 = 10 \log_{10}(1.5) = 1.7609 \text{ dB}_i}}$$

ignoring losses $A_{\text{em}} = \left(\frac{\lambda^2}{4\pi} \right) D_0 = 1.5 \left(\frac{\lambda^2}{4\pi} \right) = \underline{\underline{\frac{3\lambda^2}{8\pi}}}$

4.3 cont.

$$\bar{A} = \frac{\mu}{4\pi} \left[\hat{a}_z \int_{z'=-l/2}^0 I_0 \left(1 + \frac{zz'}{l}\right) \frac{e^{-jkR}}{R} dz' + \hat{a}_z \int_{z'=0}^{l/2} I_0 \left(1 - \frac{zz'}{l}\right) \frac{e^{-jkR}}{R} dz' \right]$$

again $R = |\bar{r}| = \sqrt{x^2 + y^2 + (z - z')^2} \approx r$ only small phase results when r is small

$$\begin{aligned} \bar{A} &= \frac{\mu I_0}{4\pi} \frac{e^{-jkr}}{r} \hat{a}_z \left[\int_{-l/2}^0 \left(1 + \frac{zz'}{l}\right) dz' + \int_0^{l/2} \left(1 - \frac{zz'}{l}\right) dz' \right] \\ &= \hat{a}_z \frac{\mu I_0}{4\pi} \frac{e^{-jkr}}{r} \left[\left(z' + \frac{z'^2}{l}\right) \Big|_{-l/2}^0 + \left(z' - \frac{z'^2}{l}\right) \Big|_0^{l/2} \right] \\ &= \hat{a}_z \frac{\mu I_0}{4\pi} \frac{e^{-jkr}}{r} \left[\left(0 + \frac{l}{2} - \frac{l}{4}\right) + \left(\frac{l}{2} - \frac{l}{4} - 0 + 0\right) \right] \end{aligned}$$

$$\bar{A} = \hat{a}_z \frac{1}{2} \left(\frac{\mu I_0 l e^{-jkr}}{4\pi r} \right) \leftarrow \frac{1}{2} \text{ result of infinitesimal dipole}$$

Therefore:

$$\begin{aligned} \bar{H}_{\text{Small}} &= \frac{1}{2} \bar{H}_{\text{inf}} = \hat{a}_\phi \frac{j k I_0 l \sin\theta}{8\pi r} \left(1 + \frac{1}{jkr}\right) e^{-jkr} \\ \bar{E}_{\text{Small}} &= \frac{1}{2} \bar{E}_{\text{inf}} = \hat{a}_r \frac{j I_0 l \cos\theta}{4\pi r^2} \left(1 + \frac{1}{jkr}\right) e^{-jkr} \\ &\quad + \hat{a}_\theta \frac{j k I_0 l \sin\theta}{8\pi r} \left[1 + \frac{1}{jkr} - \frac{1}{(kr)^2}\right] e^{-jkr} \end{aligned}$$

4.3 cont.

$$\overline{W}_{ave,small} = \frac{1}{4} \overline{W}_{ave,int} \leftarrow \left(\frac{1}{2}\right)^2 \text{ from } \vec{E} + \vec{H} \text{ terms}$$

$$\overline{W}_{ave,small} = \hat{a}_r \frac{\eta}{32} \left| \frac{I_0 l}{\lambda} \right|^2 \frac{\sin^2 \theta}{r^2}$$

$$\overline{P}_{rad,small} = \frac{1}{4} \overline{P}_{rad,int} = \frac{\eta \pi}{12} \left| \frac{I_0 l}{\lambda} \right|^2$$

$$R_{r,small} = \frac{1}{4} R_{r,int} = \eta \frac{2\pi}{12} \left(\frac{l}{\lambda} \right)^2 = \eta \frac{\pi}{6} \left(\frac{l}{\lambda} \right)^2$$

$$\text{For free space } R_r = 197.25 \left(\frac{l}{\lambda} \right)^2 \Omega$$

$$0.08 \leq R_{r,small} \leq 2 \Omega \leftarrow \text{still hard to match}$$

$\uparrow \quad \quad \quad \uparrow$
 $l = \lambda/50 \quad \quad \quad l = \lambda/10$

$$\underline{R_L = \frac{R_{ref}}{3}} \text{ due to triangular current distribution}$$

$$\text{Also } |\overline{W}_{ave}| = \frac{\eta}{32} \left| \frac{I_0 l}{\lambda} \right|^2 \frac{\sin^2 \theta}{r^2}$$

$$\underline{U = r^2 |\overline{W}_{ave}| = \frac{\eta}{32} \left| \frac{I_0 l}{\lambda} \right|^2 \sin^2 \theta}$$

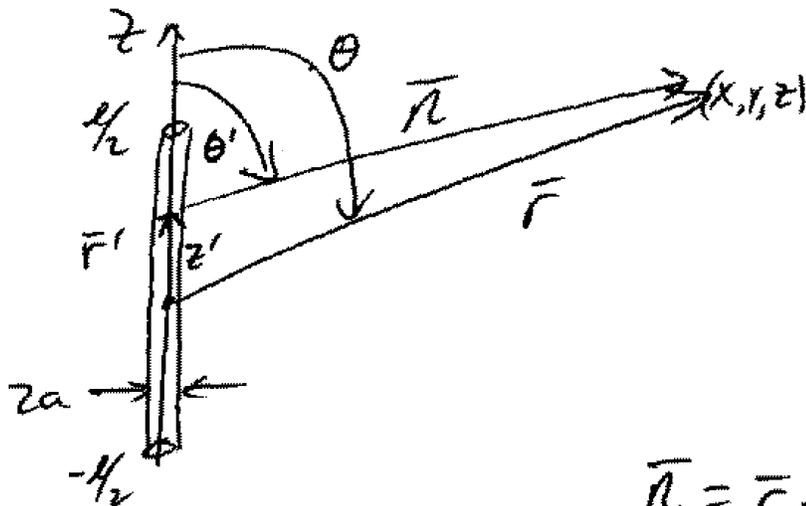
$$D(\theta) = \frac{4\pi U}{P_{rad}} = \frac{4\pi \cancel{\frac{\eta}{32}} \left| \frac{I_0 l}{\lambda} \right|^2 \sin^2 \theta}{\cancel{\frac{\eta}{12}} \left| \frac{I_0 l}{\lambda} \right|^2}$$

$$\underline{D(\theta) = 1.5 \sin^2 \theta} \quad \& \quad \underline{D_0 = 1.5 = 1.76 \text{ dB}}$$

4.4 Region Separation

on a finite length dipole on the z-axis

$$\bar{A} = \frac{\mu}{4\pi} \int \bar{I}_e(x', y', z') \frac{e^{-jkr}}{r} dl'$$



$$dl' = dz'$$

$$\bar{r} = \bar{r} - \bar{r}' \text{ where}$$

$$\bar{r} = x\hat{a}_x + y\hat{a}_y + z\hat{a}_z$$

$$\bar{r}' = x'\hat{a}_x + y'\hat{a}_y + z'\hat{a}_z$$

$$\approx z'\hat{a}_z \text{ if } a \ll r$$

$$\bar{r} = \bar{r} - \bar{r}' = x\hat{a}_x + y\hat{a}_y + (z - z')\hat{a}_z$$

$$|\bar{r}| = r = \sqrt{x^2 + y^2 + (z - z')^2}$$

So,

$$\bar{A} = \frac{\mu}{4\pi} \int \bar{I}_e(x', y', z') \frac{e^{-jk\sqrt{x^2 + y^2 + (z - z')^2}}}{\sqrt{x^2 + y^2 + (z - z')^2}} dz'$$

↳ can be difficult to evaluate

However, r can be expressed in terms of a binomial expansion

$$r = \sqrt{x^2 + y^2 + (z - z')^2} = \sqrt{x^2 + y^2 + z^2 - 2zz' + z'^2}$$

but $r^2 = x^2 + y^2 + z^2$ & $z = r \cos \theta$

4.4 cont.

So $R = \sqrt{r^2 - 2rz' \cos \theta + z'^2}$ ← still exact

a binomial series expansion $(a+x)^n = a^n + na^{n-1}x + \frac{n(n-1)}{2!}a^{n-2}x^2 + \dots$

with $n = \frac{1}{2}$, $a = r^2$, and $x = -2rz' \cos \theta + z'^2$ gives

$$R = r - z' \cos \theta + \frac{1}{r} \left(\frac{z'^2}{2} \sin^2 \theta \right) + \frac{1}{r^2} \left(\frac{z'^3}{2} \cos \theta \sin^2 \theta \right) + \dots$$

Far-field

as $r \gg z'$, we can drop the z'^n terms where $n \geq 2$

$$\Rightarrow \underline{R \approx r - z' \cos \theta}$$

What will be the worst case error?

→ when $\frac{1}{r} \left(\frac{z'^2}{2} \sin^2 \theta \right)$ is biggest (e.g. $\theta = \pi/2$)

$$\text{Max} \left\{ \frac{1}{r} \left(\frac{z'^2}{2} \sin^2 \theta \right) \right\} = \frac{z'^2}{2r}$$

Note: all the other high order terms are zero when $\theta = \pi/2$ because they contain $\cos \theta$ arguments

Examining the $\frac{e^{-jkr}}{r}$ term of \bar{A} , we can

see that small variations in $1/r$ will not have much effect. However, since e^{-jkr}

4.4 cont.

is periodic w/ $kR = n2\pi + kR \Rightarrow$ The phase error is more critical.

Researchers have found that a phase error $< 22.5^\circ$ ($\frac{\pi}{8}$) is usually acceptable

ex. $e^{j0} = 1$

$$e^{\pm j\frac{\pi}{8}} = 0.9239 \pm j0.3827 \quad \left\{ \begin{array}{l} \text{still 'fairly'} \\ \text{close} \end{array} \right.$$

$$e^{\pm j\frac{\pi}{16}} = 0.9808 \pm j0.1951 \quad \leftarrow \text{better}$$

So, the criteria is that $\frac{kz'^2}{2r} \leq \frac{\pi}{8}$

\rightarrow Worst case $z' = \pm \frac{l}{2}$

$$\frac{k \frac{l^2}{4}}{2r} \leq \frac{\pi}{8} \quad (k = \frac{2\pi}{\lambda})$$

$$\frac{2\pi l^2}{8\lambda r} \leq \frac{\pi}{8}$$

\downarrow

$$r \geq \frac{2\pi l^2}{8\lambda} \frac{8}{\pi} = \frac{2l^2}{\lambda}$$

but $l = D = \text{max dimension of antenna}$

$$\underline{\underline{r \geq \frac{2D^2}{\lambda}}} \quad (\text{far-field!})$$

4.4 cont.

Radiating Near-Field (Fresnel) Region

Here, let $R \approx r - z' \cos \theta + \frac{1}{r} \left(\frac{z'^2}{2} \sin^2 \theta \right)$
 following a similar argument for phase error leads to

$$r \geq 0.62 \sqrt{\frac{L^3}{\lambda}} \rightarrow 0.62 \sqrt{\frac{D^3}{\lambda}}$$

Therefore, as discussed in Chapter 2

Near-field	$r < 0.62 \sqrt{\frac{D^3}{\lambda}}$
Fresnel	$0.62 \sqrt{\frac{D^3}{\lambda}} \leq r < \frac{2D^2}{\lambda}$
Far-field	$r \geq \frac{2D^2}{\lambda}$

Note: When converting these phasor results back to the time-domain, the e^{-jkR} term yields "retarded time"

$$\text{e.g. } \text{Re} \{ E(\omega) e^{-jkR} e^{j\omega t} \} = \text{Re} \left\{ E(\omega) e^{j\omega(t - R/c)} \right\}$$

$$\text{since } R = \frac{\omega}{c} = \frac{2\pi}{\lambda}$$

"retarded" time
AKA: propagation time

→ have "retarded" potentials when we take this into account

4.5 Finite Length Dipole

→ use a better approximation that the current on a thin dipole is sinusoidally distributed when center-fed as:

$$\bar{I}_e(z') = \begin{cases} \hat{a}_z I_0 \sin[k(\frac{l}{2} - z')] & 0 \leq z' \leq \frac{l}{2} \\ \hat{a}_z I_0 \sin[k(\frac{l}{2} + z')] & -\frac{l}{2} \leq z' \leq 0 \end{cases}$$

→ Now the current $\bar{I}_e(z' = \pm \frac{l}{2}) = 0$

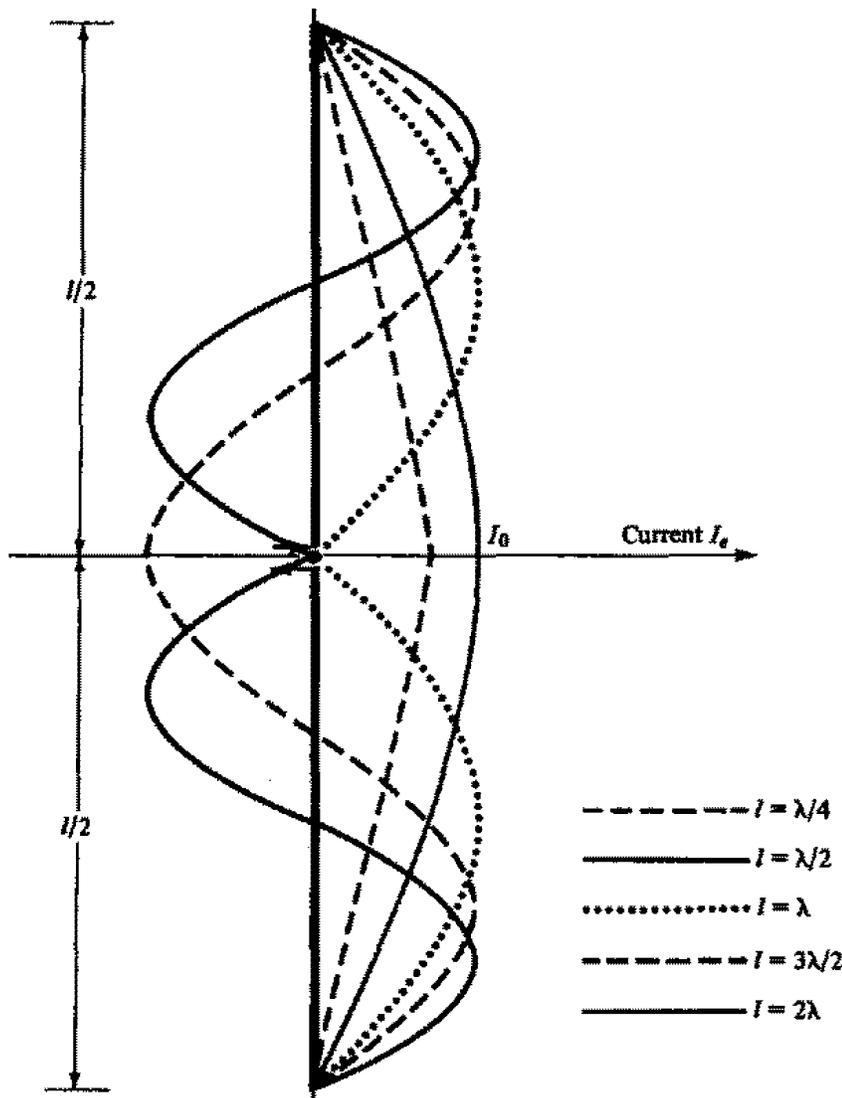


Figure 4.8 Current distributions along the length of a linear wire antenna.
(Balanis, Ant. Theory, 2nd Edn, P 156)

4.5 cont.

In the far-field, we have that

$$\left. \begin{aligned} E_{\theta} &= j\eta \frac{\kappa I_0 l e^{-jk r}}{4\pi r} \sin\theta \\ H_{\phi} &= j \frac{\kappa I_0 l e^{-jk r}}{4\pi r} \sin\theta \\ E_r = E_{\phi} = H_r = H_{\theta} &= 0 \end{aligned} \right\} (4-26)$$

for an infinitesimal dipole of length l located at the origin. A finite length dipole can be "built" from these.

To adapt this result to our finite length dipole, let $I_0 \Rightarrow I_e(z')$

exponent: $r \Rightarrow R = r - z' \cos\theta + \frac{1}{r} \Rightarrow \frac{1}{R} \Rightarrow \frac{1}{r}$ denominator \downarrow

$l \Rightarrow dz'$ \leftarrow accounts for infinitesimal dipole being off the origin

$E_{\theta} \Rightarrow dE_{\theta}$ \leftarrow contributions from each

$H_{\phi} \Rightarrow dH_{\phi}$ \leftarrow infinitesimal dipole

$$dE_{\theta} = j\eta \frac{\kappa I_e(z') dz' e^{-jk(r - z' \cos\theta)}}{4\pi r} \sin\theta$$

$$dE_{\theta} = j\eta \kappa \frac{e^{-jk r}}{4\pi r} \sin\theta I_e(z') e^{+jk z' \cos\theta} dz'$$

$$dH_{\phi} = j\kappa \frac{e^{-jk r}}{4\pi r} \sin\theta I_e(z') e^{+jk z' \cos\theta} dz'$$

4.5 cont.

Now, if we "add-up" / integrate dE_θ & dH_ϕ over the length of our finite length dipoles

$$E_\theta = \int_{z'=-l/2}^{l/2} dE_\theta = \left(j\eta k \frac{e^{-jkr}}{4\pi r} \sin\theta \right) \left[\int_{z'=-l/2}^{l/2} I_c(z') e^{jkz'\cos\theta} dz' \right]$$

$$H_\phi = \int_{z'=-l/2}^{l/2} dH_\phi = \left(jk \frac{e^{-jkr}}{4\pi r} \sin\theta \right) \left[\int_{z'=-l/2}^{l/2} I_c(z') e^{jkz'\cos\theta} dz' \right]$$

Total fields = element factor \times space factor
 (same as infinitesimal dipole) (accounts for current distribution)

\Rightarrow similar thing happens w/ antenna arrays
 Substitute in $I_c(z')$ and use the indefinite integral

$$\int e^{\alpha x} \sin(\beta x + \gamma) dx = \frac{e^{\alpha x}}{\alpha^2 + \beta^2} \left[\alpha \sin(\beta x + \gamma) - \beta \cos(\beta x + \gamma) \right]$$

$$w/ \alpha = jk \cos\theta \quad x \rightarrow z'$$

$$\beta = \pm k$$

$$\gamma = kl/2$$

4.5 cont.

Then

$$E_{\theta} \approx j\eta \frac{I_0 e^{-jkr}}{2\pi r} \left[\frac{\cos\left(\frac{kr}{2} \cos\theta\right) - \cos\left(\frac{kr}{2}\right)}{\sin\theta} \right]$$

$$H_{\phi} \approx j \frac{I_0 e^{-jkr}}{2\pi r} \left[\frac{\cos\left(\frac{kr}{2} \cos\theta\right) - \cos\left(\frac{kr}{2}\right)}{\sin\theta} \right]$$

$$= \frac{E_{\theta}}{\eta}$$

$$\overline{W}_{\text{ave}} = \frac{1}{2} \text{Re} \{ \vec{E} \times \vec{H}^* \} = \frac{1}{2} \text{Re} \{ \hat{a}_{\theta} E_{\theta} \times \hat{a}_{\phi} H_{\phi}^* \}$$

$$= \frac{1}{2} \text{Re} \left\{ \hat{a}_{\theta} E_{\theta} \times \hat{a}_{\phi} \frac{E_{\theta}^*}{\eta} \right\}$$

$$= \hat{a}_r \frac{1}{2\eta} |E_{\theta}|^2$$

$$\overline{W}_{\text{ave}} = \hat{a}_r \frac{\eta |I_0|^2}{8\pi^2 r^2} \left[\frac{\cos\left(\frac{kr}{2} \cos\theta\right) - \cos\left(\frac{kr}{2}\right)}{\sin\theta} \right]^2$$

$$U = r^2 \overline{W}_{\text{ave}} = \frac{\eta |I_0|^2}{8\pi^2} \left[\frac{\cos\left(\frac{kr}{2} \cos\theta\right) - \cos\left(\frac{kr}{2}\right)}{\sin\theta} \right]^2$$

↑ No ϕ dependence

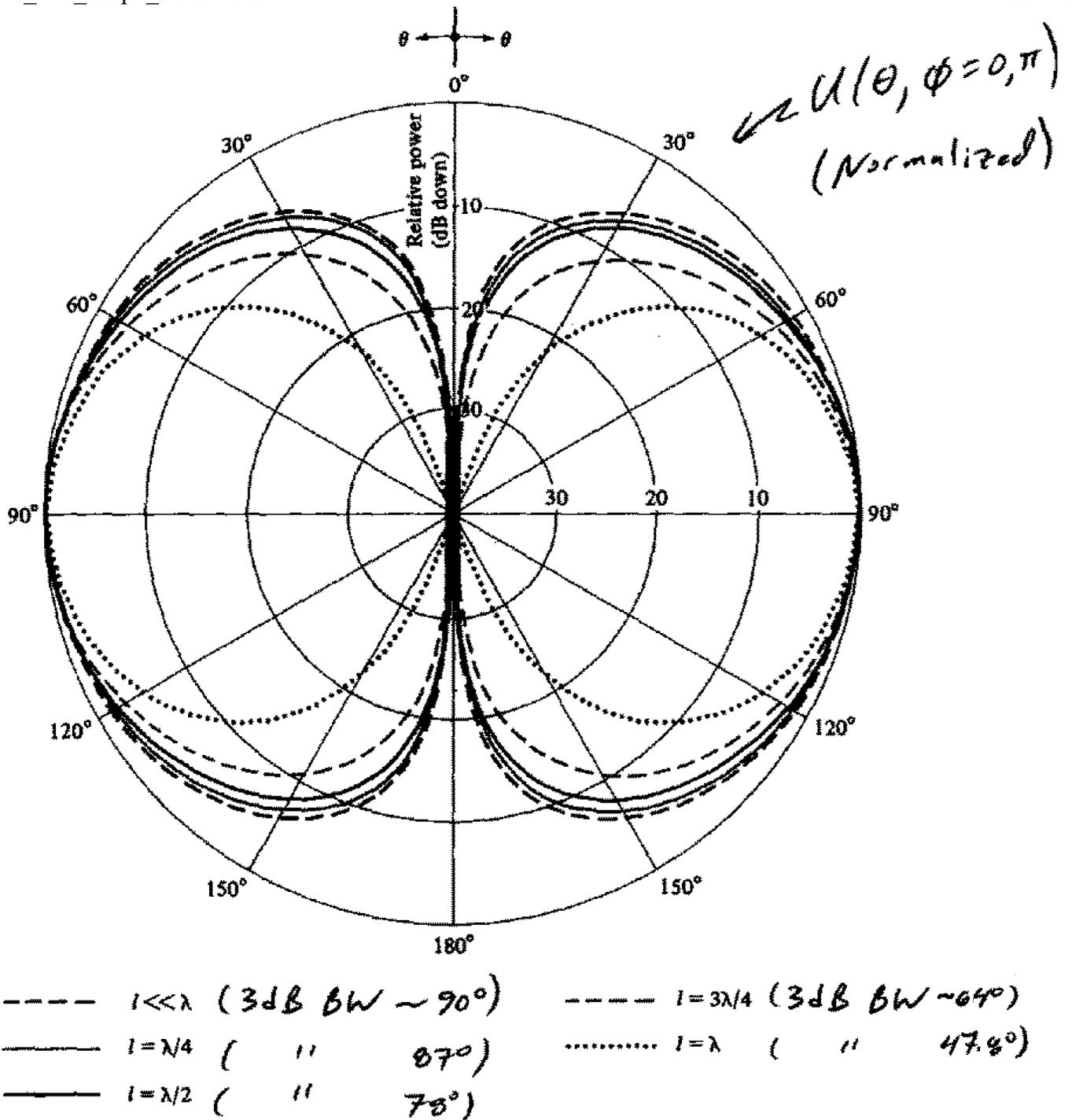
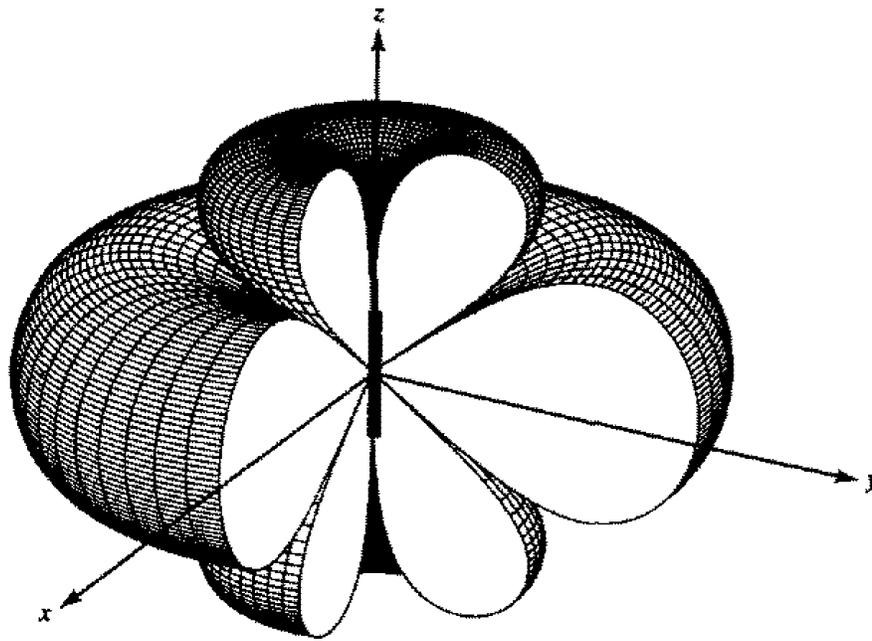


Figure 4.6 Elevation plane amplitude patterns for a thin dipole with sinusoidal current distribution ($l = \lambda/4, \lambda/2, 3\lambda/4, \lambda$).

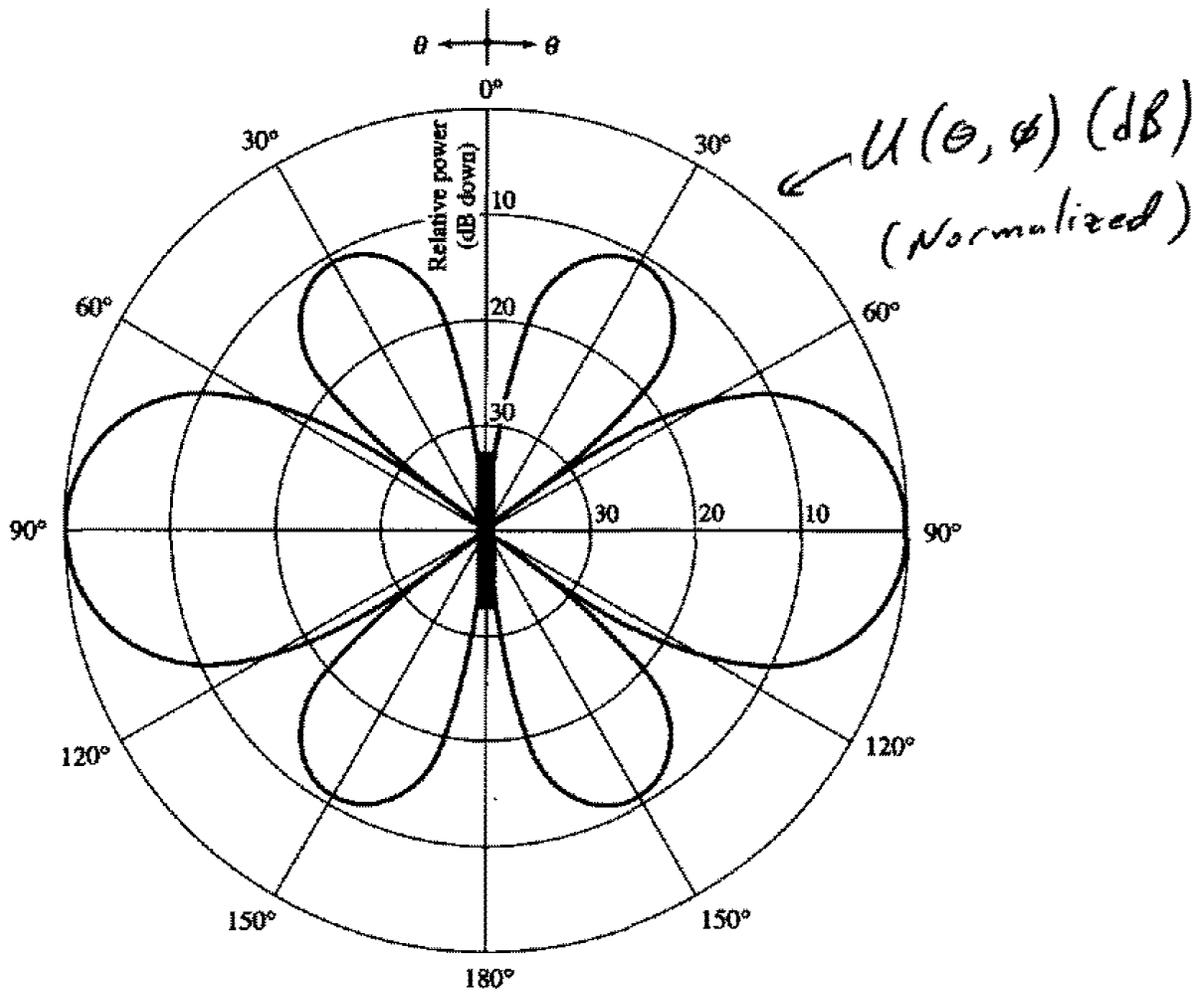
[Balanis, Ant. Theory (2nd Ed), p. 154]

Relative Power = $U(\theta, \phi) \text{ (dB}_i\text{)} - \text{Max}\{U(\theta, \phi) \text{ (dB}_i\text{)}\}$
(Normalized)

→ Makes it easier to compare the shapes of the radiation intensity.



(a) Three-dimensional



(b) Two-dimensional

Figure 4.7 Three- and two-dimensional amplitude patterns for a thin dipole of $l = 1.25\lambda$ and sinusoidal current distribution.

[Balanis, Antenna Theory (2nd Ed), p. 155]

4.5 cont.

Next, we'll determine the directivity + radiation resistance. To do so, we'll need P_{rad}

$P_{rad} = \iint_S \vec{W}_{ave} \cdot d\vec{S}$ or choose large sphere of radius r

$$= \iint \left(\frac{\eta |I_0|^2}{8\pi^2 r^2} \left[\frac{\cos(\frac{kr}{2} \cos\theta) - \cos(\frac{kr}{2})}{\sin\theta} \right]^2 \right) r^2 \sin\theta d\theta d\phi$$

$$= \frac{\eta |I_0|^2}{8\pi^2} \int_{\phi=0}^{2\pi} d\phi \int_{\theta=0}^{\pi} \frac{[\cos(\frac{kr}{2} \cos\theta) - \cos(\frac{kr}{2})]^2}{\sin\theta} d\theta$$

$$P_{rad} = \frac{\eta |I_0|^2}{4\pi} \int_{\theta=0}^{\pi} \frac{[\cos(\frac{kr}{2} \cos\theta) - \cos(\frac{kr}{2})]^2}{\sin\theta} d\theta$$

OR

Not bad numerically, but difficult analytically

Euler's Constant

$$P_{rad} = \frac{\eta |I_0|^2}{4\pi} \left\{ \begin{aligned} &0.5772 + \ln(kr) - C_i(kr) \\ &+ \frac{1}{2} \sin(kr) [S_i(2kr) - 2S_i(kr)] \\ &+ \frac{1}{2} \cos(kr) [0.5772 + \ln(\frac{kr}{2}) + C_i(2kr) - 2C_i(kr)] \end{aligned} \right\}$$

where $C_i()$ + $S_i()$ are the cosine + sine integrals

$$C_i(x) = -\int_x^{\infty} \frac{\cos y}{y} dy \quad + \quad S_i(x) = \int_0^x \frac{\sin y}{y} dy$$

Euler-Mascheroni constant (i.e., Euler's constant) = 0.5772156649

4.5 cont.

Now, we can get the radiation resistance

$$R_r = \frac{2 P_{rad}}{|I_0|^2} = \frac{\eta}{2\pi} \int_{\theta=0}^{\pi} \frac{[\cos(\frac{kl}{2} \cos \theta) - \cos(\frac{kl}{2})]^2}{\sin \theta} d\theta$$

$$(4-70) \quad R_r = \frac{\eta}{2\pi} \left\{ \begin{array}{l} \leftarrow C \text{ or Euler's Constant} \\ 0.5772 + \ln(kl) - C_i(kl) + \frac{1}{2} \sin(kl) [S_i(2kl) - 2S_i(kl)] \\ + \frac{1}{2} \cos(kl) [0.5772 + \ln(\frac{kl}{2}) + C_i(2kl) - 2C_i(kl)] \end{array} \right\}$$

$$(4-70a) \quad X_r = X_m = \frac{\eta}{4\pi} \left\{ \begin{array}{l} 2S_i(kl) + \cos(kl) [2S_i(kl) - S_i(2kl)] \\ - \sin(kl) [2C_i(kl) - C_i(2kl) - C_i(\frac{2kl^2}{l})] \end{array} \right\}$$

→ Remember $kl = 2\pi \frac{l}{\lambda}$, a_1 + l can be expressed in terms of λ .
 This makes it convenient to treat kl and $\frac{a}{\lambda}$ as combined variables.
 E.g., $C_i(\frac{2kl^2}{l}) = C_i[2kl(\frac{a}{\lambda})^2]$

The directivity can be found using $D = \frac{4\pi U}{P_{rad}}$

$$D_{max} = D_0 = \frac{4\pi U_{max}}{P_{rad}} \text{ letting } U = \overset{\downarrow \text{constant}}{B_0} F(\theta, \phi) = \frac{\eta |I_0|^2}{8\pi^2} \left[\frac{\cos(\frac{kl}{2} \cos \theta) - \cos(\frac{kl}{2})}{\sin \theta} \right]^2$$

$$So, F(\theta) = \left[\frac{\cos(\frac{kl}{2} \cos \theta) - \cos(\frac{kl}{2})}{\sin \theta} \right]^2 \quad \uparrow \quad F(\theta, \phi)$$

$$D(\theta, \phi) = \frac{4\pi F(\theta, \phi)}{\int_{\phi=0}^{2\pi} \int_{\theta=0}^{\pi} F(\theta, \phi) \sin \theta d\theta d\phi} \quad (2-21)$$

4.5 cont.

This will lead to:

$$D(\theta, \phi) = D(\theta) = \frac{4\pi \left[\frac{\cos(\frac{kr}{2} \cos \theta) - \cos(\frac{kr}{2})}{\sin \theta} \right]^2}{\int_{\phi=0}^{2\pi} d\phi \int_{\theta=0}^{\pi} \underbrace{\left[\frac{\cos(\frac{kr}{2} \cos \theta) - \cos(\frac{kr}{2})}{\sin \theta} \right]^2}_{\text{Same integral again "Q"}} d\theta}$$

Same integral again "Q"

$$D_0 = \frac{2 \{F(\theta)\}_{\max}}{\int_{\theta=0}^{\pi} \frac{[\cos(\frac{kr}{2} \cos \theta) - \cos(\frac{kr}{2})]^2}{\sin \theta} d\theta} = \frac{2 \{F(\theta)\}_{\max}}{Q}$$

$$\text{Where } Q = \left\{ 0.5772 + \ln(kr) - C_i(kr) + \frac{1}{2} \sin(kr) \left[S_i(2kr) - 2S_i(kr) \right] + \frac{1}{2} \cos(kr) \left[0.5772 + \ln\left(\frac{kr}{2}\right) + C_i(2kr) - 2C_i(kr) \right] \right\}$$

Again

$$A_{\text{em}} = \frac{d^2}{4\pi} D_0$$

4.5 cont.

Input Resistance - with finite length dipoles
 the current maximum I_0 will not necessarily
 be at the input terminals (e.g. $l = 3\lambda/4$)

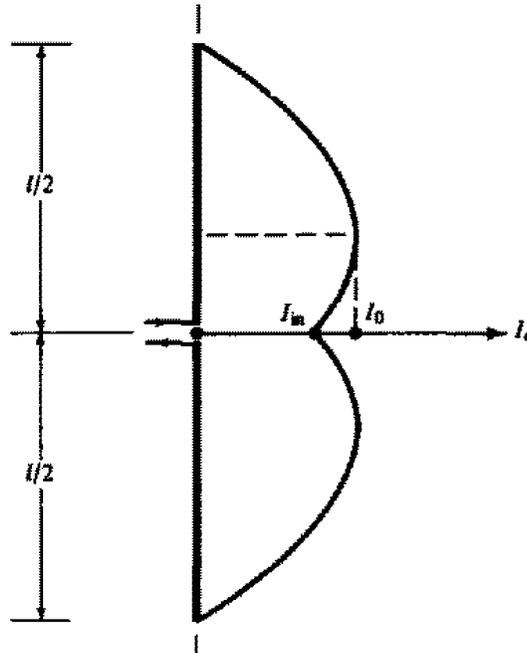


Figure 4.10 Current distribution of a linear wire antenna when current maximum does not occur at the input terminals. (Balanis, Ant Theory (2nd Ed), p.160)

In this case, defining the radiation resistance as $P_{rad} = \frac{1}{2} |I_0|^2 R_r$ ^{maximum current magnitude} will not give the radiation resistance at the input terminals. For a lossless antenna, however, $P_{in} = P_{rad}$

$$\frac{1}{2} |I_{in}|^2 R_{in} = \frac{1}{2} |I_0|^2 R_r$$

$$\hookrightarrow R_{in} = \left[\frac{|I_0|}{|I_{in}|} \right]^2 R_r$$

4.5 cont.

Now $I_{in} = I_0 \sin\left(\frac{k\ell}{2}\right)$, so

$$R_{in} = \frac{R_r}{\sin^2\left(\frac{k\ell}{2}\right)} = \frac{R_r}{\sin^2(\pi \ell/\lambda)}$$

↪ Same for X_{in} & X_r

When $\ell/\lambda = 1, 2, 3, \dots \Rightarrow \sin(n\pi) = 0$

So, in theory, $R_{in} \rightarrow \infty$ ($I_{in} = 0$).

Reality - There is a feed gap at the dipole center + dipoles have finite conductivity and radius \rightarrow so, while R_{in} is very big (or I_{in} very small), it does not go to infinity

\Rightarrow current distribution is not perfectly sinusoidal

\Rightarrow These issues + how to model them analytically are still a topic of discussion. Usually, people use numerical models to analyze specific geometries.

\Rightarrow one consequence is that the so called $\frac{1}{2}$ dipole is actually slightly shorter as a result of these issues

4.6 Half-Wavelength Dipole

$$R_r \approx 73 \Omega \quad \left(\begin{array}{l} \text{varies w/ wire radius} \\ \text{\& } \sigma_{\text{wire}} \end{array} \right)$$

→ close to 75Ω transmission line impedance
(makes matching easy)

→ very widely used

w/ $l = \lambda/2$, the far fields are:

$$E_{\theta} = j\eta \frac{I_0 e^{-jkr}}{2\pi r} \left[\frac{\cos(\pi/2 \cos\theta)}{\sin\theta} \right]$$

$$H_{\phi} \approx j \frac{I_0 e^{-jkr}}{2\pi r} \left[\frac{\cos(\pi/2 \cos\theta)}{\sin\theta} \right]$$

$$\overline{\text{Wave}} = \eta \frac{|I_0|^2}{8\pi^2 r^2} \left[\frac{\cos(\pi/2 \cos\theta)}{\sin\theta} \right]^2 \hat{a}_r$$

$$\approx \eta \frac{|I_0|^2}{8\pi^2 r^2} \sin^3\theta \hat{a}_r$$

$$U = r^2 \overline{\text{Wave}} = \eta \frac{|I_0|^2}{8\pi^2} \left[\frac{\cos(\pi/2 \cos\theta)}{\sin\theta} \right]^2$$

$$\approx \eta \frac{|I_0|^2}{8\pi^2} \sin^3\theta$$

4.6 cont.

get a 2π from $\int_0^{2\pi} d\phi$

$$P_{rad} = \iint U dr = \eta \frac{|I_0|^2}{4\pi} \left(\int_{\theta=0}^{\pi} \frac{\cos^2(\pi/2 \cos\theta)}{\sin\theta} d\theta \right)$$

$\rightarrow 1.2188258$

$$= \eta \frac{|I_0|^2}{8\pi} \int_0^{2\pi} \left(\frac{1-\cos y}{y} \right) dy = \eta \frac{|I_0|^2}{8\pi} \text{Cin}(2\pi)$$

where $\text{Cin}(2\pi) = 2.435$ ^(book) (2.43765339)

\uparrow
TI-684 Math Cael

$$D_0 = 4\pi \frac{U_{max}}{P_{rad}} = 4\pi \frac{\eta \frac{|I_0|^2}{8\pi^2}}{\eta \frac{|I_0|^2}{8\pi} \text{Cin}(2\pi)}$$

$$D_0 = \frac{4}{\text{Cin}(2\pi)} = 1.6409 = 2.15088 \text{ dB}_i$$

$$A_{em} = \frac{d^2}{4\pi} D_0 \approx 0.13058 \lambda^2$$

$$R_r = \frac{2P_{rad}}{|I_0|^2} = \frac{\eta}{4\pi} \text{Cin}(2\pi) \approx 73.08 \Omega$$

$$Z_{in} = Z_{ANT} \approx 73 + j42.5 \Omega \text{ when } l = \lambda/2 = 0.5 \lambda$$

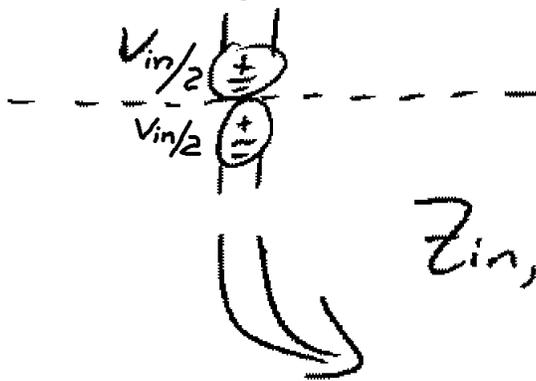
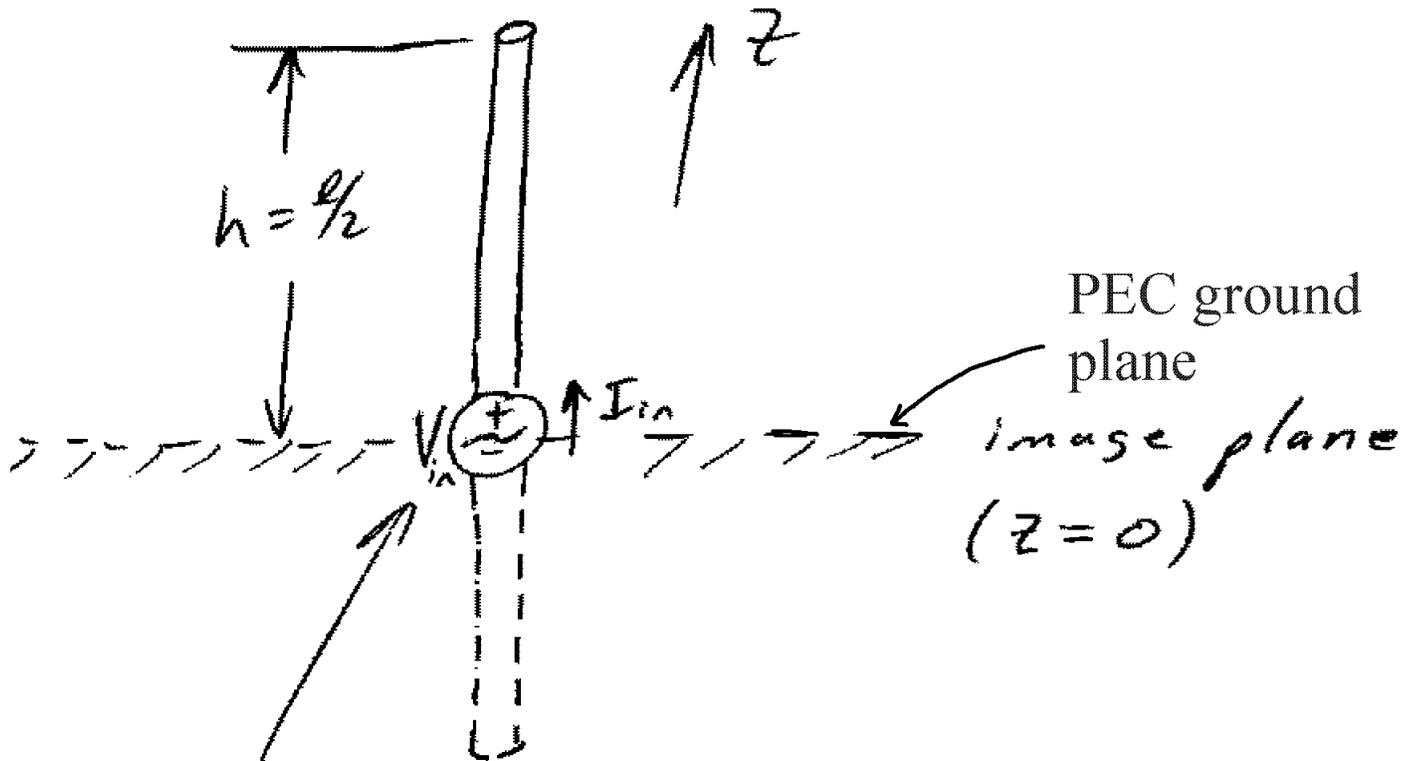
↳ due to non-sinusoidal current distribution actual first resonance occurs when

$$0.47\lambda < l < 0.48\lambda \quad \leftarrow \text{where } X_A = 0$$

bigger a \uparrow

\uparrow small a (thin wire)

Monopoles (Whips)



$$Z_{in, dipole} = \frac{V_{in}}{I_{in}}$$

$$Z_{in, monopole} = \frac{V_{in}/2}{I_{in}} = \frac{1}{2} \frac{V_{in}}{I_{in}}$$

$$Z_{in, monopole} = \frac{1}{2} Z_{in, dipole}$$

Monopoles cont.

What about fields?

The electric + magnetic fields are identical in the positive half-space (i.e., $z > 0$ or $0 \leq \theta < 90^\circ$) to those of the comparable dipole. This implies $\bar{W}_{\text{ave}} + U(\theta, \phi)$ are the same.

What about directivity and gain?

If we have identical fields for the monopole + dipole, then $P_{\text{rad, monopole}} = 0.5 P_{\text{rad, dipole}}$

since we are only doing positive half-space.

$$\begin{aligned} \text{Then, } D_{\text{monopole}} &= \frac{4\pi U_{\text{monopole}}}{P_{\text{rad, monopole}}} \\ &= \frac{4\pi U_{\text{dipole}}}{0.5 P_{\text{rad, dipole}}} = \underline{\underline{2 D_{\text{dipole}}!}} \end{aligned}$$

$$\underline{\underline{D_{\text{monopole}} (\text{dB}) = D_{\text{dipole}} (\text{dB}) + 3.01 \text{ dB}}}$$

$$\Rightarrow \underline{\underline{G_{\text{monopole}} = 2 G_{\text{monopole}} = G_{\text{dipole}} + 3.01 \text{ dB}}}$$

Reality - Over earth (dirt), $G_{\text{monopole}} \approx G_{\text{dipole}}$ due to losses (varies w/ soil params), Also, distorts fields to some extent.