

The Numerical Electromagnetics Code, Ver 2 (NEC-2)

- Based on the numerical solution of integral equations by the Method of Moments (MoM) → single freq. method (time-harmonic assumption)
- Combines an electric field integral equation for modeling thin wires with a magnetic field integral equation for closed perfectly conducting (PEC) surfaces

What can be modeled?

- wires
 - metal patches
 - lumped loads (R, L, C)
 - voltage sources
 - incident EM plane waves
 - transmission lines
 - ground (PEC or lossy dielectric)
- ⋮
⋮
⋮

} single or multiple frequencies

What kind of outputs can you get from NEC?

- currents on structure(s)
- charge distributions
- near field $\bar{E} + \bar{H}$
- radiated (i.e., far-field) $\bar{E} + \bar{H}$
- input impedance
- gain / directivity
- ⋮

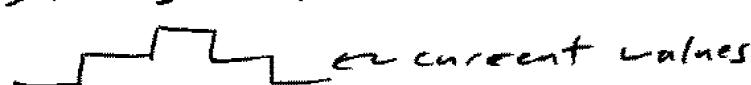
Limitations

- can handle structures up to several λ in size
- Matrices grow as N^2 where N is the # of segments (Memory & speed requirements!)
- Best suited for symmetric structures

Modeling Guidelines

- we are making structures out of straight wire segments and flat surface patches
- critical to select enough segments + patches for accuracy while minimizing their total number (speed + memory concerns)

Wire Modeling → Wire segments

- defined by two end points and its radius
- For curves, try to follow path as closely as possible (piece-wise linear fit) + keep length of piece-wise linear approximation as close as possible to curve being modeled
- Segment length (Δ)
 - ★ → want $\Delta < \lambda_{10}$ (can stretch to λ_8 in a But $\Delta > \lambda_{1000}$ pinch)
 - use smaller segments for critical areas (e.g., curves, feed area, ...)
 - can use longer segments on long straight pieces
 - Current is computed at center of segments (more segments - more current resolution)


Plot a sinusoid for one wavelength using different segment (Δ) sizes

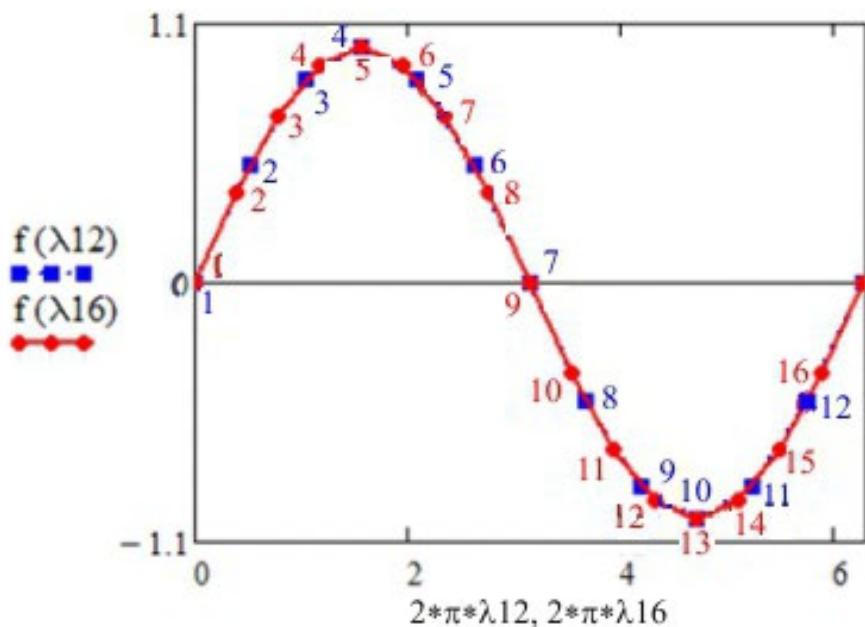
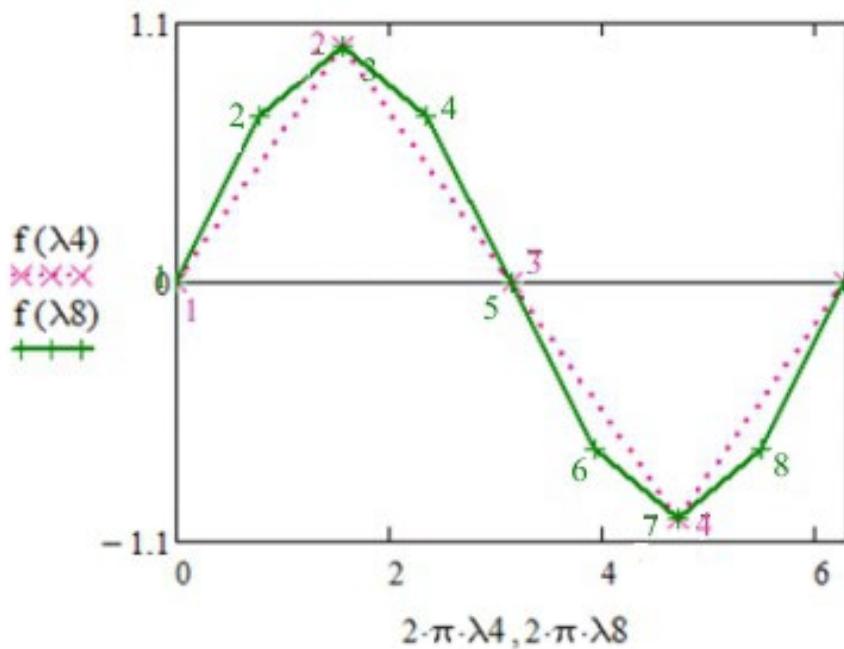
$$\text{4 segments} \quad n4 := 0..4 \quad \lambda_{n4} := \frac{n4}{4}$$

$$\text{8 segments} \quad n8 := 0..8 \quad \lambda_{n8} := \frac{n8}{8}$$

$$f(x) := \sin(2\pi x)$$

$$\text{12 segments} \quad n12 := 0..12 \quad \lambda_{n12} := \frac{n12}{12}$$

$$\text{16 segments} \quad n16 := 0..16 \quad \lambda_{n16} := \frac{n16}{16}$$



Wire Modeling cont.

→ wire radius 'a' is important as NEC makes a "thin wire" approximation that currents are axial not transverse

→ So, what is Thin (filamentary)?

$$\frac{C}{\lambda} = \frac{2\pi a}{\lambda} \ll 1 \quad \begin{array}{l} \text{(rule of thumb is)} \\ \text{1/10 or less is OK} \end{array}$$

→ How are Δ + a inter-related?

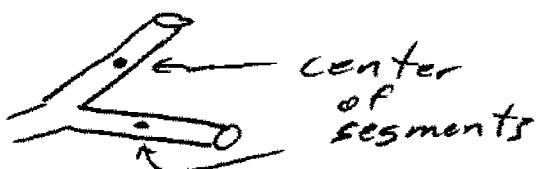
⇒ avoid $\Delta a \leq 0.5$ (hockey puck),

$\Delta a \geq 2$ is better, and $\frac{\Delta}{a} \geq 8$ is best

[use extended kernel (EKC card/command) if $\Delta a < 8$]

→ end points of connected wires should match (a stop factor of $10^{-3} \Delta_{\text{longest}}$ is allowed)

→ Be careful with wires intersecting at acute angles



If the center of one segment is within the volume of another segment → big errors

Example Select a segment length Δ to model a 20.8 cm long dipole antenna made from a 1/2" (O.D.) aluminum rod for a frequency range from 600 MHz to 900 MHz.

From above, $\ell = 20.8 \text{ cm}$ and $d = 2a = 0.5" = 1.27 \text{ cm}$ or $a = 0.25" = 0.635 \text{ cm}$

Find longest wavelength λ_{low} (lowest frequency)

$$\lambda_{\text{low}} = c/f_{\text{low}} = 2.998 \cdot 10^8 / 600 \cdot 10^6 \Rightarrow \lambda_{\text{low}} = 0.49967 \text{ m} = 49.967 \text{ cm}$$

and the dipole is a bit under a half wavelength: $\ell/\lambda_{\text{low}} = 20.8/49.967 \Rightarrow \ell/\lambda_{\text{low}} = 0.4163$

Find shortest wavelength λ_{high} (highest frequency)

$$\lambda_{\text{high}} = c/f_{\text{high}} = 2.998 \cdot 10^8 / 900 \cdot 10^6 \Rightarrow \lambda_{\text{high}} = 0.33311 \text{ m} = 33.311 \text{ cm}$$

and the dipole is a bit over a half wavelength: $\ell/\lambda_{\text{high}} = 20.8/33.311 \Rightarrow \ell/\lambda_{\text{high}} = 0.6244$

Segment length Δ selection process

1) Is the rod/wire ‘thin’, i.e., $2\pi a/\lambda = \pi d/\lambda \ll 1$? Check considering worst case, i.e., shortest wavelength λ_{high} ,

\Rightarrow Yes/pretty good as $\pi d/\lambda_{\text{high}} = \pi(1.27)/33.311 = 0.12 \ll 1$.

2) Want $\Delta < \lambda/10$ and $\Delta > \lambda/1000$ for the worst cases, i.e., $\lambda_{\text{low}}/1000 < \Delta < \lambda_{\text{high}}/10$

$\Rightarrow 0.05 < \Delta < 3.33 \text{ cm}$

3) Also, want $\Delta/a > 2$ at a minimum. $\Delta/a > 8$ is better, then EK command is not needed.

$\Rightarrow \Delta > 2a = 1.27 \text{ cm}$

4) For a finite-length ($\ell > 0.1\lambda$) dipole antenna, we expect a sinusoidal current distribution. Earlier we saw that having 12 segments per wavelength (or more) is desirable for a good representation of a sinusoid. For the worst case, i.e., at λ_{high} , that implies

$\Delta < \lambda_{\text{high}}/12 = 33.311/12 \Rightarrow \Delta < 2.776 \text{ cm}$

5) Doing a logical ‘OR’ on items 2) - 4), we get a narrowed segment range of

$\Rightarrow 1.27 < \Delta < 2.78 \text{ cm}$

6) For a center-fed dipole, we need an **odd integer** number of segments in order to have a centered segment. for the range above, we get

$20.8/1.27 = 16$ segments whereas $20.8/2.78 = 7.5$ segments

7) I will choose to use 11 segments. Therefore, my segment length is:

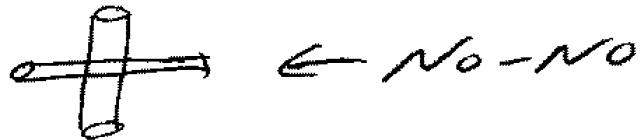
$\Delta = \ell/11 = 20.8/11 \Rightarrow \Delta = 1.891 \text{ cm (DONE!)}$

8) Check Δ/a ratio to see if extended kernel (EK) command is needed.

$\Delta/a = 1.891/0.635 = 2.98 < 8 \Rightarrow$ The EK command is necessary.

More wire segment rules:

- No overlapping (can lead to singular matrices)



- Need segment at network connections + where voltage sources located

- Avoid large changes in wire radius between segments



- Try to separate parallel wires by several radii apart (several diameters better). Also, try to align segments (end points + centers)

- No more than 30 wires connected at a junction

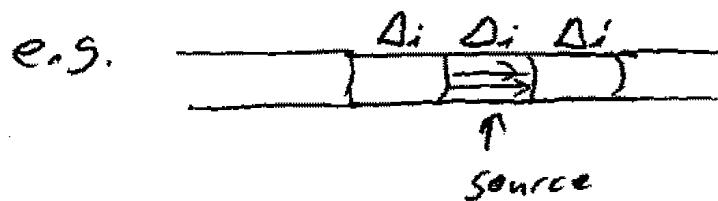
- Try to avoid small loops \textcircled{O}
(circumference $< 3 \times 10^{-4} \lambda$)

Voltage Source Model

→ important as any mistakes show up in the input impedance, gain ...

applied E-field source model $\rightarrow E_i = \frac{V_i}{\Delta_i}$

* * segments on either side of Δ_i should be same length + preferably co-linear



Other possibilities include an elementary current source + a current-slope-discontinuity voltage source (we won't use)

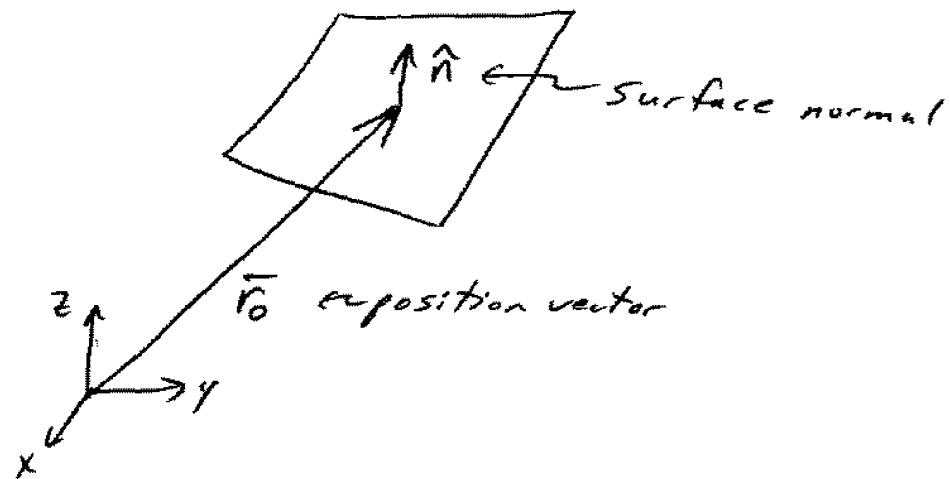
Plane Wave Excitation

→ Linear Polarization

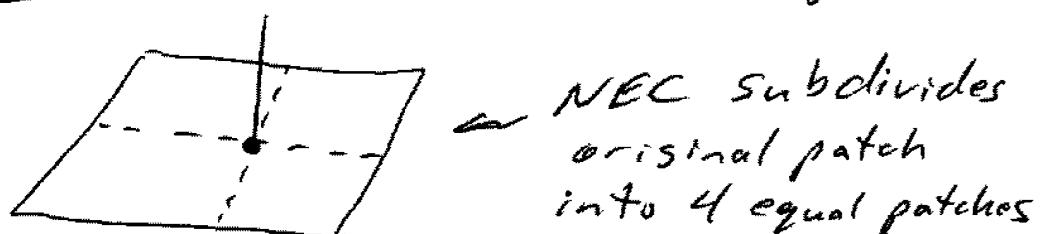
→ RH elliptical } Remember that
 → LH elliptical } circular polarization
 → } is a special case
 → } of elliptical polarization

Surface Modeling

- use small flat surface patches to model conducting surfaces
- * → Closed surfaces *
- Surface patch defined by its center, outward surface normal, and the area



- patch can have arbitrary shape (e.g. square, rectangular, ...)
- a wire must be connected to center of a patch & patch should be square for best results
- only one wire can connect to a patch



Surface patches cont.

- patch size \rightarrow at least 25 patches per λ^2 of area
- \rightarrow max size of any individual patch $\sim 0.04 \lambda^2$
 - \rightarrow can use larger patches in large flat areas
 - \rightarrow smaller patches near curvatures & edges
 - \rightarrow avoid long narrow patches

Ground & Structures

- * PEC ground \rightarrow NEC uses image theory
 - \rightarrow wires should be $> 10^6 \lambda$ over gnd & several radii over gnd
- * Finite conductivity / - structure should be at least several % over ground
- * Some other options available

Inputs to NEC Program

→ commands read from a text file
that is input (NEC asks for names
of input file and output file)

Input files

CM

CM

⋮

CE

} Comment lines

← last comment line

} Structure geometry lines

GE ← end geometry input

} ← Program control command lines
(Excitation, outputs, ...)

NX ← next structure (if desired)

} Repeat above

EN ← end of input file

Command Line format

- Two letter identifier (e.g. CM, GE, GW, ...)
in first two columns
- For CM & CE columns 3-80 are for text
- For other commands columns 3-80 will first have integer parameters (flags) + then floating-point parameters
- can separate numbers by blank spaces(s) or commas
- must enter zeros for unused integer parameters
(on punch cards blanks were the equiv. of zeros)

→ can put a comment at the end of a command line by terminating line w/ !

e.g. GW 17 0 0 -0.25 0 0 0.25 0.001 ! HI

Why 80 columns? From the OLD data card entry (i.e., we used to have to enter commands into computers using cardboard cards w/ holes punched in them that only had 80 columns)

→ 80 column limit may or may not be a problem, depends on how program was compiled

Structure Geometry Inputs

- defines wires + patches (i.e., the structure)
- ends w/ the GE command
- in addition to commands that directly define wires/patches there are commands to move, rotate, copy ... structures
- user can assign tag numbers to wire pieces or sections (useful for placing loads + voltage sources)
 - ITAG = 0 (default, identify segments by abs. #, e.g. 1 → NTOT)
 - ITAG = # (can identify segments by Tag# + seg# on that particular wire piece, e.g. ITAG=3, NSEG=4)

GA - wire arc

GE - end geometry input

GF - read numerical Green's function file

GH - helix / spiral

GM - coordinate transformation

GR - generate cylindrical structure

GS - scale structure dimensions

GW - wire specification

GX - reflection in coordinate plane(s)

SP - surface patch

SM - multiple surface patch

I'll give examples for a couple of the commands

Structure Geometry cont.

Command: End Geometry

GE II=GPFLAG ← ground plane flag

II=0 → no ground plane

II=1 → a ground plane @ $Z=0$
 (x-y plane), currents interpolated
 to image structure

II=-1 → a ground plane @ $Z=0$, no
 current interpolation (goes to
 zero @ ground)

Notes: Structure dimensions must be in
meters (default) when this command
 is executed

ex. GE 0 ! No ground plane

→ Integer flags obey "IN" FORTRAN
 convention (i.e., variables beginning w/ letters
 I, J, K, L, M, + N are assumed to be integers,
 all others are assumed to be floating point,
 unless otherwise specified.)

Structure Geometry cont.

Command : Coordinate Transformation

GM ITG1 NRPT ROX ROT ROZ XS YS ZS IT1 IS1 IT2 IS2

ITG1 → tag #

NRPT → # of new structures (0 indicates to just move the original structure)

ROX → angle in degrees to rotate structure about x-axis (positive # is RH rotation)

ROY
ROZ } ditto for y- & z- axes

XS - amount of shift in x-direction

YS - || y-direction

ZS - || z-direction

IT1-IS2 - leave blank to move entire preceding structure, else start moving w/ segment # given here

Ex. GM 1 1 0.0 0.0 0.0 0.1 0.0 0.0 ! Make one copy of Tag 1 object 0.1 m over in x-dir.

Structure Geometry cont.

Command: Scale Structure Dimensions

GS 0 0 FSCALE

FSCALE → all structure dimensions multiplied
by this parameter

Why? Input everything in inches
then multiply by 0.0254 to
convert to meters.

Ex. GS 0 0 0.0254 ! Multiply all dimensions by 0.0254 to convert inches to meters

Structure Geometry cont.

Command: Straight Wire Specification

GW ITG NS XW1 YW1 ZW1 XW2 YW2 ZW2 RAD
 GC O O RDEL RAD1 RAD2 ← optional (only for tapered wires)

ITG - Tag # assigned to all segments of wire

NS - # of segments

XW1
 YW1 } (X, Y, Z) coordinates of first end
 ZW1 } of wire

XW2
 YW2 } (X, Y, Z) coordinates of second end
 ZW2 } of wire

RAD - radius of wire or 0 for
 tapered wire option

GC

RDEL - ratio of segment length to length
 of previous segment in string

RAD1 - radius of first segment

RAD2 - " " last segment

* positive current assumed for current
 going from first end to second end

Ex. GW 3 24 0.0 0.0 0.0 0.0 0.0 0.3 0.001 ! 1 mm radius wire from origin to z = 0.3 m, Tag #3

Structure Geometry cont.

Command: Wire Arc Specification

GA ITG NS RADA ANG1 ANG2 RAD

ITG - Tag # assigned to all segments
of wire arc

NS - # of segments

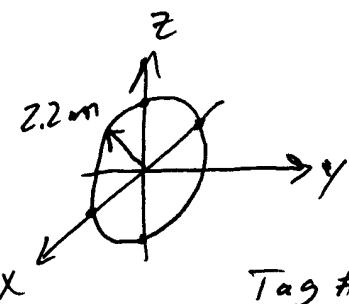
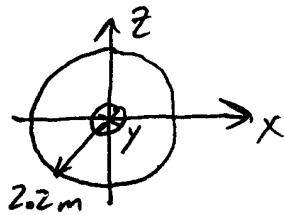
RADA - radius of arc, centered @ origin
w/ axis of symmetry the y-axis,
i.e., arc on x-z plane

ANG1 - angle in degrees wrt to positive
x-axis for first end of arc

ANG2 - angle in degrees wrt to positive
x-axis for second end of arc

RAD - radius of wire

Note: Can use GM command to move
or rotate arc



Ex. GA 1 60 2.2 0 360 0.01 !

Tag #1, 60 segments
2.2 m circular loop
w/ 1cm radius wire

Structure Geometry Cont.

Command: Surface Patch

SP 0 NS X1 Y1 Z1 X2 Y2 Z2

SC 0 0 X3 Y3 Z3 X4 Y4 Z4

optional (used if)
 $NS \neq 0$

NS - patch shape 0 - arbitrary (default)
 1 - rectangular
 2 - triangular
 3 - quadrilateral

NS=0 $\begin{matrix} X1 \\ Y1 \\ Z1 \end{matrix}$ } (X, Y, Z) location of patch center

X2 - elevation angle from x-y plane of outward surface normal

Y2 - azimuth angle from pos. x-axis of outward surface normal

Z2 - patch area

NS=1, 2, or 3

$\begin{matrix} X1 \\ Y1 \\ Z1 \end{matrix}$ } corner 1 of patch

$\begin{matrix} X2 \\ Y2 \\ Z2 \end{matrix}$ } corner 2 of patch

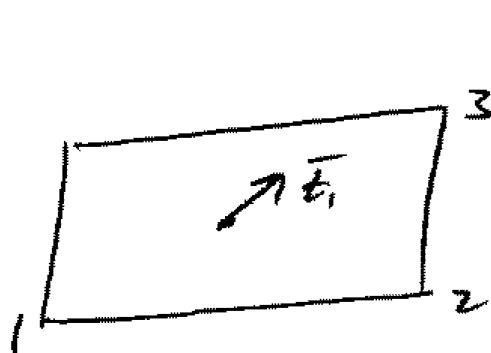
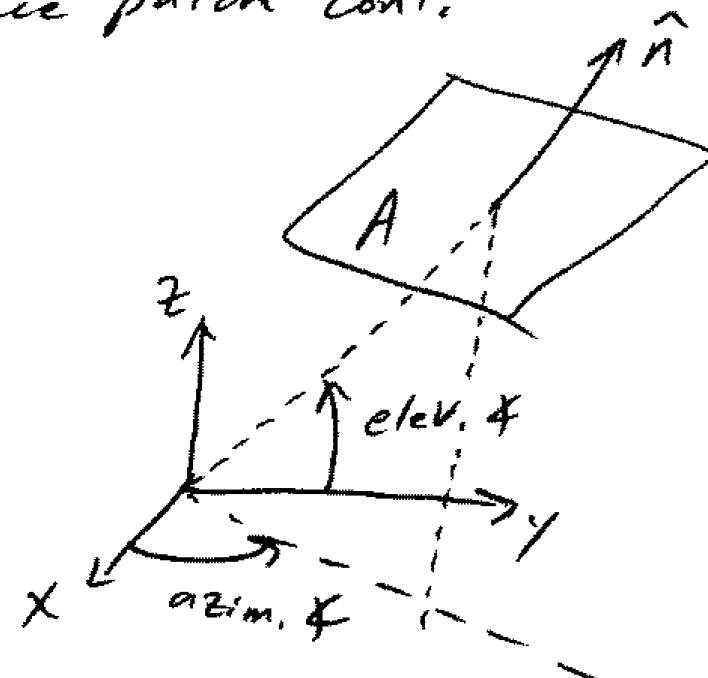
$\begin{matrix} X3 \\ Y3 \\ Z3 \end{matrix}$ } corner 3 of patch

NS=3 only

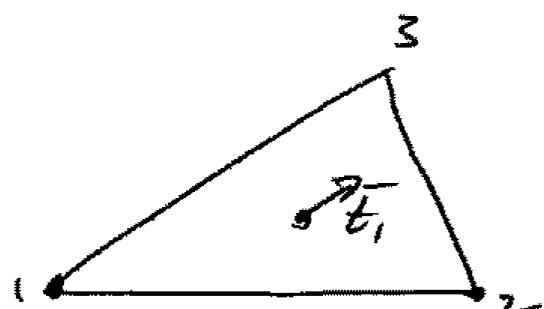
$\begin{matrix} X4 \\ Y4 \\ Z4 \end{matrix}$ } corner 4 of patch

Structure Geometry cont.

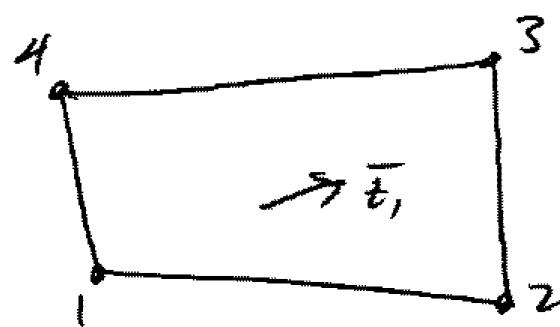
Surface patch cont.



Rectangular
Patch ($NS=1$)



Triangular
Patch ($NS=2$)



Quadrilateral
Patch ($NS=3$)

Structure Geometry cont.

Command: Multiple Patch Surface

SM $NX\ NY\ x1\ y1\ z1\ x2\ y2\ z2$

SC $0\ 0\ x3\ y3\ z3$

SM

$NX \rightarrow$ # of patches in width (from corner 1 to 2)

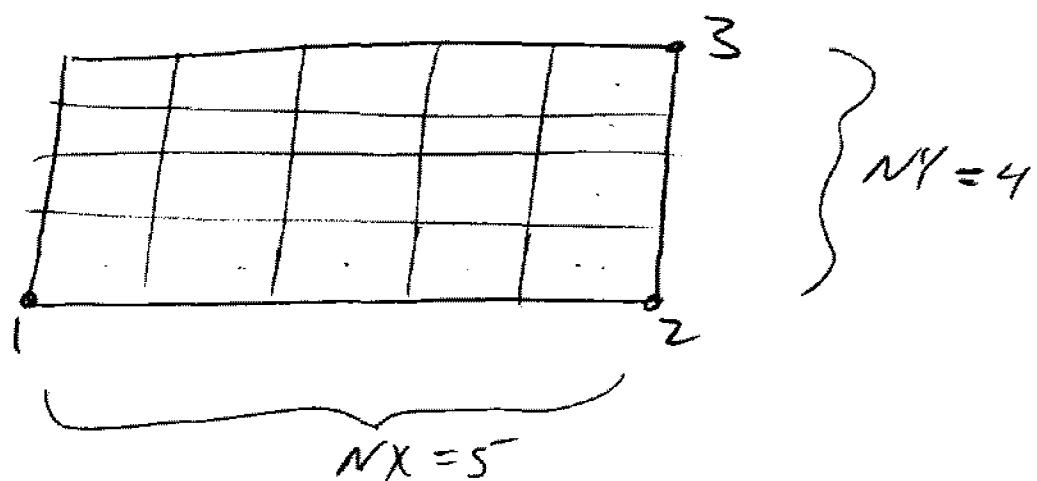
$NY \rightarrow$ # of patches in height (from corner 2 to 3)

x_1
 y_1
 z_1 } (x, y, z) coordinates of corner 1

x_2
 y_2
 z_2 } " corner 2

SC
 x_3
 y_3
 z_3 } " corner 3

Outward
normal
determined
using RHR
on corners
1, 2, 3



Program Control Commands

- Follow geometry commands (i.e. after the GE command)
- Solution options, electrical parameters, and they request data computation + outputs
- Listed by groups where (I) affect entire solution, (II) affect current but not MoM matrix, and (III) only affect results derived from current.

Group I EK - extended thin-wire Kernel flag

FR - frequency specification

GN - ground parameter specification

IH - interaction approx. range

LD - structure impedance loading

Group II EX - structure excitation

NT - two-port network specification

TL - transmission line specification

Group III CP - coupling calculation

EN - end of data flag

GD - addition ground parameter specifications

NE - Near E-field

NH - Near H-field

Program Control cont.

Group III cont.

NX - next structure

PQ - wire charge density print control

PT - wire current print control

RP - radiation pattern request

WG - write Numerical Green's function

XQ - execute command

- No fixed order, however, the commands are read in order + solution will only be affected by commands before solution request.
- If not set, most commands will go to a default value / state (e.g. default frequency is 299.8 MHz or d = 1m). For the most part, the command is omitted.
- Parameters keep set values until changed
- Let's look at the more frequently used Program Control Commands

Program Control cont.

Command : End of run

EN

→ No parameters

→ Marks the end of the input data file

Command : Extended Thin-wire Kernel

EK ITEMPL

ITEMPL = 0 initiate use of extended
thin-wire kernel

= -1 return to standard thin-wire
kernel

→ default is to use standard thin-wire
kernel

→ allows segments where $\lambda_a < \lambda_b$ to
be used

Ex. EK 0 ! Turn on the extended thin-wire kernel.

Program Control cont.

Command: Structure excitation

EX I1 I2 I3 I4 F1 F2 F3 F4 F5 F6

I1 - Type of source

I1=0 applied E-field voltage source

- can
get
RCS
- | | |
|---|---|
| $\left\{ \begin{array}{l} =1 \\ =2 \\ =3 \\ =4 \\ =5 \end{array} \right.$ | linearly polarized incident plane wave
RH elliptic " " " "
LH " " " "
elementary current source
current-slope-discontinuity Voltage source
(located at first end of specified segment) |
|---|---|

For I1=0 or 5:

I2 - tag number of source segment (if I2=0, use absolute segment #)

I3 - number of source segment

I4 - set I4=01 to collect impedances over freq.
loop + print in special format (in Ω
as well as normalized per F3) else
set I4=00

F1 - Real part of voltage

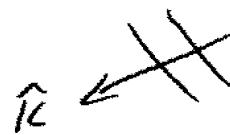
F2 - Imaginary part of voltage

F3 - normalization factor if I4=1, if F3=0
then impedances normalized by the
maximum impedance magnitude

F4, F5, & F6 - leave blank or set to zero

Program Control cont.

EX cont.



For $I1=1,2,3$ (plane wave excitation)

$I2 = \#$ of θ angles desired for incident plane wave

$I3 = \#$ of ϕ angles desired " " " "

$I4 = 0$

$F1 = \# \theta$ (in degrees) to \hat{k} in spherical coor.

$F2 = \# \phi$ (in degrees) " " " "

$F3 =$ polarization angle γ (in degrees) between
 $\hat{a}_0 + \bar{E}$ for linear polarization or the
 major ellipse axis of \bar{E}

$F4 =$ increment (degrees) to step θ variable

$F5 =$ " " " " " ϕ "

$F6 =$ axial ratio ($\frac{\text{major}}{\text{minor}}$)

ex. EX 0 1 4 00 10.0 0.0

↑ ↑ ↑ ↑ ↑ ↑
 voltage tag segment leave $V_s = 10.0 \text{ V}$
 source #1 #4 impedances alone
 $= 10e^{\circ} \text{ V}$

Program Control Cont.

Command : Set frequencies

FR IFRQ NFRQ 0 0 FMHZ DELFRQ

IFRQ - determines type of freq. stepping

IFRQ = 0 linear

IFRQ = 1 multiplicative

NFRQ - # of freq. steps

FMHZ - Starting frequency in MHz

DELFRQ - Δf (MHz) or size of freq. step for IFRQ=0,
multiplication factor for IFRQ=1

ex. FR 0 3 0 0 2000.0 500.0

↑ run NEC @ 2 GHz, 2.5 GHz, + 3 GHz

Note: The pair of zero flags, e.g., '0 0', between NFRQ and FMHZ can NOT be omitted despite the NEC-2 User's Guide saying 'blank'. A blank, i.e., no hole, on an actual cardboard punch card is treated as a zero. However, that is NOT the case when ASCII text files are read into the program.

Program Control cont.

Command : Ground Parameters

GN IPERF NRAOL 0 0 EPSR SIG F3 F4 F5 F6

IPERF - ground flag type

IPERF = -1 nullifies previous ground parameters & sets free-space conditions (omit remaining params)

= 0 lossy ground, refl coefficient approx.

= 1 PEC ground (omit remaining parameters)

= 2 lossy ground, Sommerfeld-Norton method

NRAOL - # of radial ground screen wires (0 for no screen)

EPSR - relative dielectric constant ($\epsilon = \epsilon_r \epsilon_0$) of ground

SIG - conductivity in S/m or Ω^{-1}/m of ground

NRAOL > 0 (ground screen centered @ (0,0,0))

F3 - radius of screen

F4 - radius of wires used to make screen.

NRAOL = 0 F3-F6 used for a second medium, leave blank for single ground medium

Example- GN 0 0 0 0 3.2 0.002 !Lossy dielectric gnd w/ er=3.2, sigma=0.002 S/m

Program Control cont.

Command: Impedance Loading

LD LDTYP LOTAG LOTAGF LOTAGT ZLR ZLI ZLC

LDTYP - use to pick type of load

LDTYP = -1 Use to erase previous loads (short circuit), leave remaining parameters blank

= 0 Series RLC (ω_L, H, F)

= 1 Parallel RLC (ω_L, H, F)

= 2 Series RLC ($\omega_{Lm}, H_{lm}, F_{lm}$)

= 3 Parallel RLC ($\omega_{Lm}, H_{lm}, F_{lm}$)

= 4 Impedance in ohms

= 5 wire conductivity in S/m or σ /m

LOTAG - tag # of wire section w/ load(s), set to zero to use abs. Seg #

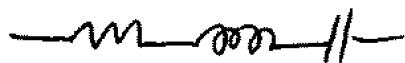
LOTAGF - first segment on LOTAG w/ load, leave equal to zero to load all segments on LOTAG

LOTAGT - last segment on LOTAG w/ load. Must be \geq LOTAGF. Leave equal to zero to load all segments on LOTAG

Program Control cont.

LD cont.

LDTYPE = 0 (Series RLC)



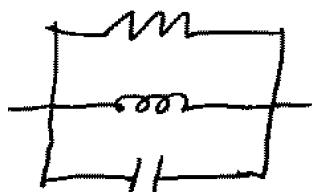
Z_{LR} = resistance (Ω)

Z_{LI} = inductance (H)

Z_{LC} = capacitance (F)

(set to zero for no cap.)

LDTYPE = 1 (Parallel RLC)



Z_{LR} = resistance (Ω)

Z_{LI} = inductance (H)

(Set to zero for no inductor)

Z_{LC} = capacitance (F)

LDTYPE = 2 (series RLC per unit length)

Z_{LR} = resistance (S/m)

Z_{LI} = inductance (H/m)

Z_{LC} = capacitance (F/m)

LDTYPE = 3 (parallel RLC per unit length)

11

LDTYPE = 4 (fixed impedance) Z_{LR} = real resistance (Ω)

→ doesn't change w/ frequency

Z_{LI} = Reactance (Ω)

LDTYPE = 5 (conductivity) $Z_{LR} = \sigma (S/m)$

$Z_{LI} = \mu_r$ (defaults to 1)

Program Control cont.

Command: Next Structure

NX

→ No parameters

→ next line must be CM (Comment Command)

Command: Printing options for currents

PT IPTFLG IPTAG IPTAGF IPTAGT

IPTFLG - printing options

IPTFLG = -2 print all currents (default)

= -1 do NOT print currents

= 0 only print currents on specific segments using next 3 parameters

= 1 }

= 2 }

= 3 }

won't use these options

IPTAG - tag # of wire section (0 for absolute seg #)

IPTAGF - first segment #

IPTAGT - last segment #

Example- PT -1 ! Do NOT print any currents

Example- PT 0 2 10 24 ! ONLY output currents for Tag #2 segments 10 through 24

Note: Use ONLY one PT command in an input file for a single structure, the PT commands overwrite. So, only the last PT command is executed.

Program Control cont.

Command: Radiation Pattern

RP II NTH NPH XNDA THETS PHIS OTH DPH RFLO GMON

II - calculation mode

I1=0 → space-wave field in spherical coord. θ

= 1 → total ground wave in cyl. coord. (won't use)

NTH - # of θ values

NPH - # of ϕ values

XNDA ~ 4 independent flags

X - controls gain format, X=0 → major axis,
minor axis, + total gain, X=1 → vertical,
horizontal, + total gain.

N - normalizes gain. N=0 don't normalize.

N=1 major axis normalized, N=2 minor axis normalized,

N=3 vertical axis normalized, N=4 horizontal axis
normalized, N=5 total gain normalized

O - O=0 power gain, O=1 directive gain

A - ave. power gain, A=0 no averaging,

A=1 ave. gain, A=2 ave. gain computed
+ individual gain + field values suppressed

THETS - first θ angle in degrees

PHIS - " " " " "

OTH - $\Delta\theta$ or θ increment step

DPH - $\Delta\phi$ or ϕ " "

Program Control cont.

RP cont.

RFLO - radial distance in meters from origin, optional - usually left blank or set to zero in which case $\frac{e^{-jkR}}{R}$
Dependence of radiated field omitted

GNOA - gain normalization factor

Ex. RP 0 30 1 0010 0.0 0.0 6.0 0.0 0 0
 ↑

30 θ angles ranging from 0° to 174°
 in 6° increments @ $\phi = 0^\circ$

Notes:

- The RP command immediately initiates program execution. Make sure all needed commands are input prior to the RP command.
- At a single frequency, any number of RP commands may be used in sequence, i.e., you can do multiple radiation pattern ‘cuts’.
- If multiple frequency steps are used (i.e., NFRQ on the FR command is greater than one), only the first RP command will execute as part of the frequency loop. Subsequent RP commands will only execute at the final frequency.

Program Control cont.

Command - Execute

XQ I1

I1 = 0 no radiation patterns

= 1 radiation pattern in x-z plane ($\phi = 0^\circ$)
w/ θ going from 0° to 90° in 1° steps

= 2 ditto in y-z plane ($\phi = 90^\circ$)

= 3 both x-z + y-z planes

→ usually only used if RP command not used (RP command will initiate program soln)

→ handy if all you are interested in are input impedance(s) and current(s).

Example- XQ 0 ! execute program without radiation patterns

Running NEC-2 Instructions

The Numerical Electromagnetic Code version 2 or NEC-2 (freeware) is available on the web. The executable installed locally is ‘nec2d_xs1k5.exe’ (up to 1500 segments); located at F:\NetApps\NetSoft\Nec_viewer. Other versions of the executable are located at F:\NetApps\NetSoft\Nec_viewer\Nec2dXS_VM.

To run NEC-2 off the server using your Windows 10 computer, you will need to:

- 1) Bring up a command (DOS) window by clicking:

Start icon  (lower left corner) → Windows System → Command Prompt,

- 2) go to the appropriate drive & directory in the command window, e.g., type:

c: <enter>, cd ee483 <enter>),

- 3) execute (i.e., run on the f: drive server) the program by typing:

F:\NetApps\NetSoft\Nec_viewer\ nec2d_xs1K5.exe <enter>,

- 4) enter the input filename when prompted (e.g., vee_dipole.txt <enter>),

- 5) enter the output filename when prompted (e.g., vee_dipole.dat <enter>),

- 6) wait for NEC-2 program to finish.

To run NEC on your own computer, you will need to:

- 1) copy executable (i.e., **nec2d_xs1K5.exe**) to your own hard drive from

F:\NetApps\NetSoft\Nec_viewer

- 2) bring up a command (DOS) window on your computer by clicking

Start icon  (lower left corner) → Windows System → Command Prompt,

- 3) go to the appropriate drive & directory in the command window, e.g., type:

c: <enter>, cd ee483 <enter>),

- 4) execute (i.e., run on the f: drive server) the program by typing:

nec2d_xs1K5.exe <enter>,

- 5) enter the input filename when prompted (e.g., vee_dipole.txt <enter>),

- 6) enter the output filename when prompted (e.g., vee_dipole.dat <enter>),

- 7) wait for NEC-2 program to finish.

Input file- vee_dipole.txt

CM PEC VEE-DIPOLE ANTENNA.

CM THIS FILE IS USED TO DETERMINE THE RADIATION PATTERN

CM AT 450 MHz FOR A 60 deg PEC VEE-DIPOLE THAT IS DRIVEN

CM AT THE CENTER. DIMENSIONS ARE: radius a=1mm, arm length h ~ 1 m,

CM SEGMENT LENGTH = h/150. DRIVEN SEGMENT IS #2.

CE

GW 1 3 0.01732 0.0 -0.01 0.01732 0.0 0.01 0.001 ! Driven section (Tag 1)

GW 2 150 0.01732 0.0 0.01 0.866 0.0 0.5 0.001 ! Top arm (Tag 2)

GW 3 150 0.01732 0.0 -0.01 0.866 0.0 -0.5 0.001 ! Bottom arm (Tag 3)

GE 0 ! No ground plane

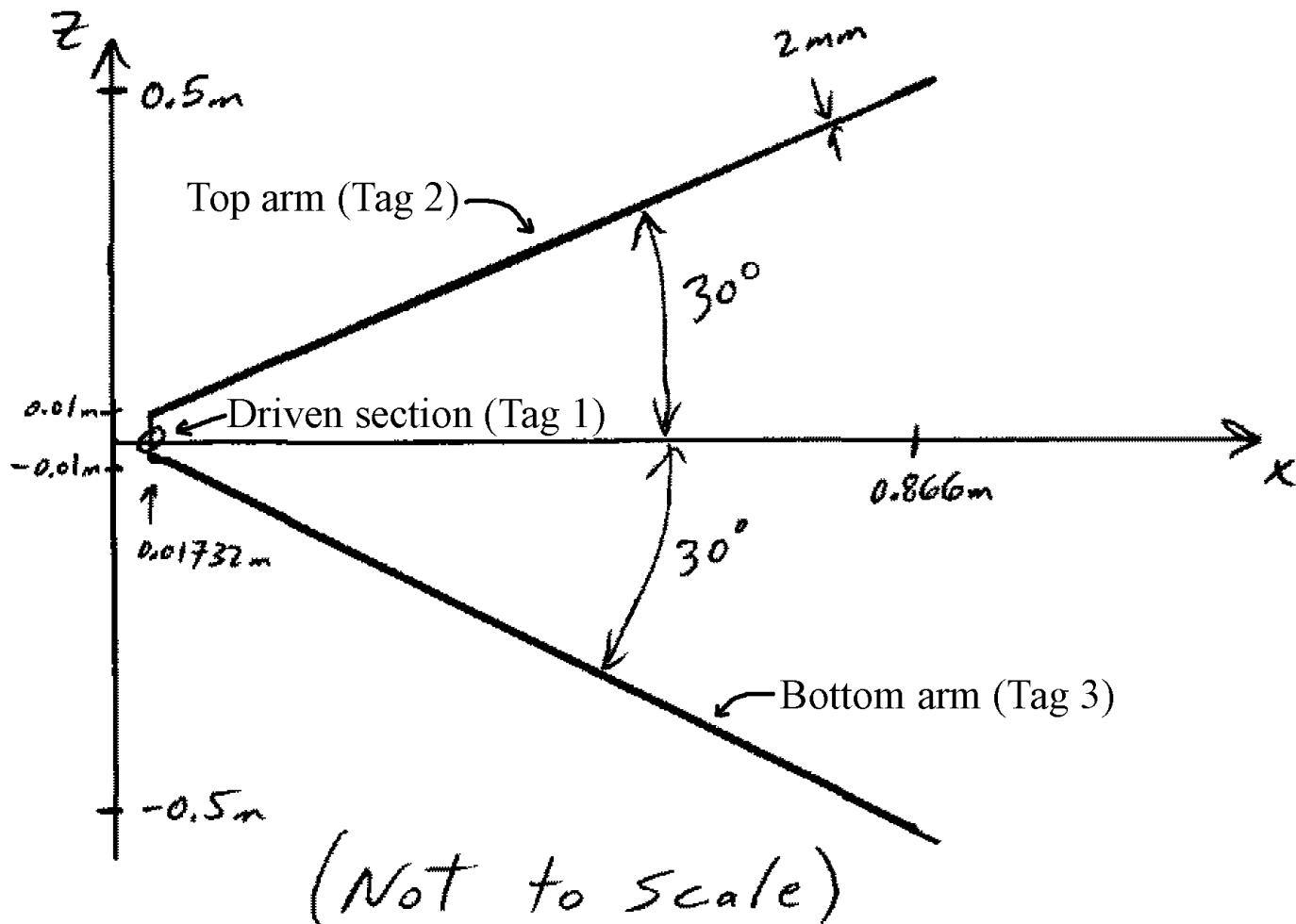
FR 0 1 0 0 450.0 0.0 ! 450 MHz input

EX 0 1 2 0 1.0 0.0 ! 1V input at segment 2 of tag 1

PT -1 ! Do NOT print currents

RP 0 36 1 0000 0.0 0.0 5.0 0.0 ! 0 to 175 deg in theta w/ 5 deg steps

EN



Output file- vee_dipole.dat

1

NUMERICAL ELECTROMAGNETICS CODE (NEC-2D)

* * * * *

- - - - COMMENTS - - - -

PEC VEE-DIPOLE ANTENNA.
THIS FILE IS USED TO DETERMINE THE RADIATION PATTERN
AT 450 MHz FOR A 60 deg PEC VEE-DIPOLE THAT IS DRIVEN
AT THE CENTER. DIMENSIONS ARE: radius a=1mm, arm length h ~ 1 m,
SEGMENT LENGTH=h/150. DRIVEN SEGMENT IS #2.

- - - STRUCTURE SPECIFICATION - - -

COORDINATES MUST BE INPUT IN
METERS OR BE SCALED TO METERS
BEFORE STRUCTURE INPUT IS ENDED

WIRE NO.	X1	Y1	Z1	X2	Y2	Z2	RADIUS	NO. OF SEG.	FIRST SEG.	LAST SEG.	TAG NO.
1	0.01732	0.00000	-0.01000	0.01732	0.00000	0.01000	0.000100	3	1	3	1
2	0.01732	0.00000	0.01000	0.86600	0.00000	0.50000	0.00100	150	4	153	2
3	0.01732	0.00000	-0.01000	0.86600	0.00000	-0.50000	0.00100	150	154	303	3

TOTAL SEGMENTS USED= 303 NO. SEG. IN A SYMMETRIC CELL= 303 SYMMETRY FLAG= 0

- MULTIPLE WIRE JUNCTIONS -
JUNCTION SEGMENTS (- FOR END 1, + FOR END 2)
NONE

- - - - SEGMENTATION DATA - - - -

COORDINATES IN METERS

I+ AND I- INDICATE THE SEGMENTS BEFORE AND AFTER I

SEG. NO.	COORDINATES OF SEG. CENTER			SEG. LENGTH	ORIENTATION		ANGLES RADIUS	WIRE		CONNECTION	DATA	TAG NO.
	X	Y	Z		ALPHA	BETA		I-	I			
1	0.01732	0.00000	-0.00667	0.00667	90.00000	0.00000	0.00100	-154	1	2		1
2	0.01732	0.00000	0.00000	0.00667	90.00000	0.00000	0.00100	1	2	3		1
3	0.01732	0.00000	0.00667	0.00667	90.00000	0.00000	0.00100	2	3	4		1
4	0.02015	0.00000	0.01163	0.00653	30.00073	0.00000	0.00100	3	4	5		2
5	0.02581	0.00000	0.01490	0.00653	30.00073	0.00000	0.00100	4	5	6		2
6	0.03146	0.00000	0.01817	0.00653	30.00073	0.00000	0.00100	5	6	7		2
7	0.03712	0.00000	0.02143	0.00653	30.00073	0.00000	0.00100	6	7	8		2
<snip>												
150	0.84620	0.00000	0.48857	0.00653	30.00073	0.00000	0.00100	149	150	151		2
151	0.85186	0.00000	0.49183	0.00653	30.00073	0.00000	0.00100	150	151	152		2
152	0.85751	0.00000	0.49510	0.00653	30.00073	0.00000	0.00100	151	152	153		2
153	0.86317	0.00000	0.49837	0.00653	30.00073	0.00000	0.00100	152	153	0		2
154	0.02015	0.00000	-0.01163	0.00653	-30.00073	0.00000	0.00100	-1	154	155		3
155	0.02581	0.00000	-0.01490	0.00653	-30.00073	0.00000	0.00100	154	155	156		3
156	0.03146	0.00000	-0.01817	0.00653	-30.00073	0.00000	0.00100	155	156	157		3
157	0.03712	0.00000	-0.02143	0.00653	-30.00073	0.00000	0.00100	156	157	158		3
<snip>												
300	0.84620	0.00000	-0.48857	0.00653	-30.00073	0.00000	0.00100	299	300	301		3
301	0.85186	0.00000	-0.49183	0.00653	-30.00073	0.00000	0.00100	300	301	302		3
302	0.85751	0.00000	-0.49510	0.00653	-30.00073	0.00000	0.00100	301	302	303		3
303	0.86317	0.00000	-0.49837	0.00653	-30.00073	0.00000	0.00100	302	303	0		3

```

***** DATA CARD NO. 1 FR 0 1 0 0 4.50000E+02 0.0 0.0 0.0 0.0 0.0 0.0
***** DATA CARD NO. 2 EX 0 1 2 0 1.00000E+00 0.0 0.0 0.0 0.0 0.0 0.0
***** DATA CARD NO. 3 PT -1 0 0 0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
***** DATA CARD NO. 4 RP 0 36 1 0 0.0 0.0 5.00000E+00 0.0 0.0 0.0 0.0

```

- - - - - FREQUENCY - - - - -

FREQUENCY= 4.5000E+02 MHZ
WAVELENGTH= 6.6622E-01 METERS

APPROXIMATE INTEGRATION EMPLOYED FOR SEGMENTS MORE THAN 1.000 WAVELENGTHS APART

- - - STRUCTURE IMPEDANCE LOADING - - -

THIS STRUCTURE IS NOT LOADED

- - - ANTENNA ENVIRONMENT - - -

FREE SPACE

- - - MATRIX TIMING - - -

FILL= 0.495 SEC., FACTOR= 0.934 SEC.

- - - ANTENNA INPUT PARAMETERS - - -

TAG NO.	SEG. NO.	VOLTAGE (VOLTS)	CURRENT (AMPS)	IMPEDANCE (OHMS)	ADMITTANCE (MHOS)	POWER (WATTS)			
NO.	REAL	REAL	IMAG.	REAL	IMAG.	REAL	IMAG.	(WATTS)	
1	2	1.00000E+00	0.0	5.59042E-04	6.62088E-04	7.44508E+02-8.81739E+02	5.59042E-04	6.62088E-04	2.79521E-04

- - - POWER BUDGET - - -

INPUT POWER = 2.7952E-04 WATTS
RADIATED POWER= 2.7952E-04 WATTS
STRUCTURE LOSS= 0.0000E+00 WATTS
NETWORK LOSS = 0.0000E+00 WATTS
EFFICIENCY = 100.00 PERCENT

- - - RADIATION PATTERNS - - -

-- ANGLES --		- POWER GAINS -			- - - POLARIZATION - - -			- - - E(THETA) - - -		- - E(PHI)	
THETA DEGREES	PHI DEGREES	MAJOR DB	MINOR DB	TOTAL DB	AXIAL RATIO	TIILT DEG.	SENSE	MAGNITUDE VOLTS/M	PHASE DEGREES	MAG. VOLTS/M	PHASE DEG
0.00	0.00	-1.12	-999.99	-1.12	0.00000	0.00	LINEAR	1.13765E-01	110.80	0.0	0.00
5.00	0.00	0.49	-999.99	0.49	0.00000	0.00	LINEAR	1.36929E-01	153.26	0.0	0.00
10.00	0.00	1.93	-999.99	1.93	0.00000	0.00	LINEAR	1.61666E-01	-171.69	0.0	0.00
15.00	0.00	2.75	-999.99	2.75	0.00000	0.00	LINEAR	1.77750E-01	-141.47	0.0	0.00
20.00	0.00	2.83	-999.99	2.83	0.00000	0.00	LINEAR	1.79277E-01	-114.31	0.0	0.00
25.00	0.00	2.07	-999.99	2.07	0.00000	0.00	LINEAR	1.64322E-01	-89.54	0.0	0.00
30.00	0.00	0.35	-999.99	0.35	0.00000	0.00	LINEAR	1.34782E-01	-67.47	0.0	0.00
35.00	0.00	-2.57	-999.99	-2.57	0.00000	0.00	LINEAR	9.63305E-02	-50.13	0.0	0.00
40.00	0.00	-6.78	-999.99	-6.78	0.00000	0.00	LINEAR	5.92935E-02	-44.79	0.0	0.00
45.00	0.00	-9.57	-999.99	-9.57	0.00000	0.00	LINEAR	4.30343E-02	-63.82	0.0	0.00
50.00	0.00	-7.42	-999.99	-7.42	0.00000	0.00	LINEAR	5.50776E-02	-73.03	0.0	0.00
55.00	0.00	-5.03	-999.99	-5.03	0.00000	0.00	LINEAR	7.25510E-02	-56.34	0.0	0.00
60.00	0.00	-3.07	-999.99	-3.07	0.00000	0.00	LINEAR	9.09021E-02	-27.74	0.0	0.00
65.00	0.00	-0.80	-999.99	-0.80	0.00000	0.00	LINEAR	1.18070E-01	3.18	0.0	0.00
70.00	0.00	1.72	-999.99	1.72	0.00000	0.00	LINEAR	1.57822E-01	29.10	0.0	0.00
75.00	0.00	3.97	-999.99	3.97	0.00000	0.00	LINEAR	2.04427E-01	47.86	0.0	0.00
80.00	0.00	5.64	-999.99	5.64	0.00000	0.00	LINEAR	2.47787E-01	60.28	0.0	0.00
85.00	0.00	6.65	-999.99	6.65	0.00000	0.00	LINEAR	2.78274E-01	67.34	0.0	0.00
90.00	0.00	6.98	-999.99	6.98	0.00000	0.00	LINEAR	2.89227E-01	69.64	0.0	0.00
95.00	0.00	6.65	-999.99	6.65	0.00000	0.00	LINEAR	2.78274E-01	67.34	0.0	0.00
100.00	0.00	5.64	-999.99	5.64	0.00000	0.00	LINEAR	2.47787E-01	60.28	0.0	0.00
105.00	0.00	3.97	-999.99	3.97	0.00000	0.00	LINEAR	2.04427E-01	47.86	0.0	0.00
110.00	0.00	1.72	-999.99	1.72	0.00000	0.00	LINEAR	1.57822E-01	29.10	0.0	0.00
115.00	0.00	-0.80	-999.99	-0.80	0.00000	0.00	LINEAR	1.18070E-01	3.18	0.0	0.00
120.00	0.00	-3.07	-999.99	-3.07	0.00000	0.00	LINEAR	9.09021E-02	-27.74	0.0	0.00
125.00	0.00	-5.03	-999.99	-5.03	0.00000	0.00	LINEAR	7.25510E-02	-56.34	0.0	0.00
130.00	0.00	-7.42	-999.99	-7.42	0.00000	0.00	LINEAR	5.50776E-02	-73.03	0.0	0.00
135.00	0.00	-9.57	-999.99	-9.57	0.00000	0.00	LINEAR	4.30343E-02	-63.82	0.0	0.00
140.00	0.00	-6.78	-999.99	-6.78	0.00000	0.00	LINEAR	5.92935E-02	-44.79	0.0	0.00
145.00	0.00	-2.57	-999.99	-2.57	0.00000	0.00	LINEAR	9.63305E-02	-50.13	0.0	0.00
150.00	0.00	0.35	-999.99	0.35	0.00000	0.00	LINEAR	1.34782E-01	-67.47	0.0	0.00
155.00	0.00	2.07	-999.99	2.07	0.00000	0.00	LINEAR	1.64322E-01	-89.54	0.0	0.00
160.00	0.00	2.83	-999.99	2.83	0.00000	0.00	LINEAR	1.79277E-01	-114.31	0.0	0.00
165.00	0.00	2.75	-999.99	2.75	0.00000	0.00	LINEAR	1.77750E-01	-141.47	0.0	0.00
170.00	0.00	1.93	-999.99	1.93	0.00000	0.00	LINEAR	1.61666E-01	-171.69	0.0	0.00
175.00	0.00	0.49	-999.99	0.49	0.00000	0.00	LINEAR	1.36929E-01	153.26	0.0	0.00

***** DATA CARD NO. 5 EN 0 0 0 0.0 0.0 0.0 0.0 0.0 0.0

RUN TIME = 1.538