

4.46 Repeat Problem 4.45 for a center-fed $5\lambda/8$ dipole.

4.45 A lossless, resonant, center-fed $3\lambda/4$ linear dipole, radiating in free-space is attached to a balanced, lossless transmission line whose characteristic impedance is 300 ohms. Assuming $a = 0.03\lambda$, calculate the:

- radiation resistance (referred to the current maximum)
- input impedance (referred to the input terminals)
- VSWR on the transmission line

For parts (a) and (b) use the computer program **Dipole** at the end of the chapter.

- Let $l/a = 64$. Do NOT ignore the reactance in this case. [Hint: See 4-70a & 8-60b.]

For part (a) Also, find radiation reactance. Check/compare with results using NEC-2 assuming $f = 299.8$ MHz and with $\Delta/a \sim 4$. Note: You may use MathCad, Matlab, ... instead of computer program at end of chapter for analytic results.

a) Using (4-67) & (4-70)

$$R_r = \frac{2P_{rad}}{I_0^2} = \frac{\eta}{2\pi} \int_{\theta=0}^{\pi} \frac{[\cos(\frac{kl}{2} \cos \theta) - \cos(\frac{kl}{2})]^2}{\sin \theta} d\theta$$

where $kl = (\frac{2\pi}{\lambda}) \frac{5\lambda}{8} = 1.25\pi$ and $\eta_0 = \sqrt{\frac{\mu_0}{\epsilon_0}} = 376.73031 \Omega$

$$R_r = \frac{376.73}{2\pi} \int_{\theta=0}^{\pi} \frac{[\cos(0.625\pi \cos \theta) - \cos(0.625\pi)]^2}{\sin \theta} d\theta \quad \leftarrow \text{MathCad}$$

$$= 59.481(2.1990257) = \underline{\underline{131.85027 \Omega}}$$

Per (4-70a) or (8-60b)

$$X_r = X_m = \frac{\eta}{4\pi} \left\{ 2S_i(1.25\pi) + \cos(1.25\pi) [2S_i(1.25\pi) - S_i(2.5\pi)] - \sin(1.25\pi) [2C_i(1.25\pi) - C_i(2.5\pi) - C_i(\frac{2.5\pi}{64^2})] \right\}$$

$$\underline{\underline{X_r = 176.423 \Omega}}$$

b) To get input resistance + reactance, use (4-79)/(8-61a) & (8-61b)

$$R_{in} = \frac{R_r}{\sin^2(\frac{kl}{4})} = \frac{131.85}{\sin^2(0.625\pi)} = 154.4722 \Omega + X_{in} = \frac{176.423}{\sin^2(0.625\pi)} = \underline{\underline{206.69 \Omega}}$$

$$\hookrightarrow \underline{\underline{\bar{Z}_{in} = R_{in} + jX_{in} = 154.47 + j206.69 \Omega}}$$

$$c) \Gamma = \frac{Z_{in} - Z_0}{Z_{in} + Z_0} = \frac{(154.47 + j206.69) - 300}{(154.47 + j206.69) + 300} = 0.5063 \angle 100.69^\circ$$

$$\underline{\underline{VSWR = \frac{1+|\Gamma|}{1-|\Gamma|} = \frac{1+0.5063}{1-0.5063} = 3.051}}$$

Check calculations using MATLAB-

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% EE 483/583 problem 4.46(p4_46.m)
% Calculate Rr & Xr for (5/8)lambda linear dipole at current maxima
% Then calculate Zin for antenna at feed. Assume l/a = 64.
clear;clc;close all;
kl = (5/8)*2*pi; % wavenumber*l product
la = 64; % antenna length to radius ratio
eta = 376.730313461; % intrinsic impedance of free space
C = 0.57721566490153286065120900824024310421; % Euler's constant
Z0 = 300; % Characteristic impedance of transmission line
% Use (4-70)/(8-60a) to get radiation resistance at current maxima
Rr = (eta/(2*pi))*(C+log(kl)-cosint(kl)+0.5*sin(kl)*(sinint(2*kl)-2*sinint(kl))...
    +0.5*cos(kl)*(C + log(kl/2) + cosint(2*kl) - 2*cosint(kl)))
% Use (4-70a)/(8-60b) to get reactance at current maxima
Xr = (eta/(4*pi))*(2*sinint(kl)+cos(kl)*(2*sinint(kl)-sinint(2*kl))...
    -sin(kl)*(2*cosint(kl)-cosint(2*kl)-cosint(2*kl/la^2)))
% Use (4-79)/(8-61a) to get input resistance at feed
Rin = Rr/(sin(0.5*kl)*sin(0.5*kl))
% Use (8-61b) to get reactance at feed
Xin = Xr/(sin(0.5*kl)*sin(0.5*kl))
Zin = Rin + j*Xin
% Calculate input reflection coefficient & VSWR
Gamma = (Zin-Z0)/(Zin+Z0)
Gmag = abs(Gamma)
VSWR = (1+Gmag)/(1-Gmag)

```

$$R_r = 131.8503 \, \Omega \text{ and } X_r = 176.4231 \, \Omega$$

$$R_{in} = 154.4722 \, \Omega \text{ and } X_{in} = 206.6925 \, \Omega$$

$$\Rightarrow \boxed{Z_{in} = 154.47 + j206.6925 \, \Omega}$$

$$\Gamma = \text{Gamma} = -0.0939 + 0.4375i, \quad G_{mag} = 0.5063, \quad \text{Gangle} = 100.6927$$

$$\Rightarrow \boxed{\text{VSWR} = 3.0511}$$

Compare/check against NEC-2 simulation-

$$\text{Wavelength } \lambda = c/f = 2.998 \times 10^8 / 299.8 \times 10^6 \Rightarrow \underline{\lambda = 1 \text{ m}}$$

$$\text{Antenna length } \ell = (5/8)\lambda = (5/8)1 \Rightarrow \underline{\ell = 0.625 \text{ m}}$$

$$\text{Antenna radius } a = \ell/64 = 0.625/64 \Rightarrow \underline{a = 0.009765625 \text{ m}}$$

Segment length Δ selection

- Is wire 'thin', i.e., $2\pi a/\lambda \ll 1$? \Rightarrow Yes, $2\pi(0.009765625)/1 = 0.061359 \ll 1 \therefore$
- Want $\Delta < \lambda/10$ and $\Delta > \lambda/1000$, $\Rightarrow 0.001 \text{ m} < \Delta < 0.1 \text{ m}$
- Want minimum $\Delta/a > 2 \Rightarrow \Delta > 2a = 0.01953125 \text{ m}$ which implies $0.625/0.039 \sim 32$ segments.
- **But** $\Delta/a > 8$ is better $\Rightarrow \Delta > 8a = 0.078125 \text{ m}$ which implies $0.625/0.078125 \sim 8$ segments.
- Another consideration is that we want a center-fed dipole \Rightarrow odd integer number of segments.
- choose **15** segments, $\Delta = \ell/15 = 0.625/15 \Rightarrow \underline{\Delta = 0.041667 \text{ m}} \Rightarrow \Delta/a = 4.3$. **Use EK command.**

NEC input file-

```

CM p4_46_la64.txt
CM Lossless (5/8)lambda center-fed dipole antenna
CM at f = 299.8 MHz (lambda = 1 m) with L/a = 64
CM i.e., length = L = 5/8(1) = 0.625 m, and
CM radius a = 0.625/64 = 0.009765625 m.
CM Used 15 segments.  DRIVEN SEGMENT IS #8.
CE
GW 1  15 0.0 0.0 -0.3125 0.0 0.0 0.3125 0.009765625
GE 0  ! No ground plane
EK 0  ! Use extended kernel in simulation
FR 0 1 0 0 299.8 0.0
EX 0 1 8 00 1.0 0.0  ! Center-fed
XQ 0  ! Start simulation
EN

```

Excerpts from NEC output file-

<snip>

```

FREQUENCY= 2.9980E+02 MHZ
WAVELENGTH= 1.0000E+00 METERS

```

<snip>

```

- - - ANTENNA INPUT PARAMETERS - - -
TAG SEG  VOLTAGE (VOLTS)  CURRENT (AMPS)  IMPEDANCE (OHMS)  POWER
NO. NO.  REAL    IMAG.    REAL    IMAG.    REAL    IMAG.    (WATTS)
1   8  1.00E+00  0.0E+00  2.86152E-03-1.75308E-03  2.54096E+02  1.55669E+02
2.86152E-03-1.75308E-03  1.43076E-03

```

```

- - - CURRENTS AND LOCATION - - -
DISTANCES IN WAVELENGTHS

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SEG TAG  COORD OF SEG  CENTER SEG.  - - - CURRENT (AMPS) - - -
NO. NO.   X    Y    Z    LENGTH  REAL    IMAG.    MAG.    PHASE
1   1   0.0  0.0  -0.2917  0.04167  4.8037E-04 -1.0929E-03  1.1938E-03  -66.273
2   1   0.0  0.0  -0.2500  0.04167  1.0464E-03 -2.1994E-03  2.4356E-03  -64.558
3   1   0.0  0.0  -0.2083  0.04167  1.5426E-03 -2.9715E-03  3.3481E-03  -62.565
4   1   0.0  0.0  -0.1667  0.04167  1.9842E-03 -3.4624E-03  3.9907E-03  -60.185
5   1   0.0  0.0  -0.1250  0.04167  2.3526E-03 -3.6429E-03  4.3365E-03  -57.146
6  1   0.0  0.0  -0.0833  0.04167  2.6302E-03 -3.4821E-03  4.3638E-03  -52.934
7   1   0.0  0.0  -0.0417  0.04167  2.8029E-03 -2.8615E-03  4.0056E-03  -45.593
8   1   0.0  0.0   0.0    0.04167  2.8615E-03 -1.7531E-03  3.3558E-03  -31.493
9   1   0.0  0.0   0.0417  0.04167  2.8029E-03 -2.8615E-03  4.0056E-03  -45.593
10 1   0.0  0.0   0.0833  0.04167  2.6302E-03 -3.4821E-03  4.3638E-03  -52.934
11  1   0.0  0.0   0.1250  0.04167  2.3526E-03 -3.6429E-03  4.3365E-03  -57.146
12  1   0.0  0.0   0.1667  0.04167  1.9842E-03 -3.4624E-03  3.9907E-03  -60.185
13  1   0.0  0.0   0.2083  0.04167  1.5426E-03 -2.9715E-03  3.3481E-03  -62.565
14  1   0.0  0.0   0.2500  0.04167  1.0464E-03 -2.1994E-03  2.4356E-03  -64.558
15  1   0.0  0.0   0.2917  0.04167  4.8037E-04 -1.0929E-03  1.1938E-03  -66.273

```

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- - - POWER BUDGET - - -

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INPUT POWER    = 1.4308E-03 WATTS
RADIATED POWER= 1.4308E-03 WATTS
STRUCTURE LOSS= 0.0000E+00 WATTS
NETWORK LOSS   = 0.0000E+00 WATTS
EFFICIENCY     = 100.00 PERCENT <snip>

```

- From NEC, $Z_{in} = 254.096 + j 155.669 \Omega$ (not too close to analytic $154.47 + j 206.69 \Omega$) at the feed point (seg #8) with $\bar{I}_{in} = 3.35583 \angle -31.493^\circ$ mA. However, the maximum currents are $\bar{I}_{max} = 4.3638 \angle -52.934^\circ$ mA occurring at segments 6 & 10, $P_{in} = P_{rad} = 1.4308$ mW, $P_{loss} = 0$, & efficiency = 100 %.

$$R_r = \frac{P_{rad}}{0.5 |\bar{I}_{max}|^2} = \frac{0.0014308}{0.5(0.0043638)^2} \Rightarrow \underline{R_r = 150.27 \Omega} \text{ (near analytic } R_r = 131.85 \Omega),$$

$$\text{Check- } R_{in} = \frac{P_{rad}}{0.5 |\bar{I}_{in}|^2} = \frac{0.0014308}{0.5(0.00335583)^2} \Rightarrow \underline{R_{in} = 254.10 \Omega}$$

Comments-

- A close reading of the text reveals that the analytic formulas assume very thin wires, whereas $\ell/a = 64$ leads to $2\pi a/\lambda = 0.061359$ which is borderline.
- Reality- input impedance of dipoles, particularly reactance, is very sensitive to feed structure.
- In NEC, we are using $\Delta = 0.041667$ m and $a = 0.009765$ m, or $\Delta/a = 4.3$ which requires the extended kernel EK command. Changing the number and length of segments can have a significant effect on results.