Design an optimum (i.e., smallest possible) LPDA with a gain of 7.5 dBi and input impedance of $75 \Omega$ to cover the over-the-air television channels $14-51$ in the ultra high frequency (UHF) band. Use booms with a $5 / 8$ inch outer diameter and the available copper/brass tubing/pipes listed in the table given with the largest elements having a $1 / 2$ inch outer diameter.
a) Tabulate design specifications
b) Show complete design procedure (e.g., design figures, spreadsheets, ...) in a fashion similar to examples given in class.
c) Make a scale drawing(s) of the final antenna design (i.e., show booms \& transmission line) that a machinist could take and use to build the antenna. Use centimeters for all dimensions. Assume grounded boom will extend 40 cm past longest elements to allow the LPDA to be attached to an antenna mast. Allow 2 cm past the shortest elements and the longest element on the non-grounded boom for feed attachment and/or mechanical strength.
a)

1. Select or specify design parameters
a. Desired directivity (gain) $\quad \Rightarrow \quad \underline{7.5 ~ d B i}$
b. Frequency range $\left(f_{\text {high }}\right.$ and $\left.f_{\text {low }}\right)$ -

Per https://en.wikipedia.org/wiki/North American television frequencies, the UHF Channel 14 lower edge is at 470 MHz while Channel 51 upper edge is at 698 MHz $\Rightarrow \quad$ liow $=470 \mathrm{MHz} \& \underline{\text { high }}=698 \mathrm{MHz}$
c. Desired input impedance $R_{0}$ (real) $\quad \Rightarrow \quad \boldsymbol{R}_{\mathbf{0}} \equiv \mathbf{7 5} \Omega$

| Parameter | Value(s) |
| :---: | :---: |
| Directivity/gain | 7.5 dBi |
| Frequency band/range | $470-698 \mathrm{MHz}$ |
| Input impedance | $75 \Omega$ |

b)
2. Use graph (Figure 11.13) on following page, which shows contours of constant directivity versus $\sigma$ (relative spacing) and $\tau$ (scale factor), to select $\sigma$ and $\tau$ for the desired directivity. $\quad \Rightarrow \quad \underline{\sigma=0.149}$ and $\underline{\tau=0.822}$
3. Calculate the apex half angle $\alpha$ using-

$$
\begin{aligned}
& \alpha=\tan ^{-1}\left(\frac{1-\tau}{4 \sigma}\right)=\tan ^{-1}\left(\frac{1-0.822}{4(0.149)}\right) \Rightarrow \underline{\alpha=16.629^{\circ}} \\
& \text { apex angle } \Rightarrow \underline{2 \alpha=33.257^{\circ}}
\end{aligned}
$$



Figure 11.13 Computed contours of constant directivity versus $\sigma$ and $\tau$ for log-periodic dipole arrays. [Balanis $4^{\text {th }}$ Edn., p. 609]
4. Find length $l_{1}$ of the longest element of LPDA

- take length in wavelengths from graph below since we are using optimum $\sigma$ and $\tau$;

$$
\lambda_{\max }=c / f_{\text {low }}=2.998 \times 10^{8} / 470 \times 10^{6}=63.7872 \mathrm{~cm} \quad \Rightarrow \quad \underline{\boldsymbol{l}_{1}}=\mathbf{0 . 5 8 1} \lambda_{\max }=\mathbf{3 7 . 0 6 0} \mathrm{cm}
$$



Measured length, normalized by $\lambda_{\max }$, of longest dipole in LPDA versus optimum $\sigma$ and $\tau$.
5. Find length $l_{N}$ of the shortest element of the LPDA

- take length in wavelengths from graph where $\lambda_{\min }=c / f_{\text {high }}$ is the wavelength at the highest frequency in the desired frequency range.

$$
\lambda_{\min }=c / f_{\text {high }}=2.998 \times 10^{8} / 698 \times 10^{6}=42.9513 \mathrm{~m} \quad \Rightarrow \quad \underline{\boldsymbol{l}_{N}}=\mathbf{0 . 2 2 5} \boldsymbol{\lambda}_{\min }=\mathbf{9 . 6 6 4} \mathbf{c m}
$$



Estimated length, normalized by $\lambda_{\min }$, of shortest dipole in LPDA versus $\sigma$ and $\tau$.
6. Calculate location $R_{1}$ of longest element (as measured from the apex)-

$$
R_{1}=\frac{l_{1}}{2} \cot (\alpha)=\frac{37.0604}{2 \tan \left(16.629^{\circ}\right)} \Rightarrow \underline{R_{1}=62.045 \mathrm{~cm}}
$$

7. Calculate the total bandwidth $B_{s}$, includes additional bandwidth $B_{\text {ar }}$ due to active region, using the specified bandwidth $B$ -

$$
\begin{array}{r}
B=f_{\text {high }} / f_{\text {low }}=698 \mathrm{MHz} / 470 \mathrm{MHz} \Rightarrow \underline{\boldsymbol{B}=\mathbf{1 . 4 8 5 1 1}} \\
B_{\mathrm{ar}}=1.1+7.7(1-\tau)^{2} \cot (\alpha)=1.1+7.7(1-0.822)^{2} \cot \left(16.629^{\circ}\right)=\underline{\mathbf{1 . 9 1 6 8 8}} \\
B_{s}=B_{\mathrm{ar}} \cdot B=1.91688 \cdot 1.48511=\underline{\mathbf{2 . 8 4 6 7 7}}
\end{array}
$$

8. Calculate the approximate number $N$ of elements required for design

$$
N=1+\log _{10}\left(B_{s}\right) / \log _{10}(1 / \tau)=1+\log _{10}(2.84677) / \log _{10}(1 / 0.822)=6.33 \quad \Rightarrow \quad \underline{N} \approx \underline{6}
$$

9. Calculate the approximate distance $L_{\mathrm{T}}$ between the longest and shortest elements.

$$
L_{T}=\frac{l_{1}}{2}\left(1-1 / B_{s}\right) \cot (\alpha)=\frac{37.06}{2}\left(1-\frac{1}{2.84677}\right) \cot \left(16.629^{\circ}\right) \quad \Rightarrow \quad \underline{L_{T}=40.25 \mathrm{~cm}}
$$

10. Calculate the location $R_{2}$ (from the apex) and length $l_{2}$ of the second longest element using the scale factor $\tau, R_{1}$, and $l_{1}$ -

$$
R_{2}=R_{1} \tau=62.045(0.822) \quad \Rightarrow \quad \underline{\boldsymbol{R}_{2}}=\mathbf{5 1 . 0 0 1} \mathbf{~ c m}
$$

and

$$
l_{2}=l_{1} \tau=37.06(0.822) \Rightarrow \underline{\boldsymbol{l}_{2}}=\mathbf{3 0 . 4 6 4} \mathbf{~ c m}
$$

11. Recursively calculate the location $R_{\mathrm{n}+1}$ and length $l_{\mathrm{n}+1}$ of the $\mathrm{n}+1^{\text {th }}$ element(s) using the scale factor $\tau, R_{\mathrm{n}}$, and $l_{\mathrm{n}}-$ e.g., $R_{\mathrm{n}+1}=R_{\mathrm{n}} \tau=R_{\mathrm{n}}(0.822) \quad \& \quad l_{\mathrm{n}+1}=l_{\mathrm{n}} \tau=l_{\mathrm{n}}(0.822)$. Stop when $l_{\mathrm{n}+1}$ is less than or equal to $l_{\mathrm{N}}$ (calculated in step 5.).
12. Count actual number of elements and calculate actual length of LPDA (compare to approximate calculations in steps 8. \& 9.).

- Steps 10-12 done using MS-Excel spreadsheet shown below.

| Steps 10. \& 11. |  | Calculate: $\boldsymbol{R}_{\mathrm{n}+1}=\boldsymbol{R}_{\mathrm{n}} * \tau$ and $l_{\mathrm{n}+1}=l_{\mathrm{n}} * \tau$ |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | where $\tau=$ | 0.822 |  |  |  |  |
| $n$ | $l_{n}(\mathrm{~cm})$ | $\boldsymbol{R}_{\boldsymbol{n}}(\mathrm{cm})$ |  |  |  |  |  |  |
| 1 | 37.06038 | 62.04491 |  |  |  |  |  |  |
| 2 | 30.464 | 51.001 |  |  |  |  |  |  |
| 3 | 25.041 | 41.923 |  |  |  |  |  |  |
| 4 | 20.584 | 34.461 |  |  |  |  |  |  |
| 5 | 16.920 | 28.327 |  |  |  |  |  |  |
| 6 | 13.908 | 23.284 |  |  |  |  |  |  |
| 7 | 11.432 | 19.140 |  |  |  |  |  |  |
| 8 | 9.398 | 15.733 | Stop since | $l 8<l N$ | 64 cm |  |  |  |
| Step 12. | Actual \# of elements \& |  | $N_{\text {approx }}=6$ |  | $\boldsymbol{N}_{\text {actual }}=\mathbf{8}$ |  |  |  |
|  | antenna length |  | $L_{T}=40.25$ | cm | $L_{\text {actual }}=\boldsymbol{R}_{\mathbf{1}}-\boldsymbol{R}_{\mathbf{8}}=$ |  | 46.312 | cm |

13. Select a length to diameter ratio $K=l / d$ for the elements of the LPDA. This choice is a compromise between mechanical strength for the largest and smallest elements, available tubing sizes, and the selected diameter of the boom.

Choose boom diameter $\underline{\boldsymbol{D}=\mathbf{5 / 8}} \boldsymbol{\prime \prime}=\mathbf{1 . 5 8 7 5} \mathbf{c m}$

$$
\text { If } d_{1}=1 / 2 "=1.27 \mathrm{~cm} \text {, then } K_{1}=l_{1} / d_{1}=37.0604 / 1.27=29.18
$$

$$
\text { If } d_{8}=1 / 8^{\prime \prime}=0.3175 \mathrm{~cm} \text {, then } K_{8}=l_{8} / d_{8}=9.398 / 0.3175=29.6
$$

Select $K$ to be $\sim$ average of the two values above $\Rightarrow \underline{\boldsymbol{K}=\mathbf{2 9 . 3 9}}$.
14. Calculate the diameter $d_{\mathrm{n}}=l_{\mathrm{n}} / K$ for each element. Then, select the closest available tube/pipe/rod diameter to the calculated value.
15. Calculate the actual length to diameter ratio $K_{\mathrm{n}}$ for each element and the average length to diameter ratio $K_{\text {ave }}$ after quantization. Check for unusually large deviations from desired $K$ (may want to go back to step 13. and select another value of $K$ ).

- Steps 14-15 done using MS-Excel spreadsheet shown below.

Step 13. Select $K=29.39$
Step 14. \& 15. $\quad d_{\mathrm{n}}=l_{\mathrm{n}} / K \quad K_{\text {actual }}=l_{\mathrm{n}} / d_{\text {quantized }}$

|  |  | Exact | Quantized |  | Actual | $\Delta \boldsymbol{K}=$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\boldsymbol{n}$ | $\boldsymbol{l}_{\boldsymbol{n}}(\mathbf{c m})$ | $\boldsymbol{d}_{\boldsymbol{n}}(\mathbf{c m})$ | $\boldsymbol{d}_{\boldsymbol{n}}(\mathbf{c m})$ | $\boldsymbol{d}_{\boldsymbol{n}}(\mathbf{i n})$ | $\boldsymbol{K}_{\boldsymbol{n}}$ | $\boldsymbol{K}_{\boldsymbol{n}} \boldsymbol{-} \boldsymbol{K}$ |
| 1 | 37.06038 | 1.261 | 1.2700 | $1 / 2$ | 29.181 | -0.209 |
| 2 | 30.464 | 1.037 | 1.0320 | $13 / 32$ | 29.519 | 0.129 |
| 3 | 25.041 | 0.852 | 0.8730 | $11 / 32$ | 28.684 | -0.706 |
| 4 | 20.584 | 0.700 | 0.7140 | $9 / 32$ | 28.829 | -0.561 |
| 5 | 16.920 | 0.576 | 0.5560 | $7 / 32$ | 30.431 | 1.041 |
| 6 | 13.908 | 0.473 | 0.4760 | $3 / 16$ | 29.219 | -0.171 |
| 7 | 11.432 | 0.389 | 0.3970 | $5 / 32$ | 28.797 | -0.593 |
| 8 | 9.398 | 0.320 | 0.3175 | $1 / 8$ | 29.598 | 0.208 |
|  |  |  | Average $\boldsymbol{K}=$ <br> $\mathbf{2 9 . 2 8 2}$ |  |  |  |

16. Calculate the approximate average characteristic impedance of the active region elements-

$$
Z_{\mathrm{a}}=60 \ln \left(2 X K_{\text {ave }} / \pi\right)=60 \ln [2(0.5378) 29.282 / \pi] \quad \Rightarrow \quad \underline{\boldsymbol{Z}_{\mathrm{a}}}=\mathbf{1 3 8 . 3 0 4 \Omega}
$$

where $X=8 \tau \sigma /(1+\tau)=8(0.822) 0.149 /(1+0.822)=0.5378$.
17. Find the characteristic impedance of the unloaded transmission line $Z_{0}$ for the desired input impedance $R_{0^{-}}$

$$
\begin{aligned}
Z_{0} & =\frac{R_{0}{ }^{2}}{4 Z_{a} X}+R_{0} \sqrt{\left(\frac{R_{0}}{4 Z_{a} X}\right)^{2}+1} \\
& =\frac{75^{2}}{4(138.304) 0.5378}+75 \sqrt{\left(\frac{75}{4(185.8956) 0.5378}\right)^{2}+1} \\
& =\underline{96.254 \Omega}
\end{aligned}
$$

18. Calculate the center-to-center spacing $S$ of the booms using the unloaded, cylindrical, twin-lead transmission line formula-

$$
S=D \cosh \left(Z_{0} / 120\right)=1.5875 \cosh (96.254 / 120) \Rightarrow \underline{S}=\mathbf{2 . 1 2 6 2} \mathbf{~ c m}
$$

where $D$ is the diameter of the booms (assumed to be identical). The air gap $\Delta_{\text {gap }}$ between the inner surfaces of the booms is-

$$
\Delta_{\text {gap }}=S-D=2.1262-1.5875 \Rightarrow \underline{\Delta}_{\text {gap }}=\mathbf{0 . 5 3 9} \mathbf{~ c m}=\mathbf{5 . 3 9} \mathbf{~ m m} .
$$

c) Make a scale drawing(s) of the final antenna design (i.e., show booms \& transmission line) that a machinist could take and use to build the antenna. Use centimeters for all dimensions. Assume grounded boom will need to extend 40 cm past longest elements to allow the LPDA to be attached to an antenna mast. Allow 2 cm past the shortest elements and the longest element on the non-grounded boom for feed attachment and/or mechanical strength.
see following pages

## Perspective View of 8 Element LPDA for UHF Channels 14-51 w/ 7.5 dBi gain

Feeding Coaxial $75 \Omega$
Transmission Line

Feed Point

Not to scale. Other dimensions shown on following views of bottom \& top booms

Table of Dimensions for following top and bottom booms

| $\boldsymbol{n}$ | $\boldsymbol{l}_{\boldsymbol{n}}(\mathbf{c m})$ | $\boldsymbol{d}_{\boldsymbol{n}}(\mathbf{c m})$ | $\boldsymbol{R}_{\boldsymbol{n}}(\mathbf{c m})$ | element-element spacing |  |
| :---: | :---: | :---: | :---: | ---: | :---: |
| 1 | 37.06038 | 1.2700 | 62.04491 |  | $(\mathrm{~cm})$ |
| 2 | 30.464 | 1.0320 | 51.001 | $R_{12}$ | 11.044 |
| 3 | 25.041 | 0.8730 | 41.923 | $R_{23}$ | 9.078 |
| 4 | 20.584 | 0.7140 | 34.461 | $R_{34}$ | 7.462 |
| 5 | 16.920 | 0.5560 | 28.327 | $R_{45}$ | 6.134 |
| 6 | 13.908 | 0.4760 | 23.284 | $R_{56}$ | 5.042 |
| 7 | 11.432 | 0.3970 | 19.140 | $R_{67}$ | 4.145 |
| 8 | 9.398 | 0.3175 | 15.733 | $R_{78}$ | 3.407 |

## Top View of Top Boom



Top View of Bottom Boom


