

## Example Design of a Yagi-Uda Antenna

Problem: Design an antenna with a gain of at least 10 dBi to receive television channel 43 (UHF) using a cable-ready television.

### Design Steps:

1. Select or specify design parameters:

- a. Desired directivity- select **5 element Yagi-Uda antenna** from Table 10.6 which has a directivity of  $9.2 \text{ dBd} = 9.2 + 2.15 = \mathbf{11.35 \text{ dBi}}$  (Note: For a Yagi-Uda antenna, gain  $\approx$  directivity.)
- b. Design Frequency- Channel 43 644-650 MHz , so  **$f = 647 \text{ MHz}$** .
- c. Desired input impedance-  **$R_0 = 75 \Omega$**

2. Select diameter  $d$  of elements and diameter  $D$  of metallic supporting boom (optional, only necessary if a metallic boom is to be used) based on mechanical considerations (e.g., strength, rigidity) and parts availability (refer to Table 1).

Element diameter-  **$d = 1/4'' = 0.635 \text{ cm}$**  (use brass pipe)

Boom diameter-  **$D = 5/8'' = 1.5875 \text{ cm}$**  (use 1/2'' I.D. copper pipe)

3. Calculate design wavelength  $\lambda$ . Use  $\lambda$  to calculate  $s_{12}$  (reflector-driven element spacing) and  $s_{ij}$  [driven-director & director-director spacing(s)] using Table 10.6 values.

$$\lambda = \frac{c}{f} = \frac{3 * 10^8}{647 * 10^6} = 0.4637 \text{ m} = \underline{\underline{46.3679 \text{ cm}}}$$

$$s_{12} = s_{ij} = 0.2\lambda = \underline{\underline{9.274 \text{ cm}}}$$

**Table 10.6** OPTIMIZED UNCOMPENSATED LENGTHS OF PARASITIC ELEMENTS FOR YAGI-UDA ANTENNAS OF SIX DIFFERENT LENGTHS

$d/\lambda = 0.0085$ $s_{12} = 0.2\lambda$		LENGTH OF YAGI-UDA (IN WAVELENGTHS)					
		0.4	0.8	1.20	2.2	3.2	4.2
LENGTH OF REFLECTOR ( $l_1/\lambda$ )		0.482	0.482	0.482	0.482	0.482	0.475
LENGTH OF DIRECTORS, $\lambda$	$l_3$	0.442	0.428	0.428	0.432	0.428	0.424
	$l_4$		0.424	0.420	0.415	0.420	0.424
	$l_5$		0.428	0.420	0.407	0.407	0.420
	$l_6$			0.428	0.398	0.398	0.407
	$l_7$				0.390	0.394	0.403
	$l_8$				0.390	0.390	0.398
	$l_9$				0.390	0.386	0.394
	$l_{10}$				0.390	0.386	0.390
	$l_{11}$				0.398	0.386	0.390
	$l_{12}$				0.407	0.386	0.390
	$l_{13}$					0.386	0.390
	$l_{14}$					0.386	0.390
	$l_{15}$					0.386	0.390
	$l_{16}$					0.386	
	$l_{17}$					0.386	
SPACING BETWEEN DIRECTORS ( $s_{ij}/\lambda$ )		0.20	0.20	0.25	0.20	0.20	0.308
DIRECTIVITY RELATIVE TO HALF-WAVE DIPOLE (dB)		7.1	9.2	10.2	12.25	13.4	14.2
DESIGN CURVE (SEE FIGURE 10.25)		(A)	(B)	(B)	(C)	(B)	(D)

SOURCE: Peter P. Vezbicke, *Yagi Antenna Design*, NBS Technical Note 688, December 1976.

Table 1 Available tubing/pipe/rod sizes

Nominal Diameter		Outer Diameter*	
(inches)	(cm)	(inches)	(cm)
3/32	0.238125	3/32	0.238125
1/8	0.3175	1/8	0.3175
5/32	0.397	5/32	0.397
3/16	0.476	3/16	0.476
7/32	0.556	7/32	0.556
<b>1/4</b>	<b>0.635</b>	<b>1/4</b>	<b>0.635</b>
9/32	0.714	9/32	0.714
5/16	0.794	5/16	0.794
11/32	0.873	11/32	0.873
3/8	0.9525	3/8	0.9525
13/32	1.032	13/32	1.032
7/16	1.111	7/16	1.111
1/2	1.27	1/2	1.27
1/2	1.27	9/16	1.429
<b>1/2</b>	<b>1.27</b>	<b>5/8</b>	<b>1.5875</b>
3/4	1.905	7/8	2.223

\* For brass tubing/pipe/rods, the nominal and outer diameters are the same (i.e., wall thickness is negligible). For copper pipes, the wall thickness is substantial and should be measured as it varies between manufacturers.

4. Calculate  $d/\lambda$ . Is  $0.001 \leq d/\lambda \leq 0.04$ ? If not, go to step 2 and reconsider selection of  $d$ .

$$d/\lambda = 0.635/46.3679 = \underline{\mathbf{0.0137}} \Rightarrow \text{Within } 0.001 \leq d/\lambda \leq 0.04 \text{ range.}$$

5. If a metal boom is used, calculate  $D/\lambda$ . Is  $0.001 \leq D/\lambda \leq 0.04$ ? If not, go to step 2 and reconsider selection of  $D$ .

$$D/\lambda = 1.5875/46.3679 = \underline{\mathbf{0.0342}} \Rightarrow \text{Within } 0.001 \leq D/\lambda \leq 0.04 \text{ range.}$$

6. If  $d/\lambda = 0.0085$ , go to step 11 (no element diameter length corrections required). If  $d/\lambda \neq 0.0085$ , the elements lengths must be corrected. Plot the lengths of the reflector (element 1) and first director (element 3) from Table 10.6 on the appropriate design curves on Figure 10.25 (should fall on or near vertical line drawn from  $d/\lambda = 0.0085$ ). Label these points  $l_1''$  and  $l_3''$  respectively.

On Design curves B at  $d/\lambda = 0.0085$ , plot-

$$\underline{\mathbf{l_1'' = 0.482\lambda}}$$

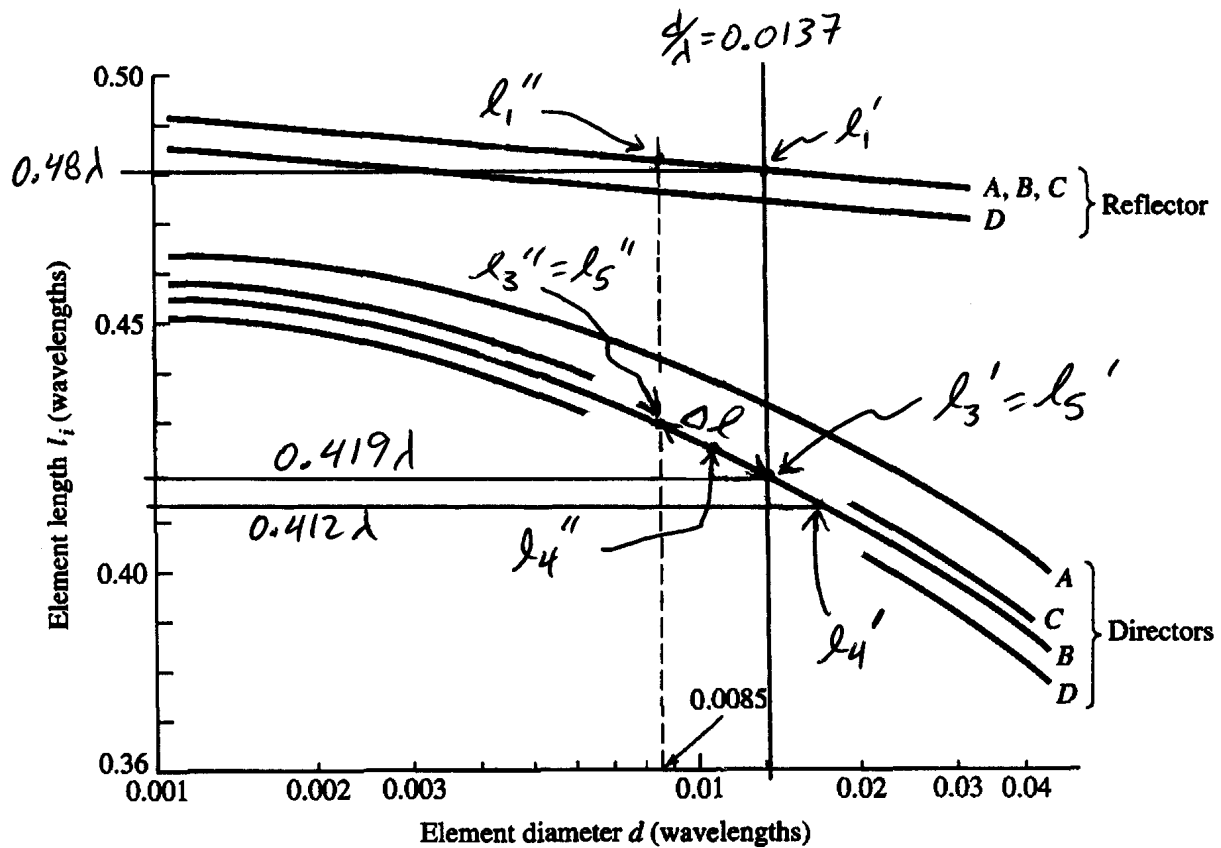
$$\underline{\mathbf{l_3'' = 0.428\lambda}}$$

7. Draw a vertical line from  $d/\lambda = 0.0137$  through reflector and director design curves **B**, where this line intersects the curves is the corrected lengths of the reflector  $l_1'$  and first director  $l_3'$ . The length  $l_3'$  should be used for any other directors that are the same original length as  $l_3$ .

Label and read the corrected (for element diameter) lengths-

$$\underline{\mathbf{l_1' = 0.48\lambda}}$$

$$\underline{\mathbf{l_3' = l_5' = 0.419\lambda}}$$



**Figure 10.25** Design curves to determine element lengths of Yagi-Uda arrays. (SOURCE: P. P. Viezbicke, "Yagi Antenna Design," NBS Technical Note 688, U.S. Department of Commerce/National Bureau of Standards, December 1976)

8. Measure and label the arc length  $\Delta l$  between  $l_3''$  and  $l_3'$  along the design curve.

Using ruler,  $\Delta l = 1.45 \text{ cm}$ .

9. Plot the remaining original optimized director lengths from Table 10.6 on the appropriate director design curve on Figure 10.25 and label  $l_i''$

On director design curve B, plot length of fourth director-

$l_4'' = 0.424\lambda$

10. To find the corrected (for element diameter) length(s) for the remaining directors, move  $\Delta l$  from  $l_i''$  (same direction as between  $l_3''$  and  $l_3'$ ) to the corrected length  $l_i'$ .

Move  $\Delta l = 1.45 \text{ cm}$  from  $l_4'' = 0.424\lambda$ , and read-

$$\underline{l_4' = 0.412\lambda}$$

11. If a metal boom is used (else, skip to next step), the element lengths must be lengthened to compensate for it. On Figure 10.26, draw a vertical line from  $D/\lambda = 0.0342$  through the curve. Draw a horizontal line from the intersection to the left axis of the figure and read the compensation length. The final lengths of the elements (label  $l_i$ ) are found by adding this length to the original (Table 10.6) or the corrected (for element diameter) element lengths.

From Figure 10.26, read-

$$\text{compensation length} = 0.0254\lambda$$

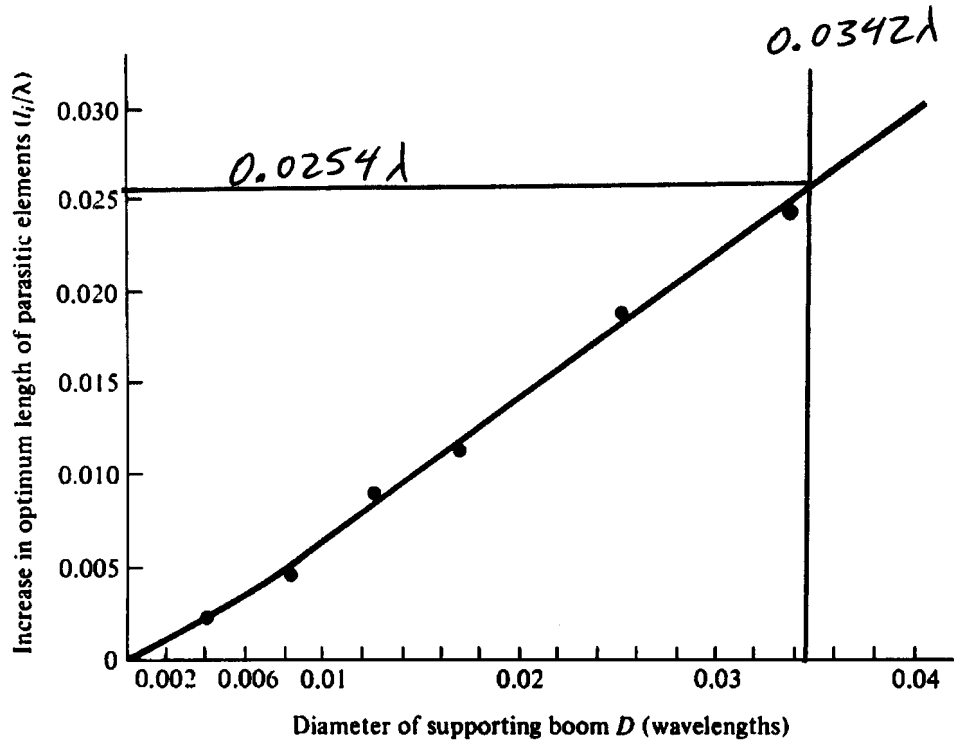
$$l_1 = l_1' + 0.0254\lambda = 0.48\lambda + 0.0254\lambda = 0.5054\lambda = \underline{23.434 \text{ cm}}$$

$$l_3 = l_5 = l_3' + 0.0254\lambda = 0.419\lambda + 0.0254\lambda = 0.4444\lambda = \underline{20.606 \text{ cm}}$$

$$l_4 = l_4' + 0.0254\lambda = 0.412\lambda + 0.0254\lambda = 0.4374\lambda = \underline{20.281 \text{ cm}}$$

12. Design matching network (e.g., Gamma match, ...) to connect the antenna to the selected transmission line. The length of the driven element is empirically adjusted to achieve a match at the design frequency. Typically, it has a length between that of the reflector and the first director.

$$l_1 = 23.434 \text{ cm} < l_2 < l_3 = 20.606 \text{ cm}$$



**Figure 10.26** Increase in optimum length of parasitic elements as a function of metal boom diameter. (SOURCE: P. P. Viezbicke, "Yagi Antenna Design," NBS Technical Note 688, U.S. Department of Commerce/National Bureau of Standards, December 1976)

## 5 element, channel 43 Yagi-Uda antenna w/ boom

