

For a $50\ \Omega$ system, design a 4th-order, lumped-element, linear phase bandpass filter with a center frequency of 2.4 GHz and a bandwidth of 20% using the architecture of Fig. 8.25a.

a) Determine the low-pass filter prototype element values. b) Draw a labeled sketch of the scaled and transformed filter with component values. c) Draw a labeled sketch of the filter in phasor form with $V_s = 1\angle 0^\circ$ V. d) Plot the amplitude response $|V_L|$ in decibels with horizontal dashed lines at $20\log(0.5)$ & $20\log(0.5/\sqrt{2})$ and vertical dashed lines at $2.4 \pm 10\%$ GHz for $1 \leq f \leq 4$ GHz and $-25 \leq |V_L| \leq -5$ dB. Plot $\angle V_L$ (deg) for $1 \leq f \leq 4$ GHz with vertical dashed lines at $2.4 \pm 10\%$ GHz.

a) From Table 8.5, we get the immittances:

$g_0 = g_5 = 1$ (resistors), $g_1 = 1.0598$ (capacitor), $g_2 = 0.5116$ (inductor), $g_3 = 0.3181$ (capacitor), and $g_4 = 0.1104$ (inductor).

TABLE 8.5 Element Values for Maximally Flat Time Delay Low-Pass Filter Prototypes ($g_0 = 1$, $\omega_c = 1$, $N = 1$ to 10)

N	g_1	g_2	g_3	g_4	g_5	g_6	g_7	g_8	g_9	g_{10}	g_{11}
1	2.0000	1.0000									
2	1.5774	0.4226	1.0000								
3	1.2550	0.5528	0.1922	1.0000							
4	1.0598	0.5116	0.3181	0.1104	1.0000						
5	0.9303	0.4577	0.3312	0.2090	0.0718	1.0000					
6	0.8377	0.4116	0.3158	0.2364	0.1480	0.0505	1.0000				
7	0.7677	0.3744	0.2944	0.2378	0.1778	0.1104	0.0375	1.0000			
8	0.7125	0.3446	0.2735	0.2297	0.1867	0.1387	0.0855	0.0289	1.0000		
9	0.6678	0.3203	0.2547	0.2184	0.1859	0.1506	0.1111	0.0682	0.0230	1.0000	
10	0.6305	0.3002	0.2384	0.2066	0.1808	0.1539	0.1240	0.0911	0.0557	0.0187	1.0000

Source: Reprinted from G. L. Matthaei, L. Young, and E. M. T. Jones, *Microwave Filters, Impedance-Matching Networks, and Coupling Structures*, Artech House, Dedham, Mass., 1980, with permission.

b) Given $\Delta = 0.2$ and $\omega_0 = 2\pi(2.4 \times 10^9)$ rad/s. Per Table 8.6 and using (8.64a) & (8.64b) for impedance scaling, each shunt capacitor in the prototype becomes a shunt L & C :

$$C_1 = g_1 = 1.0598 \text{ becomes: } L'_1 = \frac{\Delta R_0}{\omega_0 g_1} = \frac{0.2(50)}{(2\pi)2.4 \times 10^9(1.0598)} \Rightarrow \underline{L'_1 = 0.626 \text{ nH.}}$$

$$\text{and } C'_1 = \frac{g_1}{\omega_0 \Delta R_0} = \frac{1.0598}{(2\pi)2.4 \times 10^9(0.2)50} \Rightarrow \underline{C'_1 = 7.028 \text{ pF.}}$$

$$C_3 = g_3 = 0.3181 \text{ becomes: } L'_3 = \frac{\Delta R_0}{\omega_0 g_3} = \frac{0.2(50)}{(2\pi)2.4 \times 10^9(0.3181)} \Rightarrow \underline{L'_3 = 2.085 \text{ nH.}}$$

$$\text{and } C'_3 = \frac{g_3}{\omega_0 \Delta R_0} = \frac{0.3181}{(2\pi)2.4 \times 10^9(0.2)50} \Rightarrow \underline{C'_3 = 2.109 \text{ pF.}}$$

- Per Table 8.6 and using (8.64a) & (8.64b) for impedance scaling, each series inductor in the prototype becomes a series L & C :

$$L_2 = g_2 = 0.5116 \text{ becomes: } L'_2 = \frac{g_2 R_0}{\omega_0 \Delta} = \frac{0.5116(50)}{(2\pi)2.4 \times 10^9 (0.2)} \Rightarrow \underline{L'_2 = 8.482 \text{ nH.}}$$

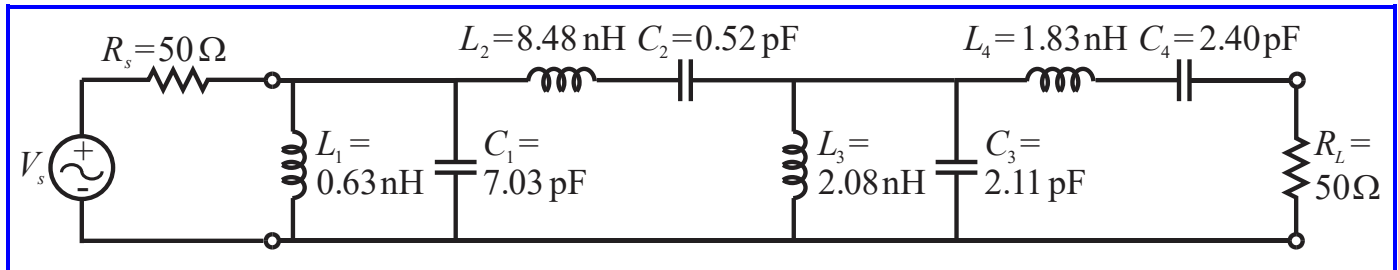
$$\text{and } C'_2 = \frac{\Delta}{\omega_0 g_2 R_0} = \frac{0.2}{(2\pi)2.4 \times 10^9 (0.5116)50} \Rightarrow \underline{C'_2 = 0.518 \text{ pF.}}$$

$$L_4 = g_4 = 0.1104 \text{ becomes: } L'_4 = \frac{g_4 R_0}{\omega_0 \Delta} = \frac{0.1104 (50)}{(2\pi)2.4 \times 10^9 (0.2)} \Rightarrow \underline{L'_4 = 1.830 \text{ nH.}}$$

$$\text{and } C'_4 = \frac{\Delta}{\omega_0 g_4 R_0} = \frac{0.2}{(2\pi)2.4 \times 10^9 (0.1104)50} \Rightarrow \underline{C'_4 = 2.403 \text{ pF.}}$$

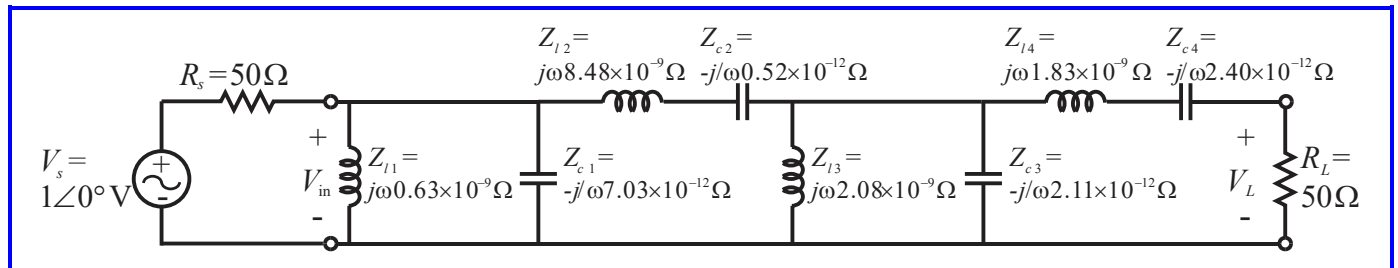
- Per (8.64c), the source resistance $R_s = g_0$ becomes: $R'_s = R_0 g_0 = (50)1 \Rightarrow \underline{R'_s = 50 \Omega.}$
- Per (8.64d), the load resistance $R_L = g_5$ becomes: $R'_L = R_0 g_5 = 50(1) \Rightarrow \underline{R'_L = 50 \Omega.}$

- The resulting **linear phase bandpass** filter circuit with component values is:



- c) From circuits, use $Z_R = R$, $Z_L = j\omega L$, and $Z_C = -j/\omega C$.

The resulting **linear phase bandpass** filter circuit in phasor form is:



d) Using MathCAD

System impedance $Z_0 := 50 \quad \Omega$ $n := 100..400$ $f_n := n \cdot 10^7$

Linear phase lumped element design N = 4 $f_c := 2.4 \cdot 10^9 \quad \text{Hz}$ $\Delta := 0.2$

Table 8.3 LPF prototype $g_0 := 1$ $g_1 := 1.0598$ $g_2 := 0.5116$ $g_3 := 0.3181$

$g_4 := 0.1104$ $g_5 := 1$ $R_S := g_0 \cdot Z_0$ $R_L := Z_0 \cdot g_5$

parallel L & C**series L & C**

$$L_1 := \frac{\Delta \cdot Z_0}{2 \cdot \pi \cdot f_c \cdot g_1} \quad C_1 := \frac{g_1}{Z_0 \cdot \Delta \cdot 2 \pi \cdot f_c} \quad L_2 := \frac{g_2 \cdot Z_0}{2 \cdot \pi \cdot f_c \cdot \Delta} \quad C_2 := \frac{\Delta}{Z_0 \cdot g_2 \cdot 2 \pi \cdot f_c}$$

$$L_3 := \frac{\Delta \cdot Z_0}{2 \cdot \pi \cdot f_c \cdot g_3} \quad C_3 := \frac{g_3}{Z_0 \cdot \Delta \cdot 2 \pi \cdot f_c} \quad L_4 := \frac{g_4 \cdot Z_0}{2 \cdot \pi \cdot f_c \cdot \Delta} \quad C_4 := \frac{\Delta}{Z_0 \cdot g_4 \cdot 2 \pi \cdot f_c}$$

$V_S := 1 \quad \text{V} \quad R_S = 50 \quad \Omega \quad R_L = 50 \quad \Omega$

$L_1 = 6.257 \times 10^{-10} \quad \text{H} \quad C_1 = 7.028 \times 10^{-12} \quad \text{F}$

$L_2 = 8.482 \times 10^{-9} \quad \text{H} \quad C_2 = 5.185 \times 10^{-13} \quad \text{F}$

$L_3 = 2.085 \times 10^{-9} \quad \text{H} \quad C_3 = 2.109 \times 10^{-12} \quad \text{F}$

$L_4 = 1.83 \times 10^{-9} \quad \text{H} \quad C_4 = 2.403 \times 10^{-12} \quad \text{F}$

Series impedance of R_L , C_4 , & L_4 $Z_1(f) := R_L + \frac{1}{(j \cdot 2 \cdot \pi \cdot f \cdot C_4)} + j \cdot 2 \cdot (\pi \cdot f \cdot L_4)$

Parallel impedance of Z_1 , L_3 , & C_3 $Z_2(f) := \left[\frac{1}{Z_1(f)} + \frac{1}{(j \cdot 2 \cdot \pi \cdot f \cdot L_3)} + j \cdot 2 \cdot \pi \cdot f \cdot C_3 \right]^{-1}$

Series impedance of L_2 , C_2 , & Z_2 $Z_3(f) := j \cdot 2 \cdot \pi \cdot f \cdot L_2 + \frac{1}{(j \cdot 2 \cdot \pi \cdot f \cdot C_2)} + Z_2(f)$

Input impedance of BPF filter w/
load $Z_{in}(f) := \left[\frac{1}{Z_3(f)} + \frac{1}{(j \cdot 2 \cdot \pi \cdot f \cdot L_1)} + j \cdot 2 \cdot \pi \cdot f \cdot C_1 \right]^{-1}$

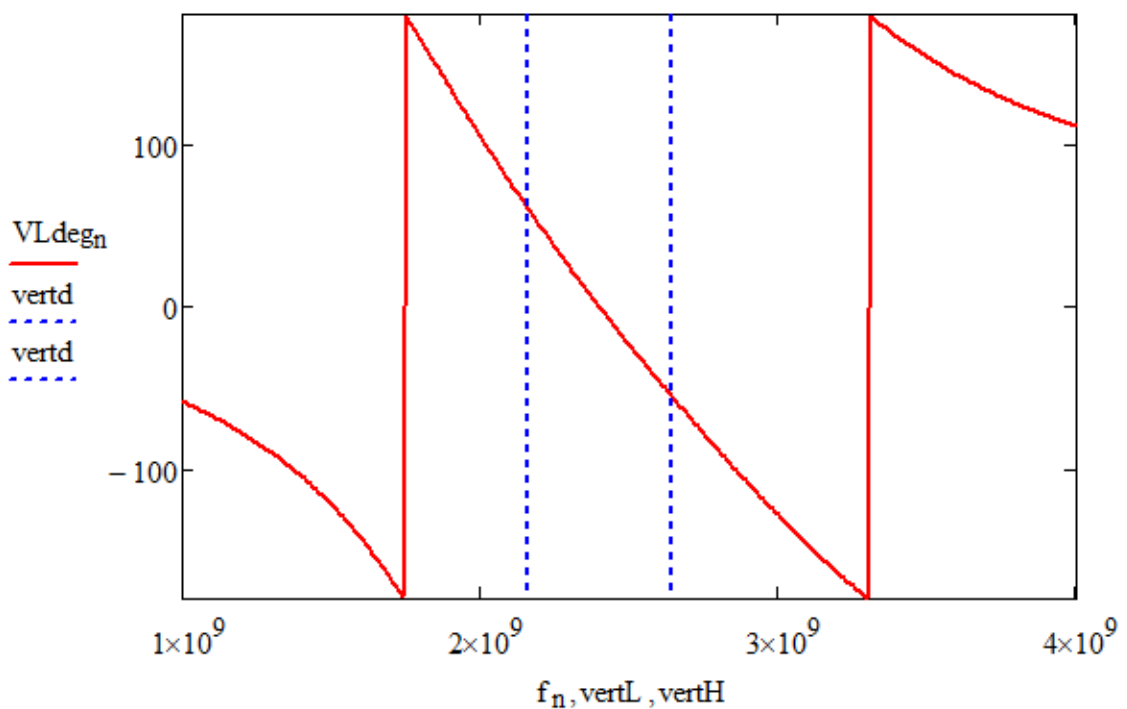
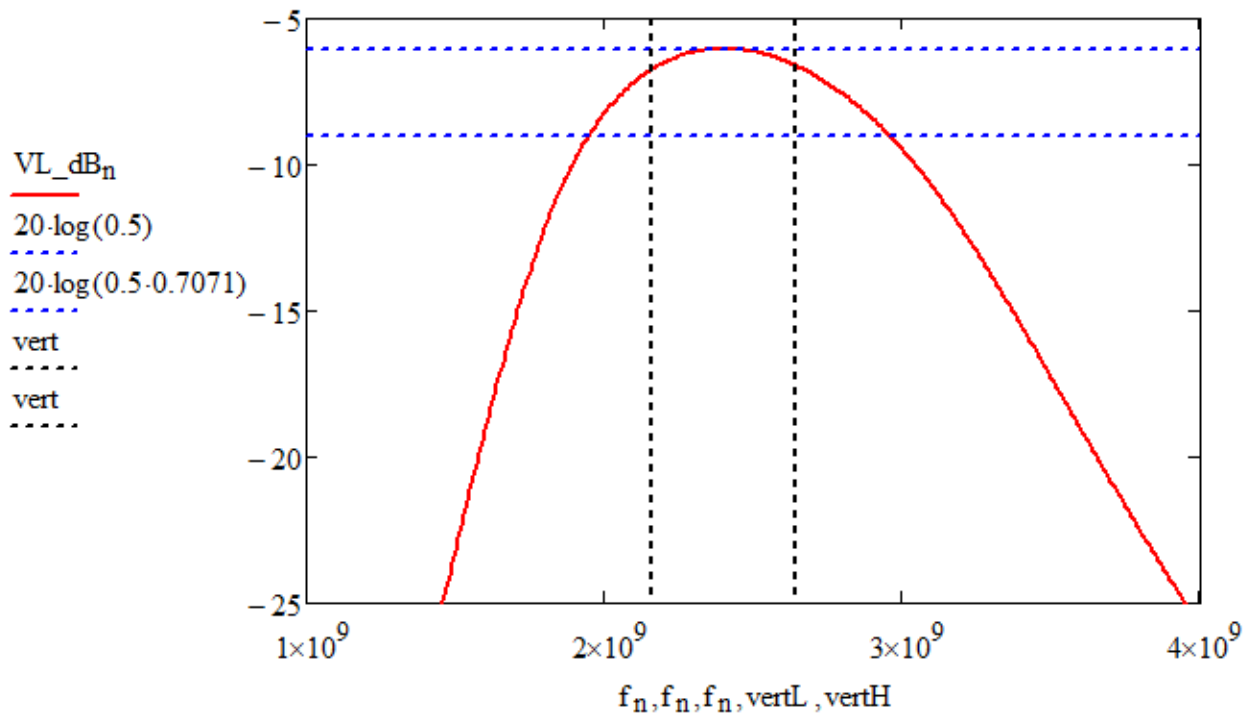
Voltage divisions to get V_{in} & V_{RL} $V_{in}(f) := V_S \cdot \frac{Z_{in}(f)}{R_S + Z_{in}(f)}$

$V_{Z2}(f) := V_{in}(f) \cdot \frac{Z_2(f)}{Z_3(f)} \quad V_{RL}(f) := V_{Z2}(f) \cdot \frac{R_L}{Z_1(f)}$

d) cont.

$$VIN_n := V_{in}(f_n) \quad VL_n := V_{RL}(f_n) \quad VL_dB_n := 20 \cdot \log(|VL_n|) \quad VLdeg_n := \arg(VL_n) \cdot \frac{180}{\pi}$$

$$vertL := \begin{pmatrix} 2.16 \cdot 10^9 \\ 2.16 \cdot 10^9 \end{pmatrix} \quad vertH := \begin{pmatrix} 2.64 \cdot 10^9 \\ 2.64 \cdot 10^9 \end{pmatrix} \quad vert := \begin{pmatrix} -5 \\ -25 \end{pmatrix} \quad vertd := \begin{pmatrix} 180 \\ -180 \end{pmatrix}$$



➤ Note: The linear phase BPF has NOT rolled off 3 dB at $f_c = 2.4 \pm 10\%$ GHz.