

For a $50\ \Omega$ system, design a lumped-element, Butterworth high-pass filter with a cut-off frequency of 2.4 GHz with an attenuation of at least 15 dB at 1.2 GHz using the architecture of Fig. 8.25a. a) Determine the filter order N and the low-pass filter prototype element values. b) Draw a labeled sketch of the scaled and transformed filter with component values. c) Draw a labeled sketch of the filter in phasor form with $V_s = 1\angle 0^\circ\text{ V}$. d) Plot the amplitude response $|V_L|$ in decibels with horizontal dashed lines at $20\log(0.5)$ & $20\log(0.5/\sqrt{2})$ and a vertical dashed line at 2.4 GHz for $0 \leq f \leq 5\text{ GHz}$ & $-25\text{ dB} \leq |V_L| \leq 0$.

- a) Since ω is at $0.5\omega_c$ for the HPF, calculate normalized frequency for LPF prototype at $2\omega_c$ $|\omega/\omega_c| - 1 = |2\omega_c/\omega_c| - 1 = 1$. From Figure 8.26, we see that an LP prototype filter of order $N=3$ is needed to meet the 15 dB attenuation specification.

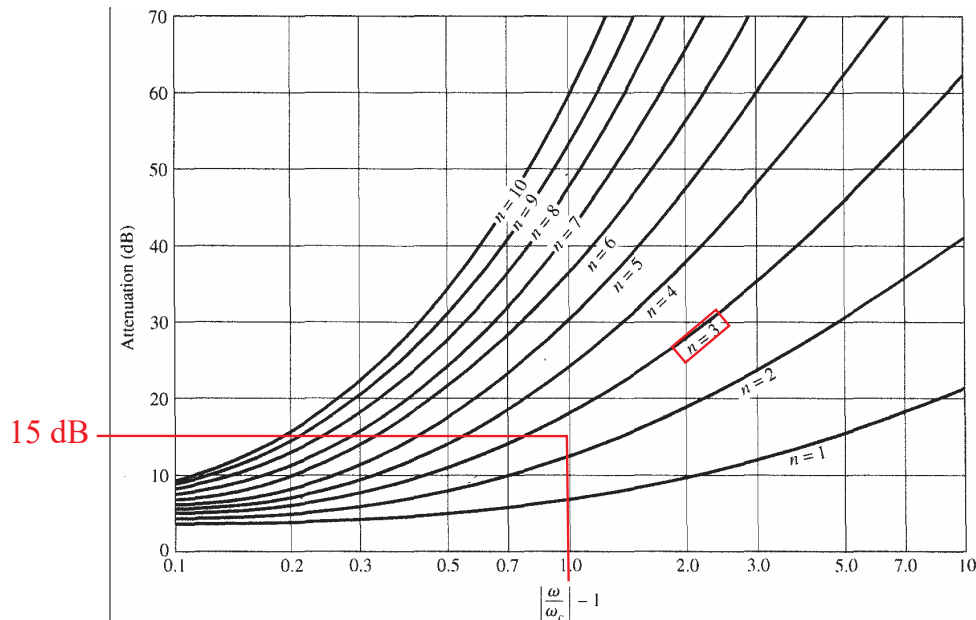


FIGURE 8.26 Attenuation versus normalized frequency for maximally flat filter prototypes. Adapted from G. L. Matthaei, L. Young, and E. M. T. Jones, *Microwave Filters, Impedance-Matching Networks, and Coupling Structures*, Artech House, Dedham, Mass., 1980, with permission.

From Table 8.3, we get the immittances:

$g_0 = g_4 = 1$ (resistors), $g_1 = g_3 = 1.0000$ (capacitors), and $g_2 = 2.0000$ (inductor).

TABLE 8.3 Element Values for Maximally Flat Low-Pass Filter Prototypes ($g_0 = 1$, $\omega_c = 1$, $N = 1$ to 10)

N	g_1	g_2	g_3	g_4	g_5	g_6	g_7	g_8	g_9	g_{10}	g_{11}
1	2.0000	1.0000									
2	1.4142	1.4142	1.0000								
3	1.0000	2.0000	1.0000	1.0000							
4	0.7654	1.8478	1.8478	0.7654	1.0000						
5	0.6180	1.6180	2.0000	1.6180	0.6180	1.0000					
6	0.5176	1.4142	1.9318	1.9318	1.4142	0.5176	1.0000				
7	0.4450	1.2470	1.8019	2.0000	1.8019	1.2470	0.4450	1.0000			
8	0.3902	1.1111	1.6629	1.9615	1.9615	1.6629	1.1111	0.3902	1.0000		
9	0.3473	1.0000	1.5321	1.8794	2.0000	1.8794	1.5321	1.0000	0.3473	1.0000	
10	0.3129	0.9080	1.4142	1.7820	1.9754	1.9754	1.7820	1.4142	0.9080	0.3129	1.0000

Source: Reprinted from G. L. Matthaei, L. Young, and E. M. T. Jones, *Microwave Filters, Impedance-Matching Networks, and Coupling Structures*, Artech House, Dedham, Mass., 1980, with permission.

- b) For filter architecture of Fig 8.25a, use the immittances & equations (8.64cd), & (8.70ab) to get necessary scaled & transformed shunt inductances and series capacitances:

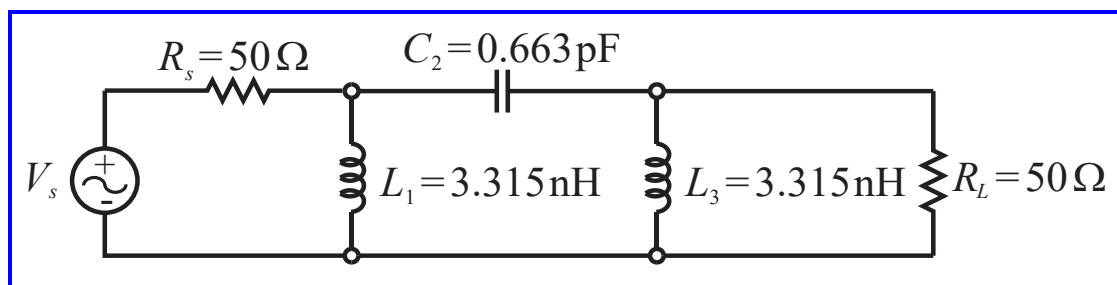
Per (8.64c), $R'_s = R_0 = 50 \Rightarrow \underline{R'_s = 50 \Omega.}$

Per (8.70b), $L'_1 = L'_3 = \frac{R_0}{\omega_c C_k} = \frac{R_0}{\omega_c g_1} = \frac{50}{(2\pi)2.4 \times 10^9 (1)} \Rightarrow \underline{L'_1 = L'_3 = 3.315 \text{ nH.}}$

Per (8.70a), $C'_2 = \frac{1}{R_0 \omega_c L_k} = \frac{1}{R_0 \omega_c g_2} = \frac{1}{50(2\pi)2.4 \times 10^9 (2)} \Rightarrow \underline{C'_2 = 0.663 \text{ pF.}}$

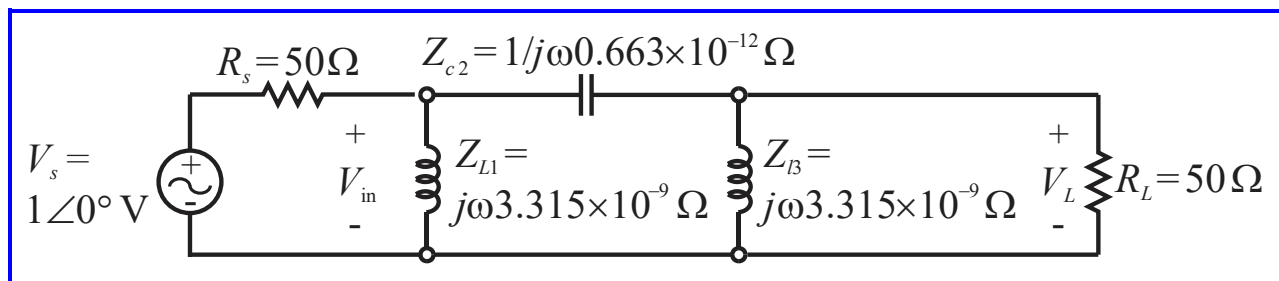
Per (8.64d), $R'_L = R_0 R_L = R_0 g_4 = 50(1) \Rightarrow \underline{R'_L = 50 \Omega.}$

➤ The resulting **Butterworth highpass** filter circuit with component values is:



- c) From circuits, use $Z_R = R$, $Z_L = j\omega L$, and $Z_C = 1/j\omega C$.

The resulting **Butterworth highpass** filter circuit in phasor form is:



- d) Using MathCAD

System impedance	$Z_0 := 50 \quad \Omega$	$n := 1..500$	$f_n := n \cdot 10^7$
Butterworth lumped element design N = 3		$f_c := 2.4 \cdot 10^9 \quad \text{Hz}$	
Table 8.3 LPF prototype	$g_0 := 1$	$g_1 := 1$	$g_2 := 2 \quad g_3 := g_1 \quad g_4 := 1$
$R_S := g_0 \cdot Z_0$	$L_1 := \frac{Z_0}{2 \cdot \pi \cdot f_c \cdot g_1}$	$C_2 := \frac{1}{Z_0 \cdot g_2 \cdot 2 \pi \cdot f_c}$	$L_3 := L_1 \quad R_L := Z_0 \cdot g_4$
$V_S := 1 \quad \text{V}$	$R_S = 50 \quad \Omega$	$L_1 = 3.31573 \times 10^{-9} \quad \text{H}$	
$C_2 = 6.63146 \times 10^{-13} \quad \text{F}$	$L_3 = 3.31573 \times 10^{-9} \quad \text{H}$	$R_L = 50 \quad \Omega$	

Parallel impedance of RL & C3
$$Z1(f) := \left[\frac{1}{RL} + \frac{1}{(j \cdot 2 \cdot \pi \cdot f \cdot L3)} \right]^{-1}$$

Series impedance of L2 & Z1
$$Z2(f) := \frac{1}{(j \cdot 2 \cdot \pi \cdot f \cdot C2)} + Z1(f)$$

Input impedance of LP filter w/ load
$$Zin(f) := \left[\frac{1}{Z2(f)} + \frac{1}{(j \cdot 2 \cdot \pi \cdot f \cdot L1)} \right]^{-1}$$

Voltage divisions to get V_{in} & V_{ld}
$$V_{in}(f) := VS \cdot \frac{Zin(f)}{RS + Zin(f)} \quad V_{ld}(f) := V_{in}(f) \cdot \frac{Z1(f)}{Z2(f)}$$

$VIN_n := V_{in}(f_n) \quad VL_n := V_{ld}(f_n) \quad VL_dB_n := 20 \cdot \log(|VL_n|)$

$vert24 := \begin{pmatrix} 0 \\ -25 \end{pmatrix} \quad vertf := \begin{pmatrix} 2.4 \cdot 10^9 \\ 2.4 \cdot 10^9 \end{pmatrix}$

