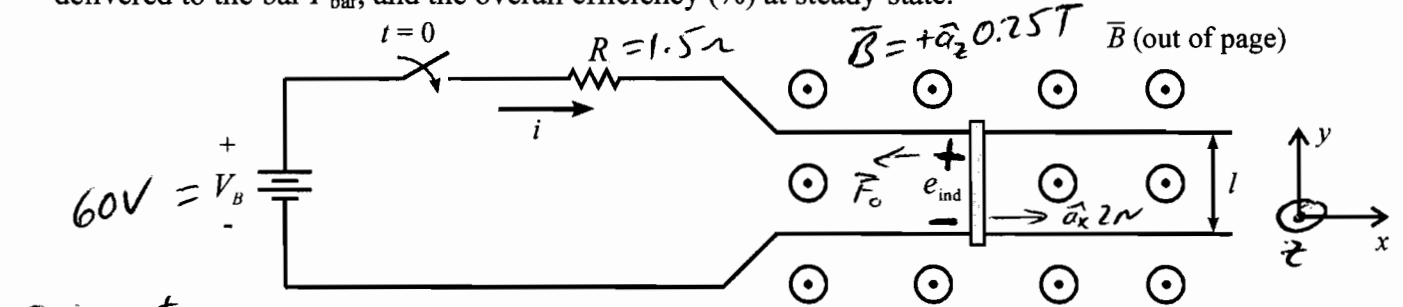


EE 330 (Spring 2012) Examination 1

Name Key A

Instructions: Show all work for full credit. Write answers in indicated places. Attach equation sheet to exam.

- 1) The linear DC machine shown has: $B = 250 \text{ mT}$, $l = 0.5 \text{ m}$, $R = 1.5 \Omega$, $m_{\text{bar}} = 1 \text{ kg}$, & $V_B = 60 \text{ V}$. With the brass bar initially at rest, find the current i_0 , induced voltage $e_{\text{ind},0}$, and force \vec{F}_0 on the bar at $t = 0^+$. If a force of $2\hat{a}_x \text{ (N)}$ is later applied to the moving bar, determine the **steady-state** current i_{ss} (direction per figure), vector velocity \vec{v}_{ss} , and induced voltage $e_{\text{ind,ss}}$ across the bar (show polarity on figure). Is the machine acting as a motor or a generator? Also, find the power supplied by the battery P_{batt} , power delivered to the bar P_{bar} , and the overall efficiency (%) at steady-state.



@ $t = 0^+$ $e_{\text{ind},0} = 0$ since $\vec{v}_0 = 0$

By KVL $-V_B + i_0 R + 0 = 0 \Rightarrow i_0 = \frac{V_B}{R} = \frac{60}{1.5} = 40 \text{ A}$

$\vec{F}_0 = i (\vec{l} \times \vec{B}) = 40 (-\hat{a}_y 0.5 \times \hat{a}_z 0.25) = -\hat{a}_x 5 \text{ N}$

② S.S. w/ $\vec{F}_{\text{app}} = \hat{a}_x 2 \text{ N} \Rightarrow$ @ S.S., $\vec{a} = 0$ so $\vec{F}_{\text{ind}} + \vec{F}_{\text{app}} = 0$ (opposing)

so $\vec{F}_{\text{ind,ss}} = -\hat{a}_x 2 = i_{\text{ss}} (-\hat{a}_y 0.5 \times \hat{a}_z (0.25)) = -\hat{a}_x 0.125 i_{\text{ss}}$

$\hookrightarrow i_{\text{ss}} = \frac{2}{0.125} = 16 \text{ A}$

By KVL, $-V_B + i_{\text{ss}} R + e_{\text{ind,ss}} = 0 \Rightarrow e_{\text{ind,ss}} = 36 \text{ V}$

Also $e_{\text{ind,ss}} = 36 \text{ V} = (\vec{v}_{\text{ss}} \times \vec{B}) \cdot \vec{l} = (\vec{v}_{\text{ss}} \times \hat{a}_z (0.25)) \cdot \hat{a}_y 0.5 \Rightarrow \vec{v}_{\text{ss}} = -\hat{a}_x \frac{36}{0.25(0.5)} = -\hat{a}_x 288 \text{ m/s}$

Batt: $P_{\text{batt}} = 60(16) = 960 \text{ W}$

$i^2 R = 16^2(1.5) = 384 \text{ W}$

Bar: $P_{\text{bar}} = F v_{\text{ss}} = (2 \text{ N})(288) = 576 \text{ W}$

$\eta = \frac{576}{960} \times 100\%$

$i_0 = 40 \text{ A}$

$e_{\text{ind},0} = 0$

$\vec{F}_0 = -\hat{a}_x 5 \text{ N}$

$\vec{v}_{\text{ss}} = -\hat{a}_x 288 \text{ m/s}$

$i_{\text{ss}} = 16 \text{ A}$

$e_{\text{ind,ss}} = 36 \text{ V}$

$P_{\text{batt}} = 960 \text{ W}$

$P_{\text{bar}} = 576 \text{ W}$

efficiency = 60%

(motor) or generator? Circle correct answer

2) A 60 Hz, 180-kVA, 240/2500-V_{rms} step-up transformer has **per-unit** equivalent circuit parameters of $R_{series} = 0.013$, $X_{series} = 0.06$, $X_m = 46$, and $R_C = 64$. Using this information, calculate and sketch a fully-labeled approximate transformer equivalent circuit (with units) referred to the **secondary** side. What is the turns ratio a ? Next, a 160-kVA load with a power factor of 0.75 lagging is connected to the transformer. Assuming that the load is receiving the rated secondary voltage (use as reference), determine the phasor load current \bar{I}_L & primary voltage \bar{V}_P , and voltage regulation VR (%). **Extra credit:** Determine the core losses P_{core} , resistive line losses P_{cu} , and efficiency η of the transformer.

$$a = \frac{V_p}{V_s} = \frac{240}{2500} = 0.096 \quad Z_{base} = \frac{V_{base}^2}{S_{base}} = \frac{2500^2}{180 \times 10^3} = 34.72 \Omega$$

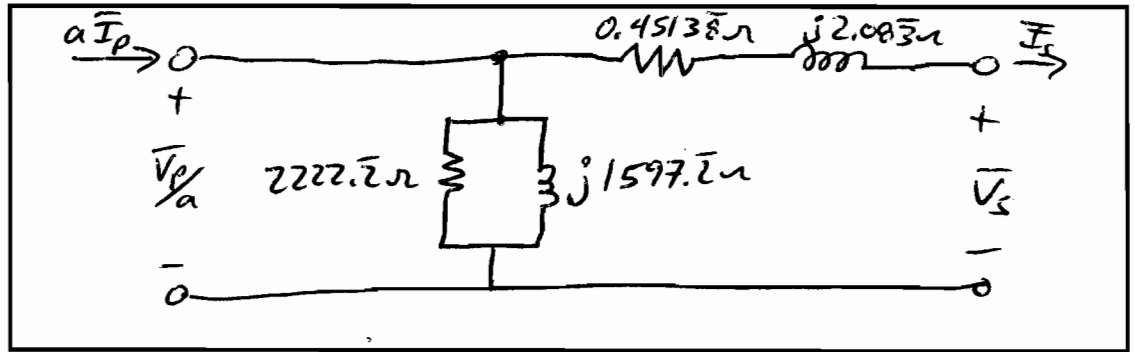
$$R_{eq,s} = 0.013(34.72) = 0.45138 \Omega$$

$$X_{eq,s} = 0.06(34.72) = 2.0832 \Omega$$

$$R_{C,s} = 64(34.72) = 2222.2 \Omega$$

$$X_{m,s} = 46(34.72) = 1597.2 \Omega$$

Secondary-side equivalent circuit



$$I_{LO} = \frac{S_{LO}}{V_{LO}} = \frac{160 \times 10^3}{2500} = 64 \text{ A}_{rms}$$

$$a = 0.096$$

$$\bar{V}_{LO} = 2500 \angle 0^\circ \text{ V}_{rms} \quad \theta = \theta_V - \theta_I = \cos^{-1} 0.75 = 41.4096^\circ \Rightarrow \theta_I = -41.41^\circ$$

By KVL $\bar{V}_p/a = \bar{I}_s(0.4514 + j2.083) + \bar{V}_s = 64 \angle -41.41^\circ (0.4514 + j2.083) + 2500 \angle 0^\circ$
 $= 2611.11168 \angle 1.7753^\circ \text{ V}_{rms} \Rightarrow \bar{V}_p = 0.096(\bar{V}_p/a) = 250.67 \angle 1.775^\circ$

$$VR = \frac{V_p/a - V_s}{V_s} \times 100\% = \frac{2611.11 - 2500}{2500} \times 100\% = 4.4445\%$$

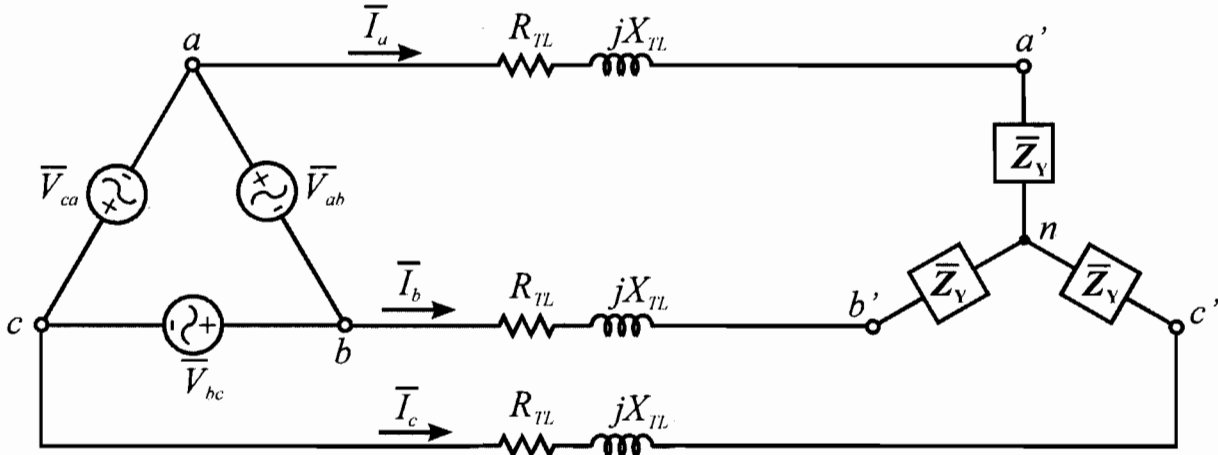
$$P_{core} = \frac{(V_p/a)^2}{R_{C,s}} = \frac{2611.11^2}{2222.2} = 3068.06 \text{ W} \quad P_{cu} = I_s^2 R_{eq,s} = 64^2(0.4514) = 1848.8 \text{ W}$$

$$\bar{I}_L = 64 \angle -41.41^\circ \text{ A}_{rms} \quad \bar{V}_p = 250.67 \angle 1.775^\circ \text{ V}_{rms} \quad VR = 4.4445\%$$

Extra credit: $P_{core} = 3068.06 \text{ W} \quad P_{cu} = 1848.89 \text{ W} \quad \eta = 96.064\%$

$$\eta = \frac{160 \times 10^3 (0.75)}{160 \times 10^3 (0.75) + 3068 + 1849}$$

3) For the 3 ϕ circuit shown, $\bar{V}_{ab} = V_{\phi} \angle 0^{\circ}$, $\bar{V}_{bc} = V_{\phi} \angle -120^{\circ}$, $\bar{V}_{ca} = V_{\phi} \angle -240^{\circ}$ with $V_{\phi} = 480 \text{ V}_{\text{rms}}$, $R_{TL} = 0.2 \Omega$, $X_{TL} = 0.6 \Omega$, and $\bar{Z}_Y = 3 + j2 \Omega$. Determine the magnitude of the line currents I_L , magnitude of the line-to-line $V_{LL,LD}$ and phase $V_{\phi,LD}$ voltages for the loads, magnitude of the voltage drop on the transmission lines V_{line} , total complex power \bar{S}_{load} for the loads, total complex power \bar{S}_{line} for the lines, and the power factor pf seen by the source.



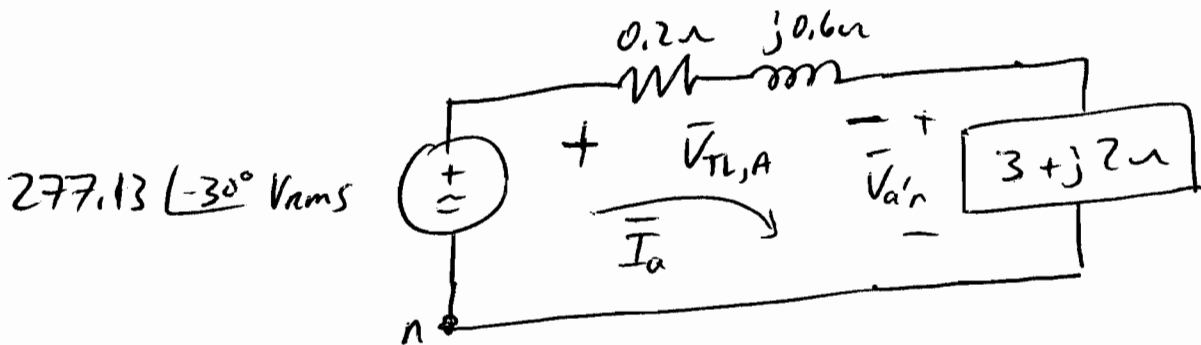
$\Delta \rightarrow Y$ Source Conversion

$$\bar{V}_{an} = \frac{480}{\sqrt{3}} \angle -30^{\circ} = 277.13 \angle -30^{\circ} \text{ V}_{\text{rms}}$$

$$\bar{V}_{bn} = \frac{480}{\sqrt{3}} \angle -150^{\circ} = 277.13 \angle -150^{\circ} \text{ V}_{\text{rms}}$$

$$\bar{V}_{cn} = \frac{480}{\sqrt{3}} \angle -270^{\circ} = 277.13 \angle -270^{\circ} \text{ V}_{\text{rms}}$$

Using Phase A, the per-phase equiv. circuit is:



$$\bar{I}_a = \frac{277.13 \angle -30^{\circ}}{(0.2 + j0.6) + (3 + j2)} = 67.213444 \angle -69.093859^{\circ} \text{ A}_{\text{rms}}$$

↑
 I_L

3) continued

$$\begin{aligned}\bar{V}_{TL,A} &= \bar{I}_a(0.2+j0.6) = (67.21 \angle -69.1^\circ)(0.2+j0.6) \\ &= \underline{42.5095145 \angle 2.47119229^\circ} \text{ V}_{rms}\end{aligned}$$

↖ V_{line}

$$\bar{V}_{a'n} = \bar{I}_a(3+j2) = (67.21 \angle -69.1^\circ)(3+j2) = \underline{242.34152 \angle -35.03791^\circ}$$

Y → Δ

$$V_{LL,LD} = \sqrt{3} V_{\phi,LD} = \underline{419.7478} \text{ V}_{rms}$$

↖ $V_{\phi,LD}$

$$\begin{aligned}\bar{S}_{load} &= 3 \bar{S}_{LN,A} = 3 \bar{V}_{a'n} \bar{I}_a^* = 3(242.34 \angle -35.04^\circ)(67.21 \angle +69.1^\circ) \\ &= \underline{48,865.8 \angle 33.69^\circ} \text{ VA} = 40658.8 + j 27,105.9 \text{ VA}\end{aligned}$$

$$\begin{aligned}\bar{S}_{line} &= 3 \bar{S}_{line,A} = 3 \bar{V}_{TL,A} \bar{I}_a^* = 3(42.5095 \angle 2.47^\circ)(67.21 \angle +69.1^\circ) \\ &= \underline{8571.6 \angle 71.565^\circ} \text{ VA} = 2710.6 + j 8131.8 \text{ VA}\end{aligned}$$

$$\bar{S}_{TOT} = \bar{S}_{Load} + \bar{S}_{line} = \underline{55880.2 \angle 39.094^\circ}$$

$$pf = \cos 39.093859^\circ = 0.7761 \text{ lagging}$$

$$I_L = \underline{67.213} \text{ A}_{rms} \quad V_{LL,LD} = \underline{419.75} \text{ V}_{rms} \quad V_{\phi,LD} = \underline{242.34} \text{ V}_{rms} \quad V_{line} = \underline{42.51} \text{ V}_{rms}$$

$$\begin{aligned}\bar{S}_{load} &= \underline{48.866 \angle 33.69^\circ} \text{ kVA} \\ &40.66 + j 27.11 \text{ kVA}\end{aligned}$$

$$\begin{aligned}\bar{S}_{line} &= \underline{8.57 \angle 71.565^\circ} \text{ kVA} \\ &2.71 + j 8.13 \text{ kVA}\end{aligned}$$

$$pf = \underline{0.7761} \text{ lagging}$$