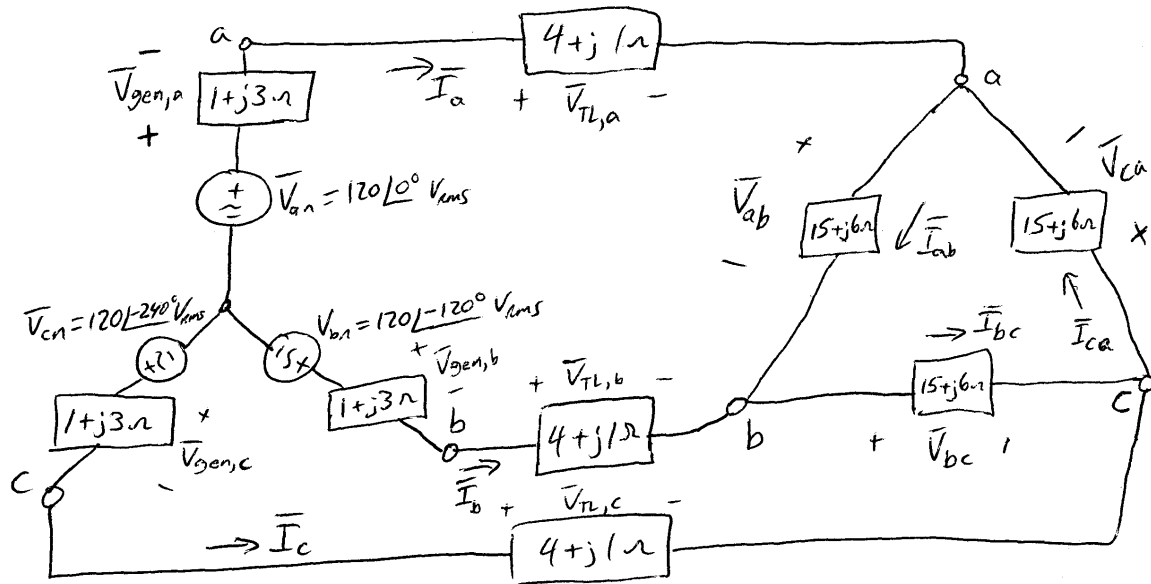


Three-Phase Circuit Power Example

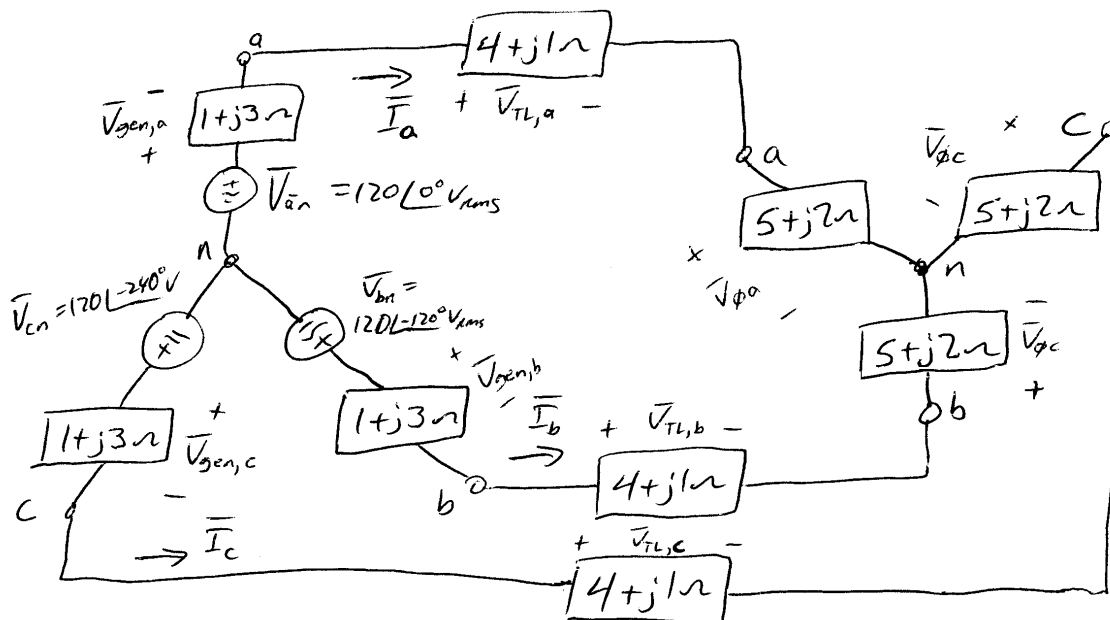
A balanced Y-configuration source (generator) has phase voltages of $120 \text{ V}_{\text{rms}}$ and an impedance of $1 + j3 \Omega$ per phase. The generator is connected to a balanced Δ -configuration load ($\bar{Z}_{\Delta} = 15 + j6 \Omega$) by balanced transmission lines (TLs) each with a line impedance of $4 + j1 \Omega$. Calculate all currents, voltages, and power quantities.



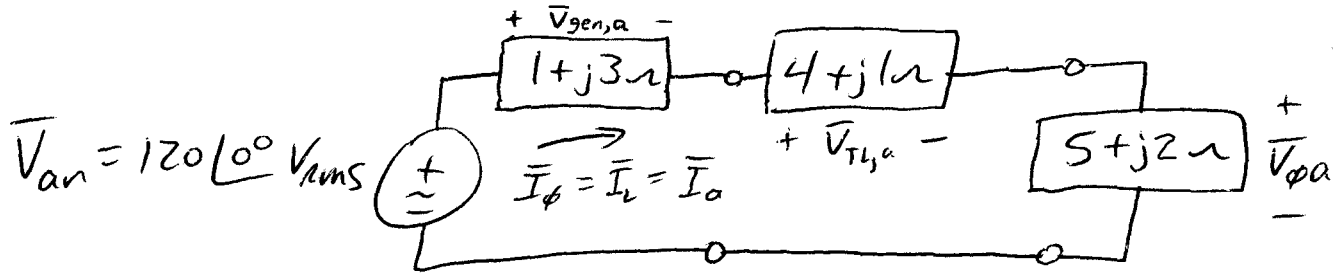
Step 1- Convert the Δ -load to an equivalent Y-load.

$$\bar{Z}_Y = \frac{\bar{Z}_{\Delta}}{3} = \frac{15 + j6}{3} \Rightarrow \bar{Z}_Y = 5 + j2 \Omega.$$

Step 2- Redraw the circuit. Note that all the impedances are now in series.



Step 3- Draw a per-phase equivalent circuit for phase a .



Step 4- Compute the equivalent impedance as well as phase and line currents.

The equivalent impedance 'seen' by source is

$$\bar{Z}_{eq} = (1 + j3) + (4 + j1) + (5 + j2) = 10 + j6 = 11.6619\angle 30.9638^\circ \Omega.$$

The phase/line current is

$$\bar{I}_a = \frac{\bar{V}_{an}}{\bar{Z}_{eq}} = \frac{120\angle 0^\circ}{11.6619\angle 30.9638^\circ} \Rightarrow \underline{\bar{I}_a = 10.290\angle -30.9638^\circ \text{ A}_{rms}},$$

$$\text{add } -120^\circ \text{ phase shift to get phase } b \Rightarrow \underline{\bar{I}_b = 10.290\angle -150.9638^\circ \text{ A}_{rms}},$$

$$\text{add } -240^\circ \text{ phase shift to get phase } c \Rightarrow \underline{\bar{I}_c = 10.290\angle -270.9638^\circ \text{ A}_{rms}},$$

and note the phase current magnitude is $\underline{I_\phi = 10.290 \text{ A}_{rms}}$.

Step 5- Compute various power quantities per-phase and overall.

The single-phase **powers** are

$$P_\phi = P_a = P_b = P_c = V_\phi I_\phi \cos(\theta) = 120(10.29) \cos(30.9638^\circ) \Rightarrow \underline{P_\phi = 1058.8 \text{ W}}.$$

The overall power from the ideal 3ϕ voltage source is

$$P = 3P_\phi = 3(1058.8) \Rightarrow \underline{P = 3176.5 \text{ W}}.$$

The single-phase **reactive powers** are

$$Q_\phi = Q_a = Q_b = Q_c = V_\phi I_\phi \sin(\theta) = 120(10.29) \sin(30.9638^\circ) \Rightarrow \underline{Q_\phi = 635.3 \text{ var}}.$$

The overall reactive power from the ideal 3ϕ voltage source is

$$Q = 3Q_\phi = 3(635.3) \Rightarrow \underline{Q = 1905.9 \text{ var}}.$$

The single-phase **complex powers** are

$$\begin{aligned}\bar{S}_\phi &= \bar{S}_a = \bar{S}_b = \bar{S}_c = P_\phi + jQ_\phi \\ \Rightarrow \bar{S}_\phi &= 1058.8 + j635.3 \text{ VA} = 1234.8 \angle 30.964^\circ \text{ VA}.\end{aligned}$$

The overall **complex power** from the ideal 3 ϕ voltage source is

$$\begin{aligned}\bar{S} &= 3\bar{S}_\phi = 3(1058.8 + j635.3) \\ \Rightarrow \bar{S} &= 3176.5 + j1905.9 \text{ VA} = 3704.4 \angle 30.964^\circ \text{ VA}.\end{aligned}$$

The single-phase **apparent powers** are

$$S_\phi = S_a = S_b = S_c = |\bar{S}_\phi| \Rightarrow \underline{S_\phi = 1234.8 \text{ VA}.$$

The overall **apparent power** from the ideal 3 ϕ voltage source is

$$S = 3S_\phi = 3(1234.8) \Rightarrow \underline{S = 3704.4 \text{ VA}.$$

The **power factor (PF)** overall and per-phase is

$$\text{PF} = P/S = P_\phi/S_\phi = \cos(\theta) = \cos(30.964^\circ) \Rightarrow \underline{\text{PF} = 0.8575 \text{ lagging } (Q > 0)}.$$

Step 6- Compute voltage drops & power quantities for **generator** impedances.

The voltage drops are found using Ohm's Law

$$\begin{aligned}\bar{V}_{gen,a} &= \bar{I}_a \bar{Z}_{gen} = (10.29 \angle -30.964^\circ)(1 + j3) \Rightarrow \underline{\bar{V}_{gen,a} = 32.54 \angle 40.6^\circ \text{ V}_{rms}}, \\ \bar{V}_{gen,b} &= \bar{I}_b \bar{Z}_{gen} = (10.29 \angle -150.964^\circ)(1 + j3) \Rightarrow \underline{\bar{V}_{gen,b} = 32.54 \angle -79.4^\circ \text{ V}_{rms}}, \text{ \& } \\ \bar{V}_{gen,c} &= \bar{I}_c \bar{Z}_{gen} = (10.29 \angle -270.964^\circ)(1 + j3) \Rightarrow \underline{\bar{V}_{gen,c} = 32.54 \angle -199.4^\circ \text{ V}_{rms}}.\end{aligned}$$

The **complex power** per phase is

$$\begin{aligned}\bar{S}_{gen,\phi} &= \bar{V}_{gen,a} \bar{I}_a^* = (32.54 \angle 40.6^\circ)(10.29 \angle +30.964^\circ) \\ \Rightarrow \underline{\bar{S}_{gen,\phi} &= 105.885 + j317.65 \text{ VA}.\end{aligned}$$

Overall **power** and **reactive power** for generator impedances are

$$P_{gen} = 3P_{gen,\phi} = 3(105.885) \Rightarrow \underline{P_{gen} = 317.7 \text{ W}} \text{ [Note: } P_{gen}/P = 10\% \text{ of total.]}$$

$$Q_{gen} = 3Q_{gen,\phi} = 3(317.65) \Rightarrow \underline{Q_{gen} = 953 \text{ var}} \text{ [Note: } Q_{gen}/Q = 50\% \text{ of total.]}$$

[Yikes! Not good. I need to work on my generators.]

Step 7- Compute voltage drops & power quantities for TL impedances.

The voltage drops are found using Ohm's Law

$$\begin{aligned}\bar{V}_{TL,a} &= \bar{I}_a \bar{Z}_{TL} = (10.29 \angle -30.964^\circ)(4 + j1) \Rightarrow \underline{\bar{V}_{TL,a} = 42.426 \angle -16.93^\circ \text{ V}_{\text{rms}}}, \\ \bar{V}_{TL,b} &= \bar{I}_b \bar{Z}_{TL} = (10.29 \angle -150.964^\circ)(4 + j1) \Rightarrow \underline{\bar{V}_{TL,b} = 42.43 \angle -136.9^\circ \text{ V}_{\text{rms}}}, \& \\ \bar{V}_{TL,c} &= \bar{I}_c \bar{Z}_{TL} = (10.29 \angle -270.964^\circ)(4 + j1) \Rightarrow \underline{\bar{V}_{TL,c} = 42.43 \angle -256.9^\circ \text{ V}_{\text{rms}}}.\end{aligned}$$

The **complex power** per phase is

$$\begin{aligned}\bar{S}_{TL,\phi} &= \bar{V}_{TL,a} \bar{I}_a^* = (42.426 \angle -16.93^\circ)(10.29 \angle 30.964^\circ) \\ &\Rightarrow \underline{\bar{S}_{TL,\phi} = 423.53 + j105.88 \text{ VA}}.\end{aligned}$$

Overall **power** and **reactive power** for TL impedances are

$$P_{TL} = 3P_{TL,\phi} = 3(423.53) \Rightarrow \underline{P_{TL} = 1270.6 \text{ W}} \text{ [Note: } P_{TL}/P = 40\% \text{ of total.]}$$

$$Q_{TL} = 3Q_{TL,\phi} = 3(105.88) \Rightarrow \underline{Q_{TL} = 317.7 \text{ var}} \text{ [Note: } Q_{TL}/Q = 16.7\% \text{ of total.]}$$

[Yikes! These are horrific TL losses. I need to buy/use heftier TLs.]

Step 8- Compute voltage drops & power quantities for loads.

The voltage drops for the **Y**-configuration equivalent are

$$\begin{aligned}\bar{V}_{\phi,a} &= \bar{I}_a \bar{Z}_Y = (10.29 \angle -30.964^\circ)(5 + j2) \Rightarrow \underline{\bar{V}_{\phi,a} = 55.413 \angle -9.16^\circ \text{ V}_{\text{rms}}}, \\ \bar{V}_{\phi,b} &= \bar{I}_b \bar{Z}_Y = (10.29 \angle -150.964^\circ)(5 + j2) \Rightarrow \underline{\bar{V}_{\phi,b} = 55.4 \angle -129.2^\circ \text{ V}_{\text{rms}}}, \& \\ \bar{V}_{\phi,c} &= \bar{I}_c \bar{Z}_Y = (10.29 \angle -270.964^\circ)(5 + j2) \Rightarrow \underline{\bar{V}_{\phi,c} = 55.4 \angle -249.2^\circ \text{ V}_{\text{rms}}}.\end{aligned}$$

The voltage drops for the actual **Δ** -configured loads are found using KVL

$$\begin{aligned}\bar{V}_{ab} &= \bar{V}_{\phi,a} - \bar{V}_{\phi,b} = (55.41 \angle -9.16^\circ) - (55.41 \angle -129.16^\circ) \Rightarrow \underline{\bar{V}_{ab} = 95.98 \angle 20.84^\circ \text{ V}_{\text{rms}}}, \\ \bar{V}_{bc} &= \bar{V}_{\phi,a} - \bar{V}_{\phi,b} \Rightarrow \underline{\bar{V}_{bc} = 95.98 \angle -99.16^\circ \text{ V}_{\text{rms}}}, \& \\ \bar{V}_{ca} &= \bar{V}_{\phi,c} - \bar{V}_{\phi,a} \Rightarrow \underline{\bar{V}_{ca} = 95.98 \angle -219.16^\circ \text{ V}_{\text{rms}}}.\end{aligned}$$

We see the line-to-line voltage for the Δ -configured loads is $V_{LL} = 95.98 \text{ V}_{\text{rms}}$ [or calculate using $V_{LL} = \sqrt{3} V_\phi = \sqrt{3} (55.413) = 95.98 \text{ V}_{\text{rms}}$]. This is a far cry from the $\sqrt{3} V_\phi = \sqrt{3} (120) = 207.85 \text{ V}_{\text{rms}}$ that left the ideal 3ϕ voltage sources.

The **currents** through the actual **Δ -configured** loads are found using Ohm's Law

$$\begin{aligned}\bar{I}_{ab} &= \bar{V}_{ab} / \bar{Z}_{\Delta} = (95.98 \angle 20.84^\circ) / (15 + j6) \Rightarrow \underline{\bar{I}_{ab} = 5.941 \angle -0.96^\circ \text{ A}_{\text{rms}}}, \\ \bar{I}_{bc} &= \bar{V}_{bc} / \bar{Z}_{\Delta} = (95.98 \angle -99.16^\circ) / (15 + j6) \Rightarrow \underline{\bar{I}_{bc} = 5.941 \angle -120.96^\circ \text{ A}_{\text{rms}}} \text{ \& } \\ \bar{I}_{ca} &= \bar{V}_{ca} / \bar{Z}_{\Delta} = (95.98 \angle -219.16^\circ) / (15 + j6) \Rightarrow \underline{\bar{I}_{ca} = 5.941 \angle -240.96^\circ \text{ A}_{\text{rms}}}.\end{aligned}$$

The **complex power** for the loads per-phase (using equivalent circuit)

$$\begin{aligned}\bar{S}_{LD,\phi} &= \bar{S}_{LD,a} = \bar{V}_{\phi,a} \bar{I}_a^* = (55.413 \angle -9.16^\circ)(10.29 \angle 30.964^\circ) \\ &\Rightarrow \underline{\bar{S}_{LD,\phi} = 529.4 + j211.8 \text{ VA}},\end{aligned}$$

or we can compute using voltage and current for the Δ -configuration

$$\begin{aligned}\bar{S}_{LD,\phi} &= \bar{S}_{LD,ab} = \bar{V}_{ab} \bar{I}_{ab}^* = 95.98 \angle 20.84^\circ (5.941 \angle +0.96^\circ) \\ &\Rightarrow \underline{\bar{S}_{LD,\phi} = 529.4 + j211.8 \text{ VA}}\end{aligned}$$

which yields the same answer.

The overall **power** and **reactive power** for the loads are

$$\begin{aligned}P_{LD} &= 3P_{LD,\phi} = 3(529.4) \Rightarrow \underline{P_{LD} = 1588.2 \text{ W}} \text{ [Note: } P_{LD}/P = 50\% \text{ of total.]} \\ Q_{LD} &= 3Q_{LD,\phi} = 3(211.8) \Rightarrow \underline{Q_{TL} = 635.3 \text{ var}} \text{ [Note: } Q_{TL}/Q = 33.3\% \text{ of total.}]\end{aligned}$$

In summary, the generator and TLs used in this example are awful! I need to spend some money (\$\$\$) to buy/design (or choose more realistic values) a better generator and TLs. General Electric, Siemens, ... do far better with their generators while Belden, Southern Wire, ... do far better with their TLs.